

Materials for spallation sources -topics from IWSMT-

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(October 20, 2009)

A short pulse spallation neutron source in mercury target

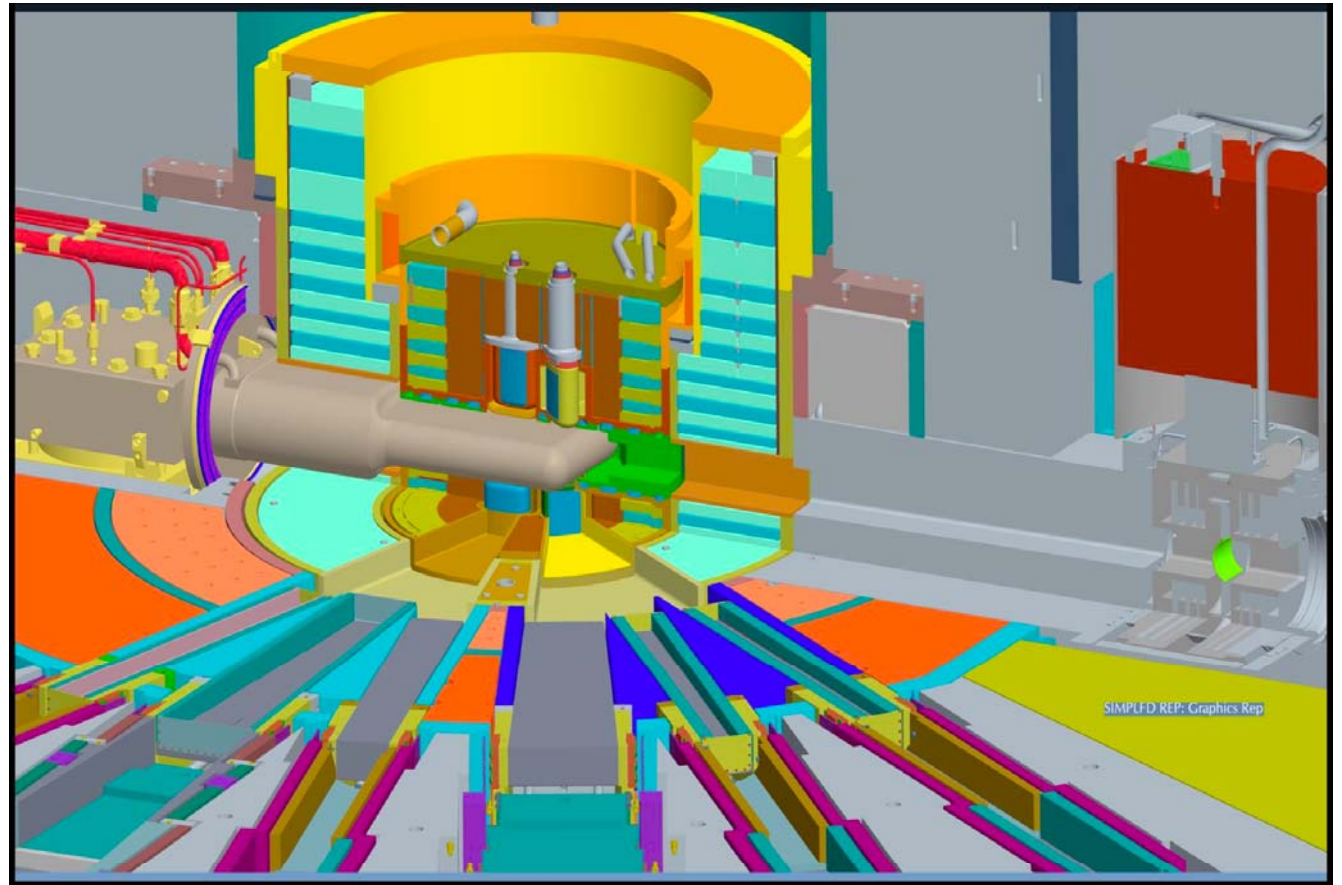
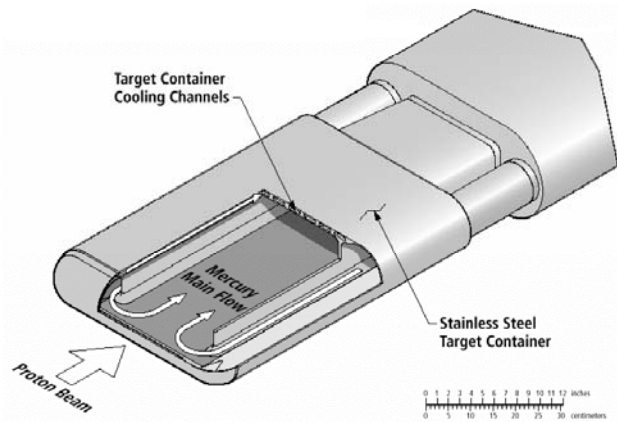
- ASTE[ORNL,JAERI,ESS,LANL]
- Exp. at AGS/BNL, pressure wave and particle transport in 1997.
- Pressure wave exp. at WNR/LANL in 2001.
- US-SNS operating from 2006/4月, now 1MW.
- J-PARC MLF operating from 2008/12, now 0.02 MW
- ESS canceled in 2004, and revises mercury or rotating W target in 5MW/2mA.

Liquid Metal Targets: Candidate Materials

Property		Pb	Bi	LME *	LBE**	Hg
Composition		elem.	elem.	Pb 97.5% Mg 2.5%	Pb 45% Bi 55%	elem.
Atomic mass A (g/mole)		207.2	209	202.6	208.2	200.6
Linear coefficient of thermal expansion (10^{-5} K^{-1})	solid liqu. (400°C)	2.91 4	1.75	4		6.1
Volume change upon solidification (%)		3.32	-3.35	3.3	0	
Melting point (°C)		327.5	271.3	250	125	-38.87
Boiling point at 1 atm (°C)		1740	1560			356.58
Specific heat (J/gK)		0.14	0.15	0.15	0.15	0.12
Th. neutron absorpt. (barn)		0.17	0.034	0.17	0.11	389

* Lead magnesium eutectic ** Lead bismuth eutectic

SNS Hg target, 1GeV, up to 2WM / ORNL



SS316L.. the liquid mercury target vessel
and water-cooled shroud

McManamy, ORNL

SNS Hg target, 3GeV / J-PARC



SS316L:Target & Helium vessels

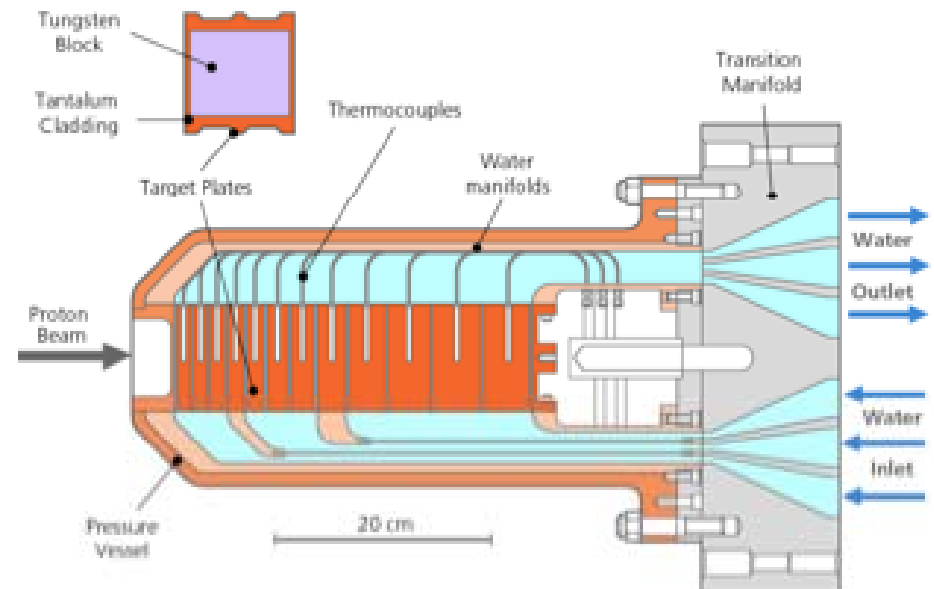
Oyama, J-PARC

Solid target

- U high neutron yield but difficult to handle
- W erosion under high speed water flow
- Ta decay heat, brittle or ductile?
- Au ?
- Pt ?

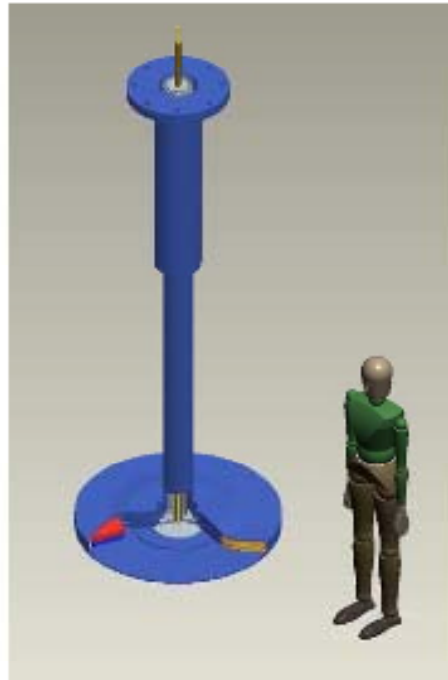
ISIS, Rutherford Appleton Laboratory

- Design for 800 MeV, 200 μ A
- Target types
 - Zircalloy-2 clad U-238
 - Tantalum
 - Tantalum clad W
- In operation since 1984
- Have highly developed remote handling capability



www.isis.rl.ac.uk/accelerator-2006

Target Module

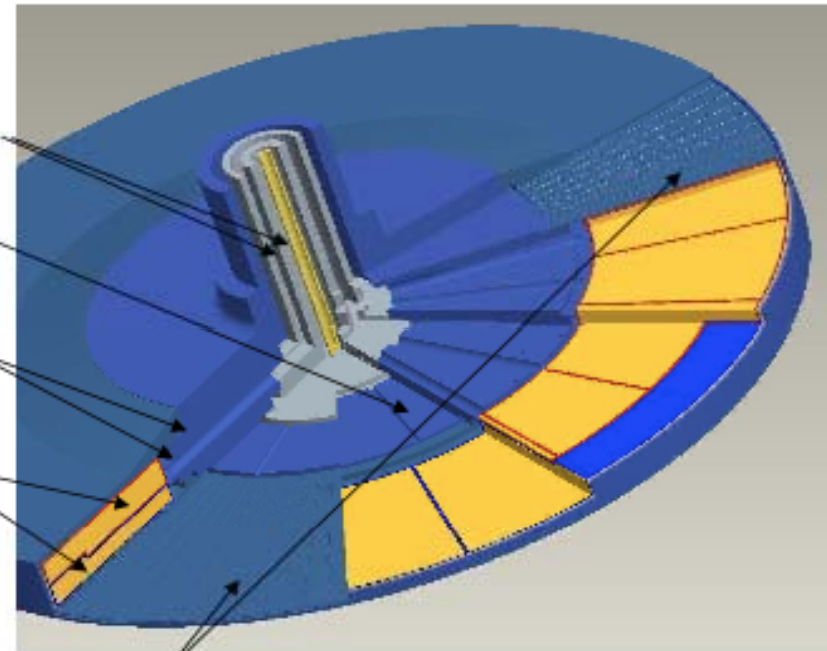


Concentric Shaft
Channels

Gun Drilled Hub

Circumferential
Manifolds

Tantalum Clad
Tungsten Blocks



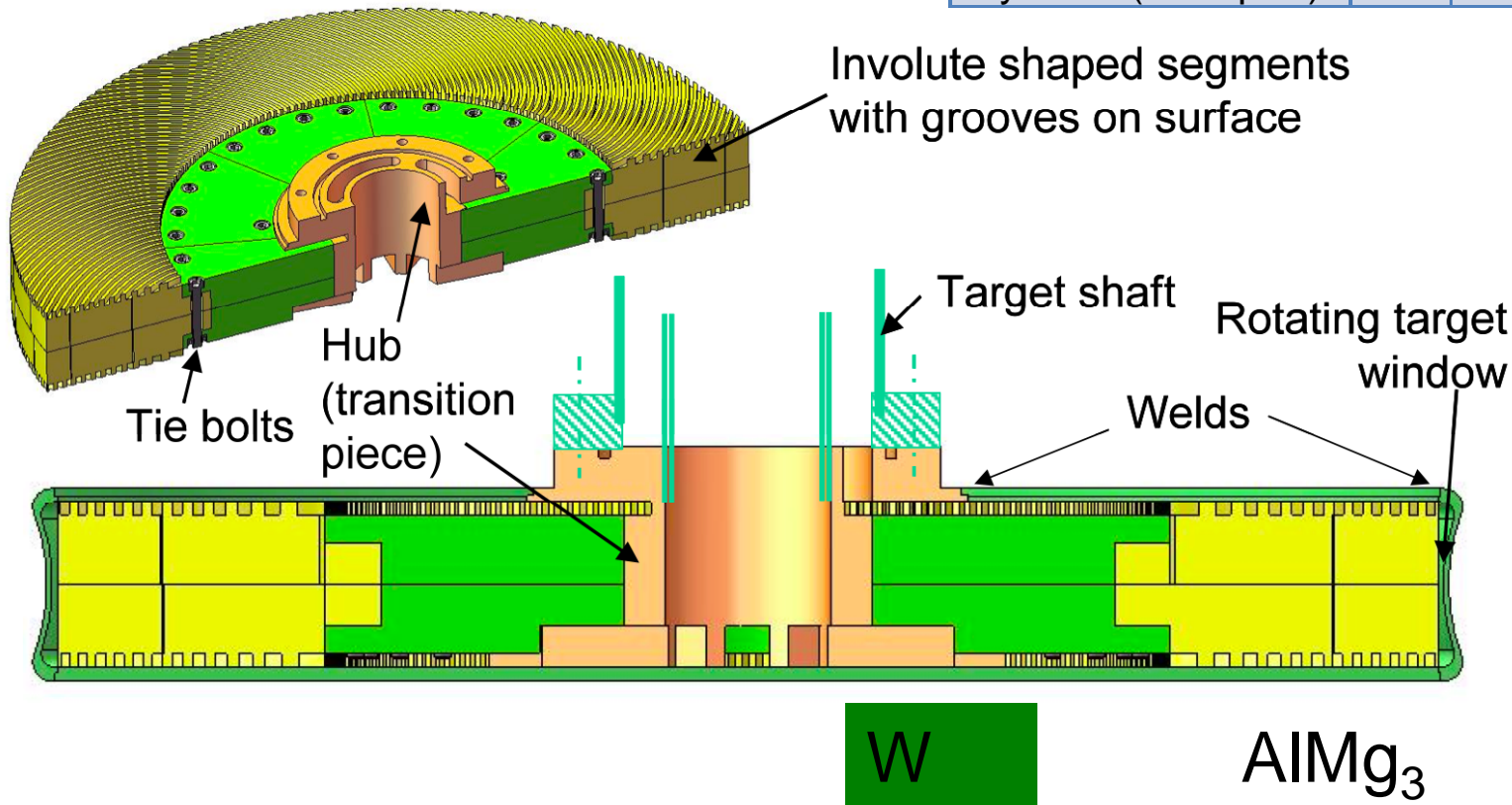
Shroud Cooling
Channels

- **The target module includes the clad segments, shroud and axle.**
- **The joint between the target and drive modules must be very precise. This joint also includes a significant water seal assembly.**
- **Concentric pipes inside the axle will require differential thermal expansion capability.**

Conceptual Solution for the CSNS Rotating Target Disk

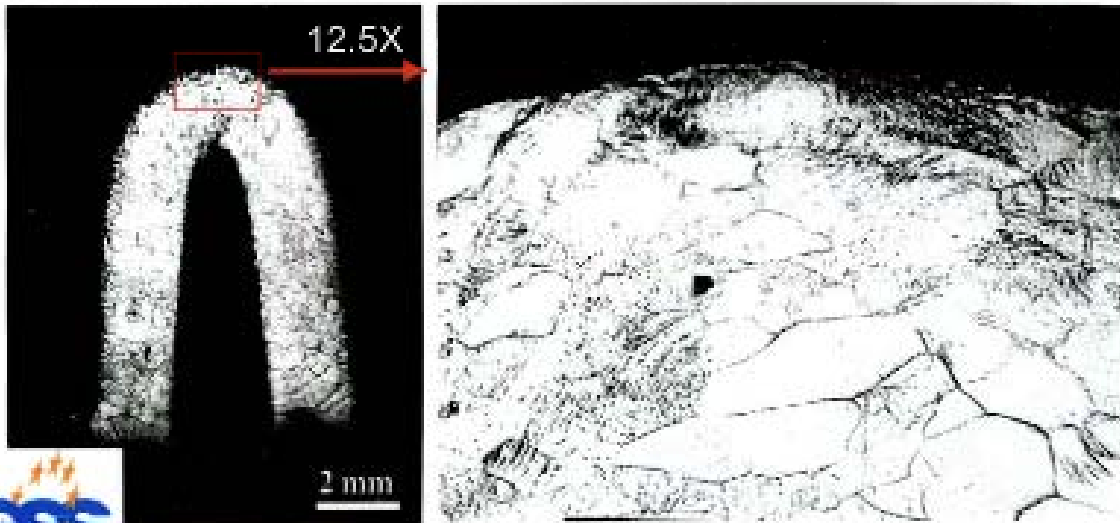
Xeujun, CSNS

Parameter		Early operation	Upgrade option
General			
Proton energy	Me V	1600	1600
Beam power	kW	120	500
Power deposited in target	kW	50.00	210
Target			
Outer diameter of cylinder	cm	50.00	50
Full height of cylinder (solid part)	cm	5.00	5

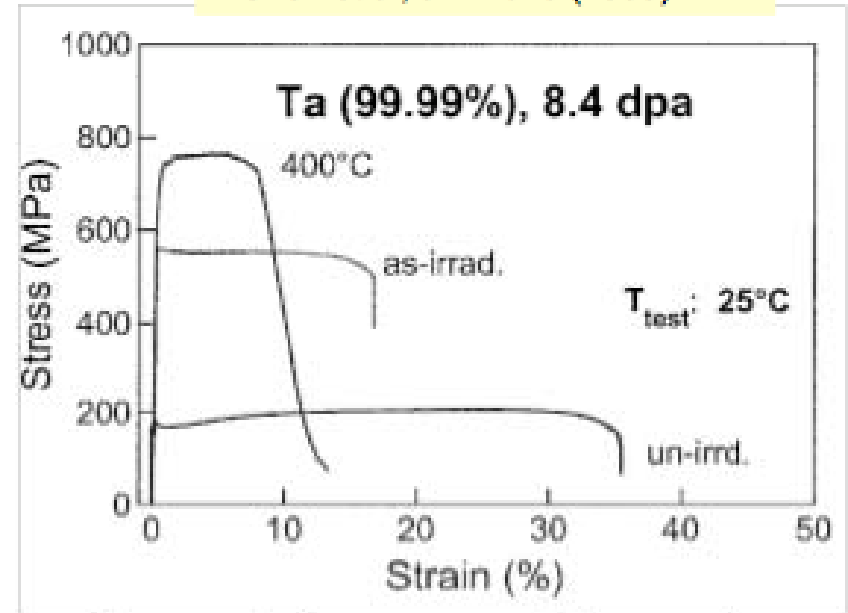


Spent ISIS Target: The Tantalum Puzzle

Side view of a bent Ta specimen from an ISIS target irradiated to 13 dpa with 800 MeV protons



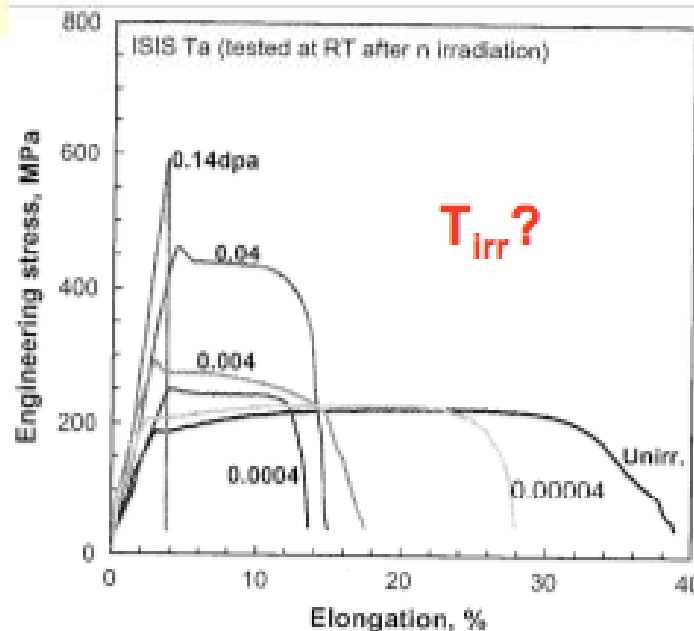
Chen et al, JNM 343 (2005)227



Stress-strain curves of Ta specimens from an ISIS-target tested at a strain rate of $10^{-3}/s$



ICANS XV



Engineering stress-strain curves for ISIS Ta at room temperature after neutron irradiation

TS Byun and SA Maloy JNM 377 (2008) 72

Cladding of LANSCE Tungsten Neutron Scattering Target with Tantalum



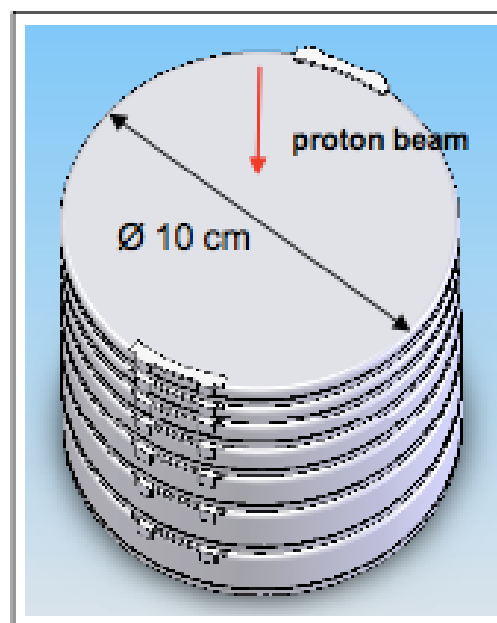
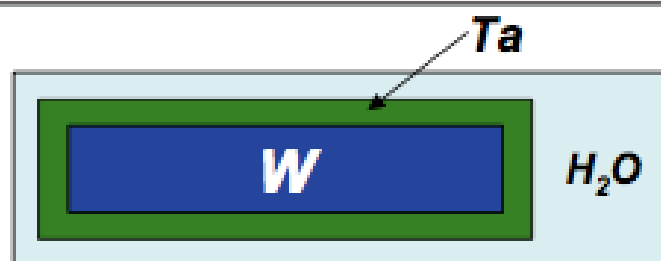
Plans underway to Clad MLNSC Target with Ta

- Main reason is to reduce activity for the water cooling system
- Initial HIP bonding tests at 1500C were successful
- Plan to have new targets fabricated by March 2009

Manuel Lujan Jr.
Neutron Scattering Center

LANSCE

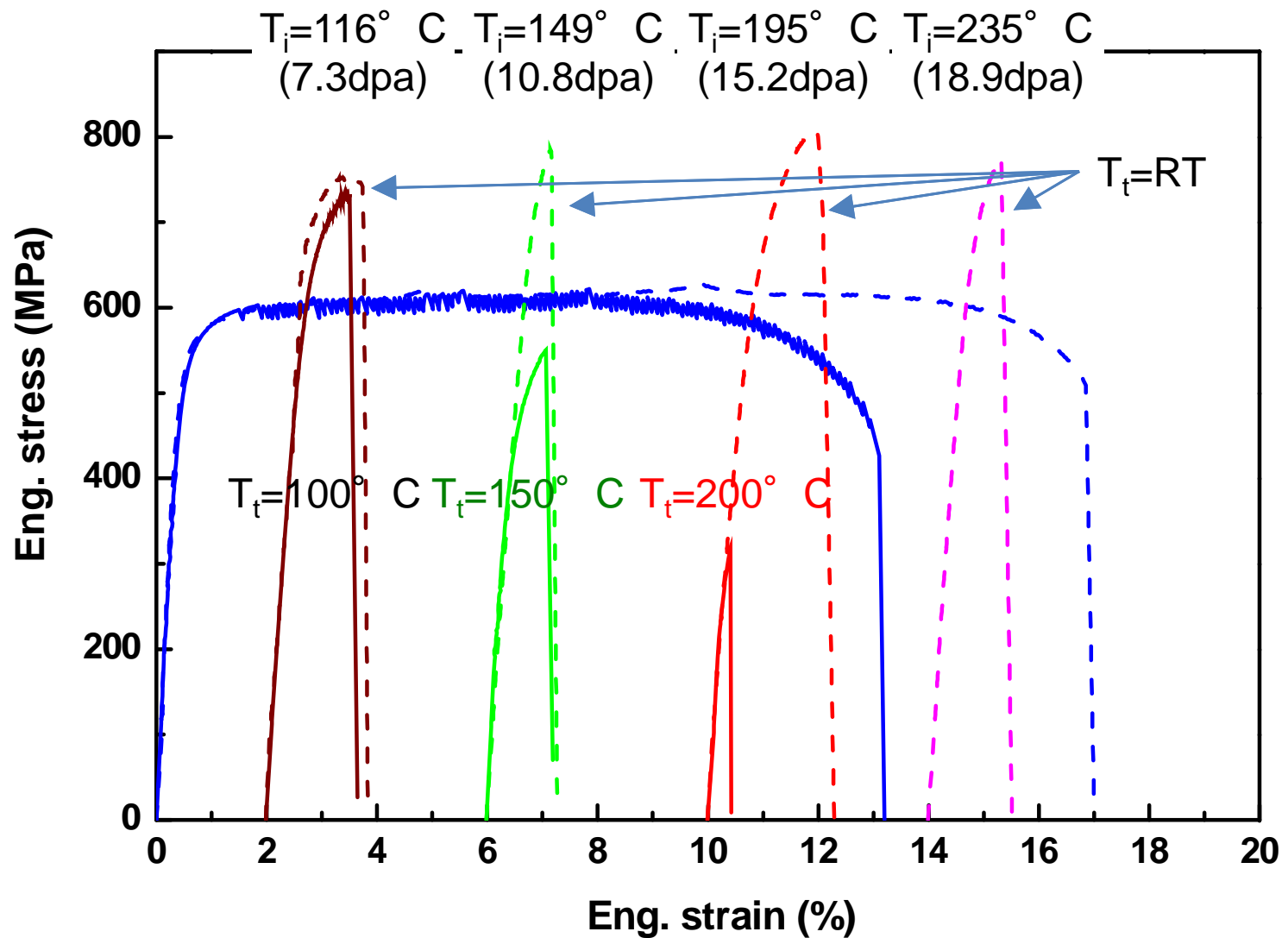
- Tungsten target 'pucks'
- Light water coolant
- Tantalum cladding



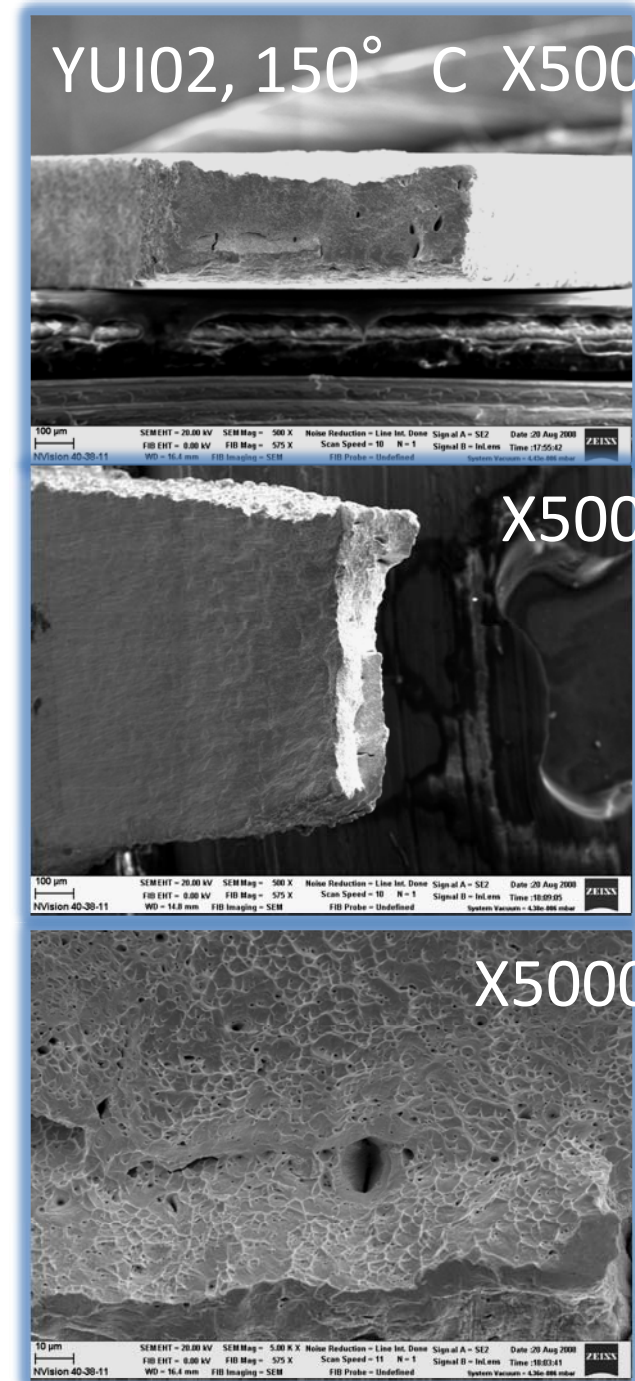
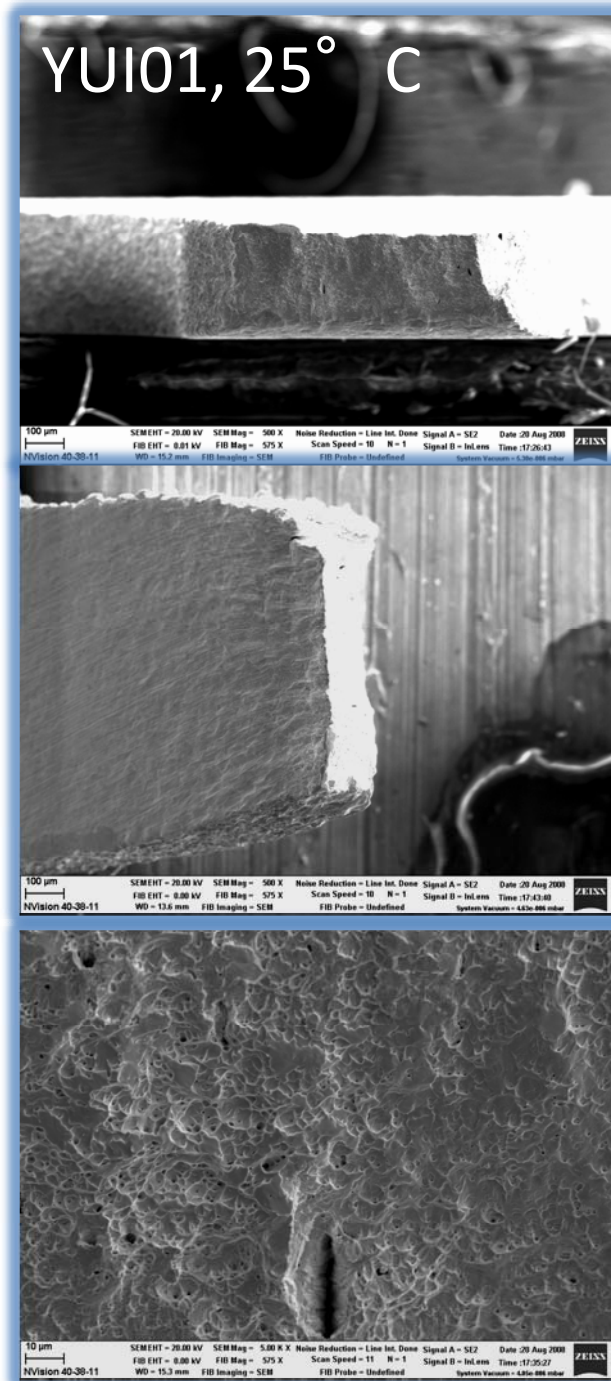
Maloy LANL

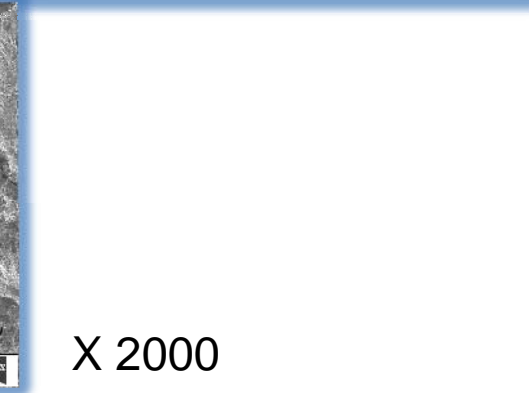
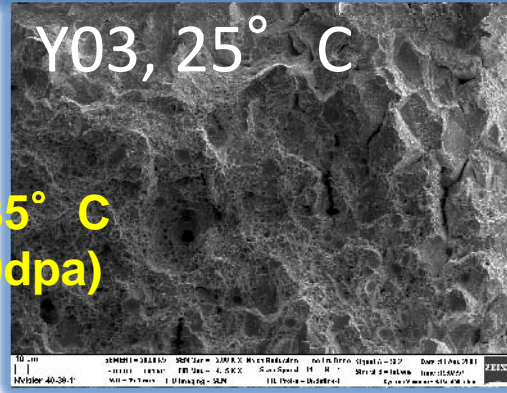
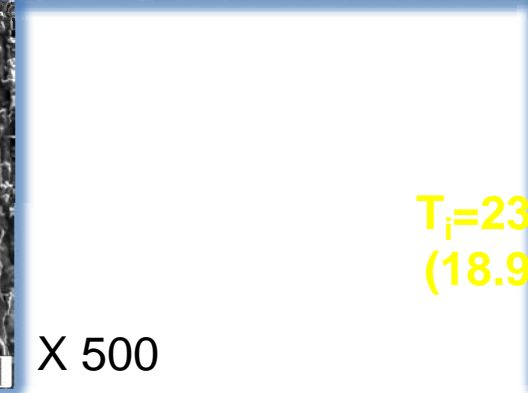
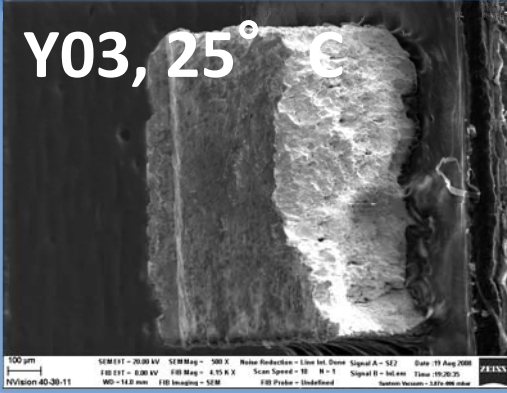
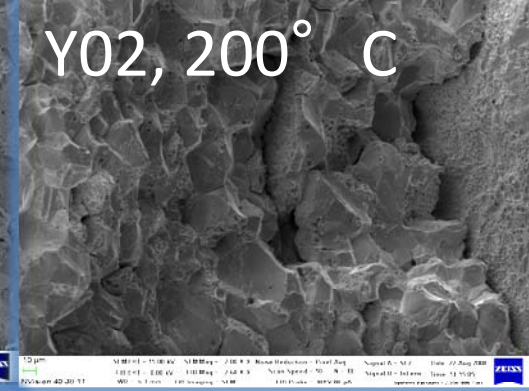
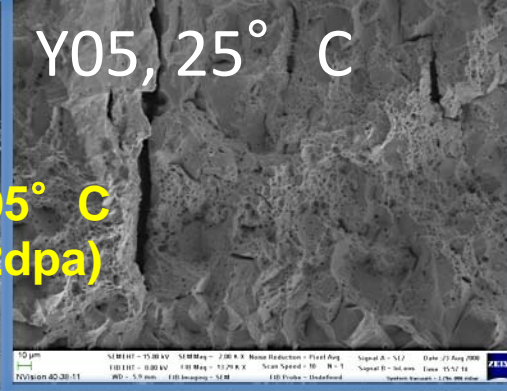
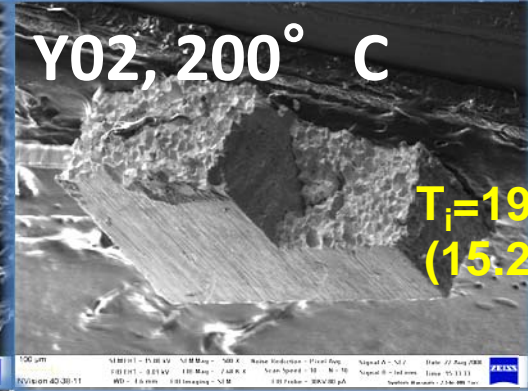
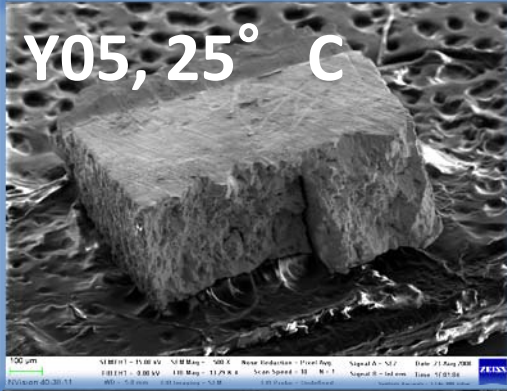
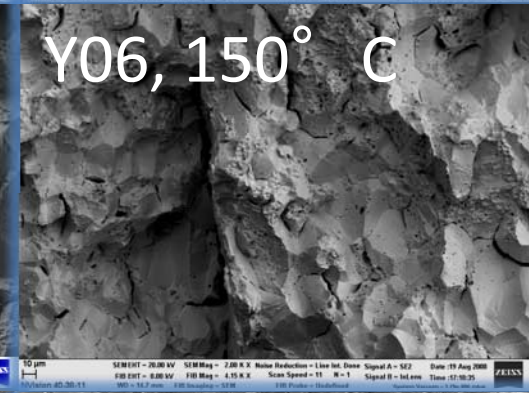
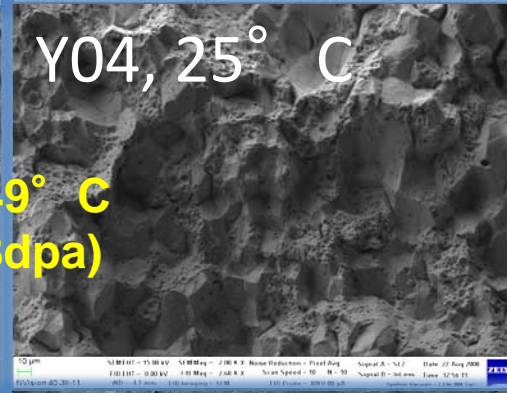
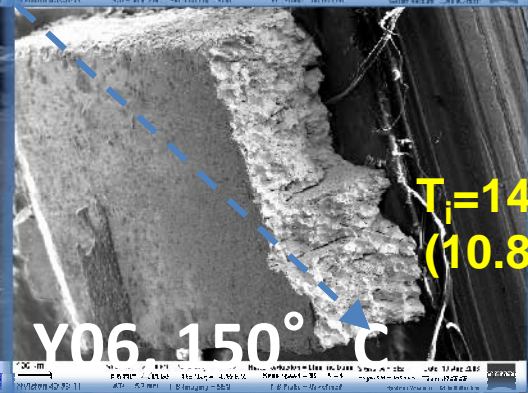
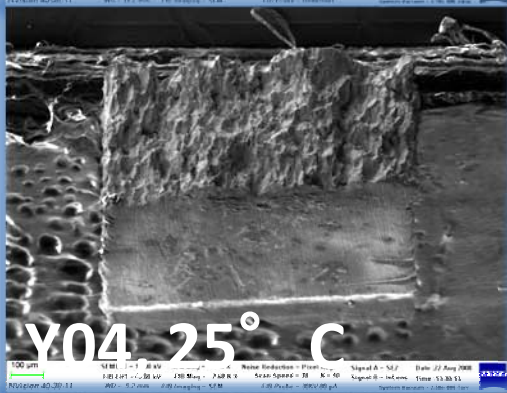
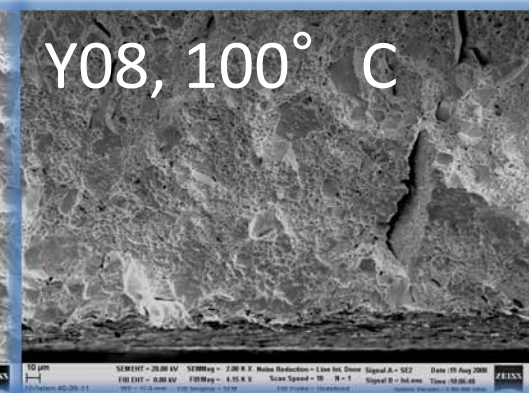
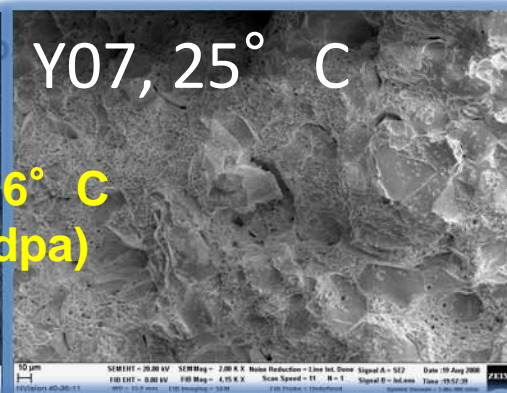
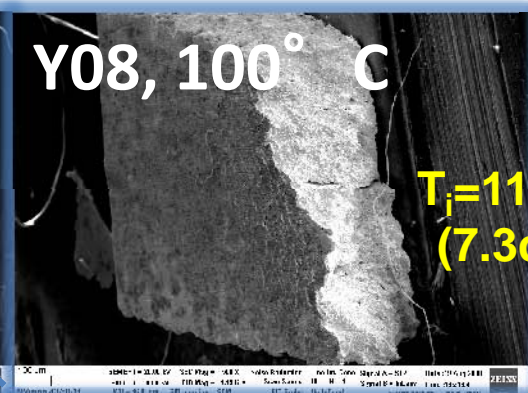
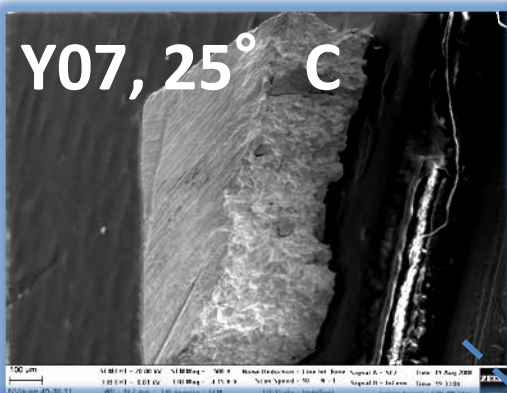
Result – Au alloys

◆ After irradiation



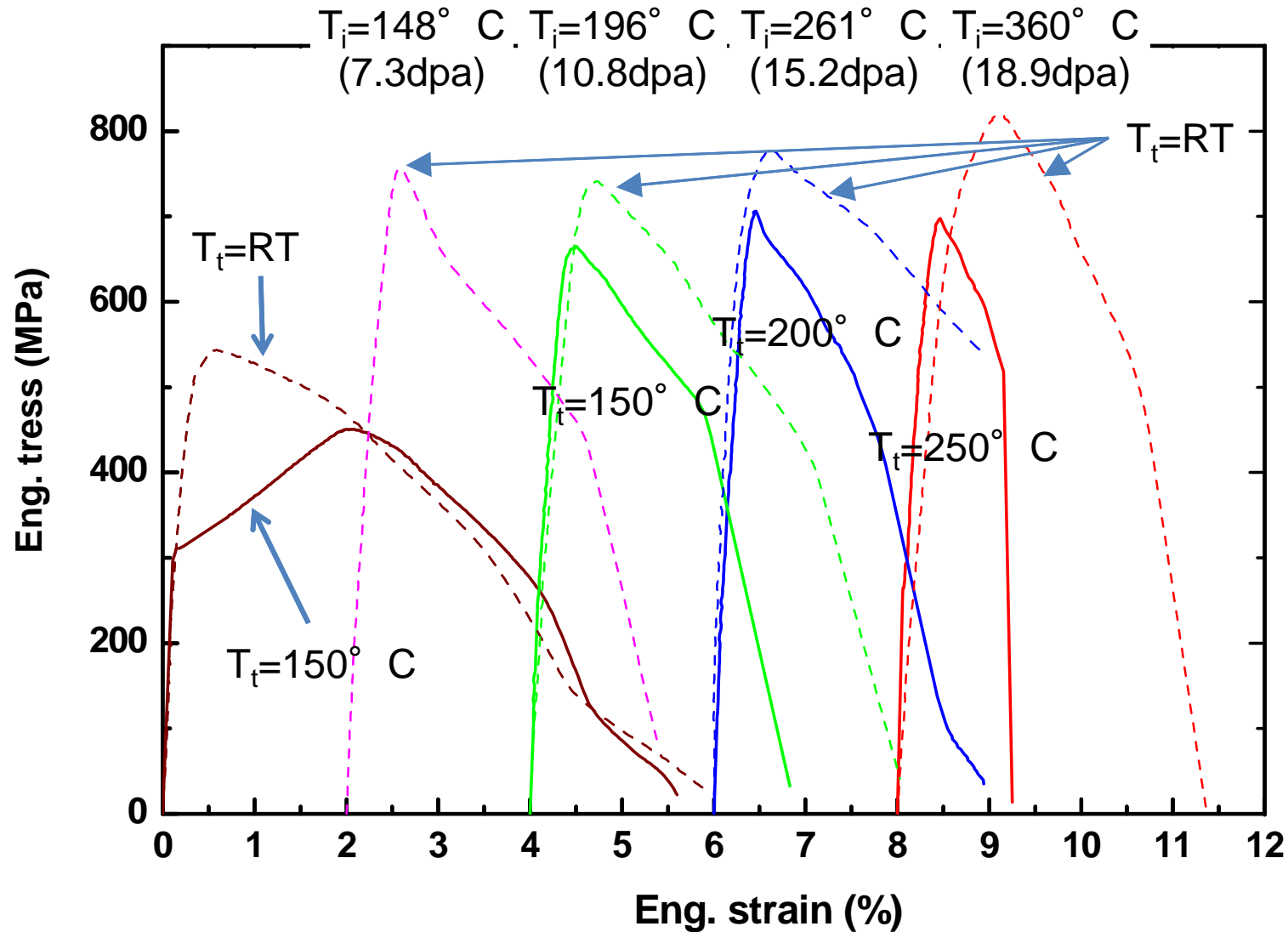
Fracture surface
Unirradiated Au
alloy
(75Au-9Ag-16Cu)



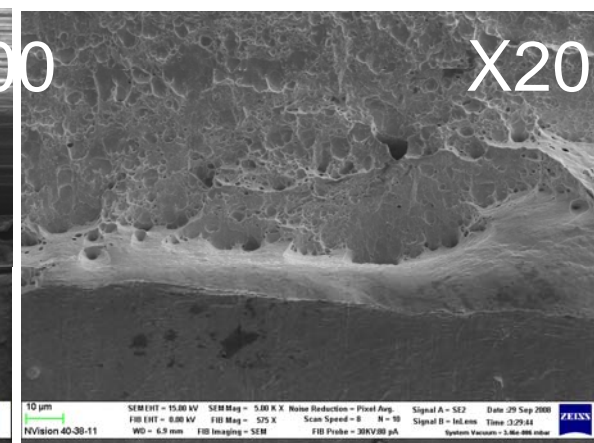
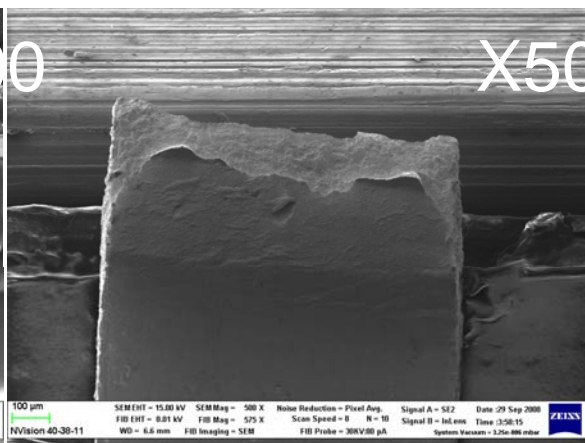
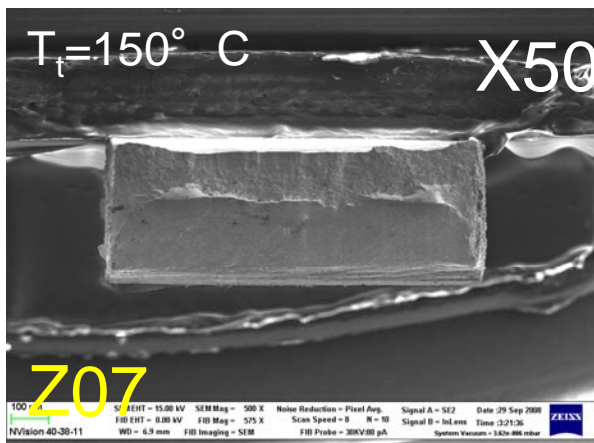


Result – Pt alloys (95Pt-5Au)

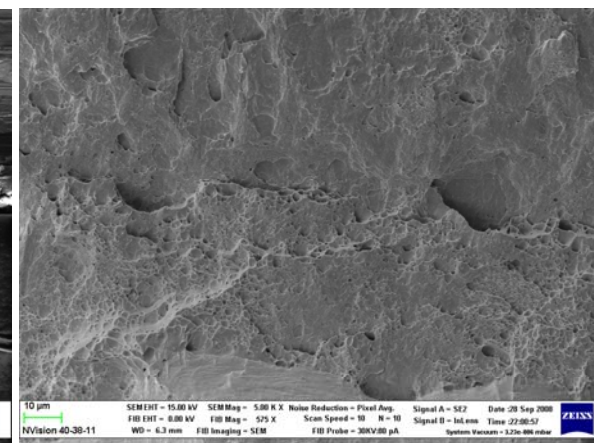
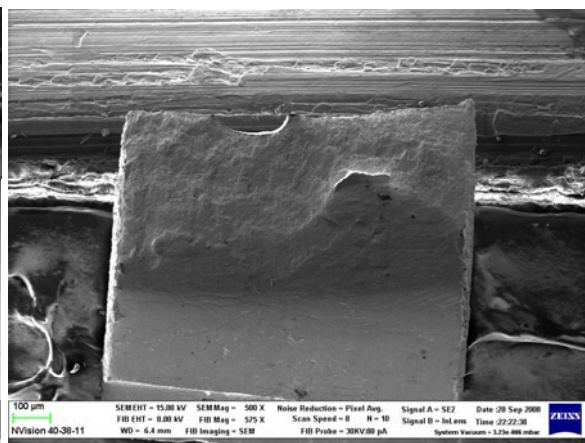
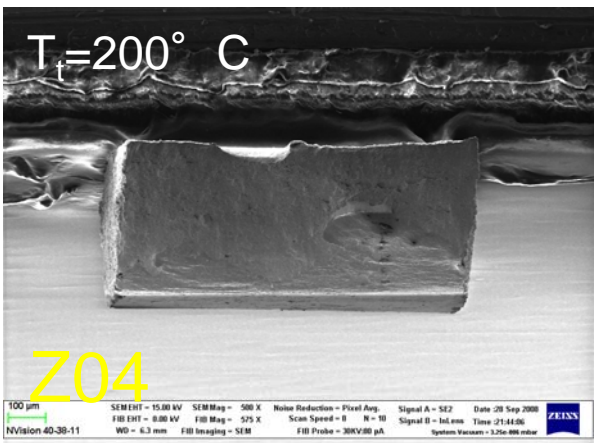
◆ After irradiation



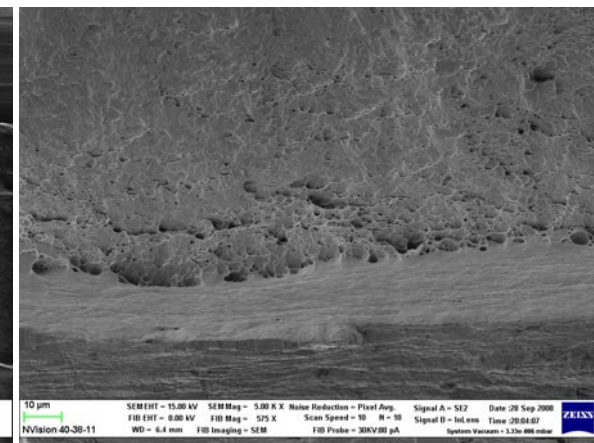
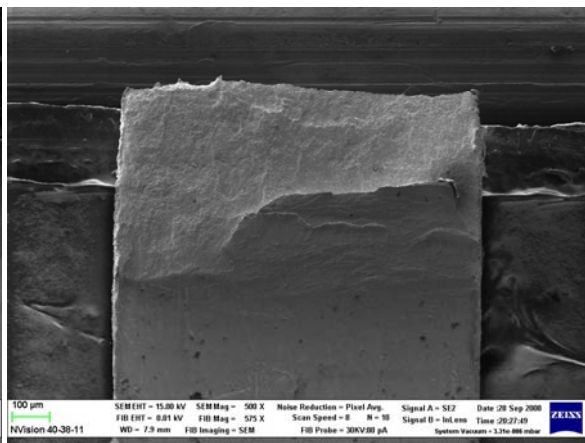
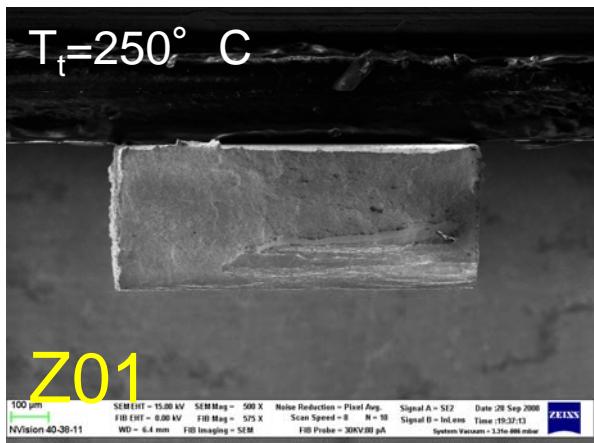
$T_i=196^\circ\text{C}$
(10.8dpa)



$T_i=261^\circ\text{C}$
(15.2dpa)



$T_i=360^\circ\text{C}$
(18.9dpa)



- ◆ Tensile tests and fracture surface investigation were performed on **Au and Pt alloys** irradiated on STIP-II in order to know design data of mechanical properties on these
- ◆ Au alloy (75Au-9Ag-16Cu) showed good tensile strength and elongation before proton irradiation
- ◆ Significant ductility loss occurred after irradiation
- ◆ Only samples tested at **150° C (Y06)** and **200° C (Y02)** showed significant loose of strength, which is more like **embrittlement**
- ◆ The sample irradiated **above 200° C (Y03, T_t=RT)** shows rather ductile fracture surface
- ◆ May be due to the **gases (He, H) introduce by irradiation**
- ◆ **Pt alloy (95Pt-5Au)** showed rather unique deformation, which is kind of one side slip deformation
- ◆ **No significant deformation features were observed after irradiations for Pt alloys except for the UTS increase of about 200MPa**

Spallation neutron source for ADS

- MEGAPIE project in cooperation with PSI, ESS(CNRS, CEA, ENEA, FZ, SCK-CEN), JAERI, LANL, KAERI.
- Materials issues for the beam window, protons/LBE.
- In-situ test at LiSoR, 72MeV-P, flowing LBE and stress
- MEGAPIE run in 2006.8-12, at 0.75MW.
- MEGAPIE target samples will ship this year/2009.
- MIRRAH / SCK-CEN plans XADS (EU)
- PSI plans power-up in neutron flux in LIMETS.
- J-PARC Phase-II plans experiment facility for ADS.

the MEGAPIE target



final assembly



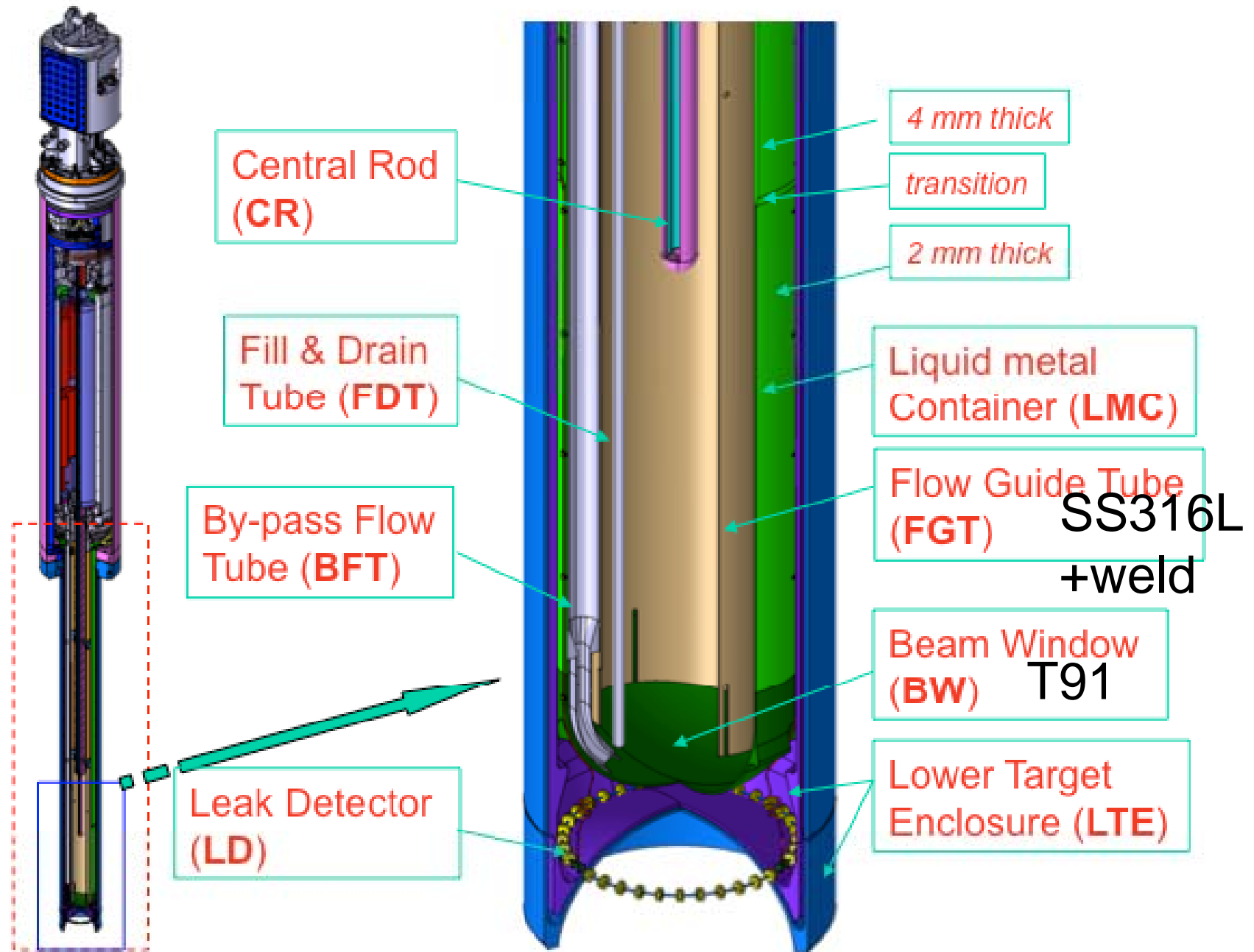
inserting the target into SINGO
with the exchange flask



LEAK detector:
best view



MEGAPIE LBE target, 600MeV, 1.2mA / PSI



Dai, PSI

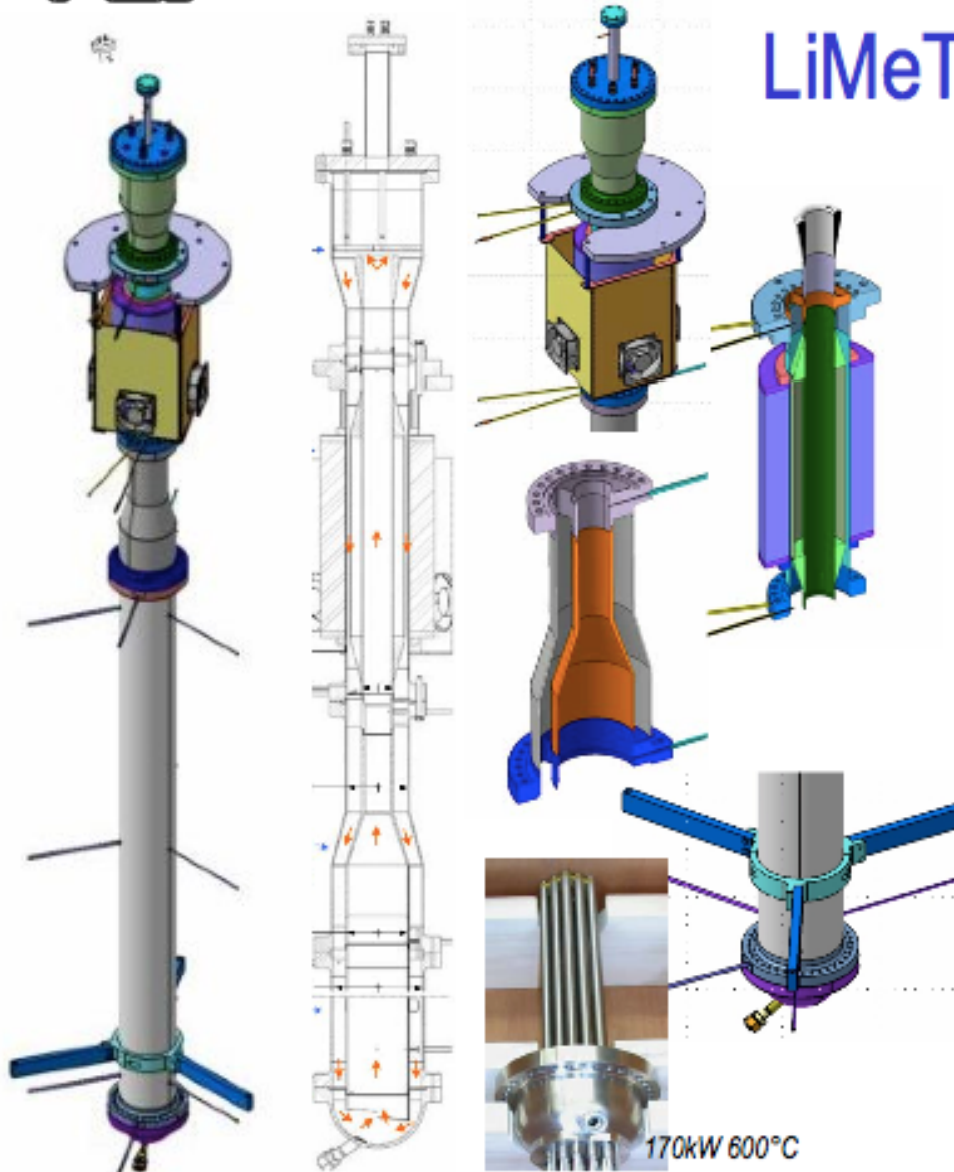
The GOALS of LIMETS

Liquid Metal Target for routine operation at SINQ

which must (should) be

- safe
- robust
- easy to operate
- simple & reliable
- efficient
- interesting to a wider community
- cheaper than MEGAPIE

LiMeTS mock-up design (stage 1)

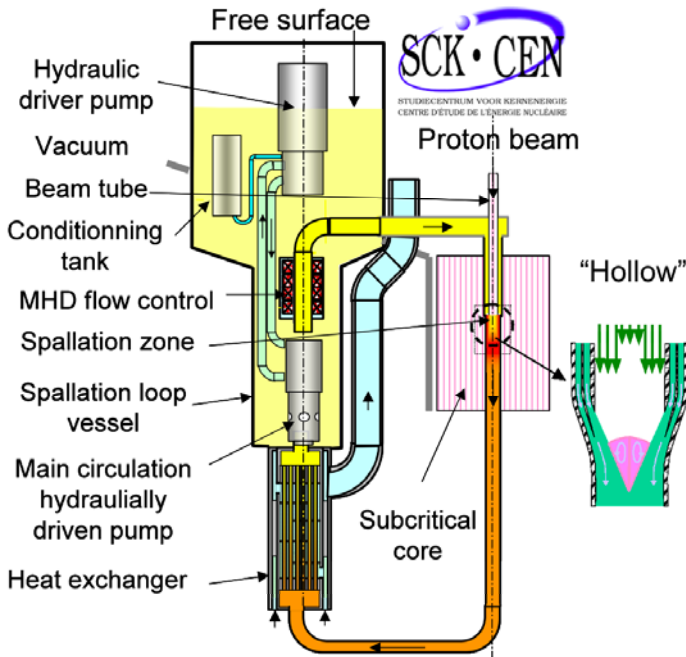


Basic technical parameters:

- ▶ **Modular design** allowing testing of different concepts of the THX, EMP, BEW
- ▶ Existing EMP (prototype of EMP1 for MEGAPIE) is adopted for the mock-up
- ▶ – **Working fluid PbBi** eutectic (melting temp. 126°C) **or Pb** (327°C), volume 65 l
- ▶ Maximum operating temperature – **500°C**
- ▶ **Liquid metal flowrate**, nominal – 4 l/s
- ▶ Design pressure – 10 bar
- ▶ extensive **instrumentation** (temp., pressure, flow)
- ▶ **Electric heater** – 170 kW (former MEGAPIE test heater)

MYRRHA spallation target LBE loop

2.2 mA at 600 MeV

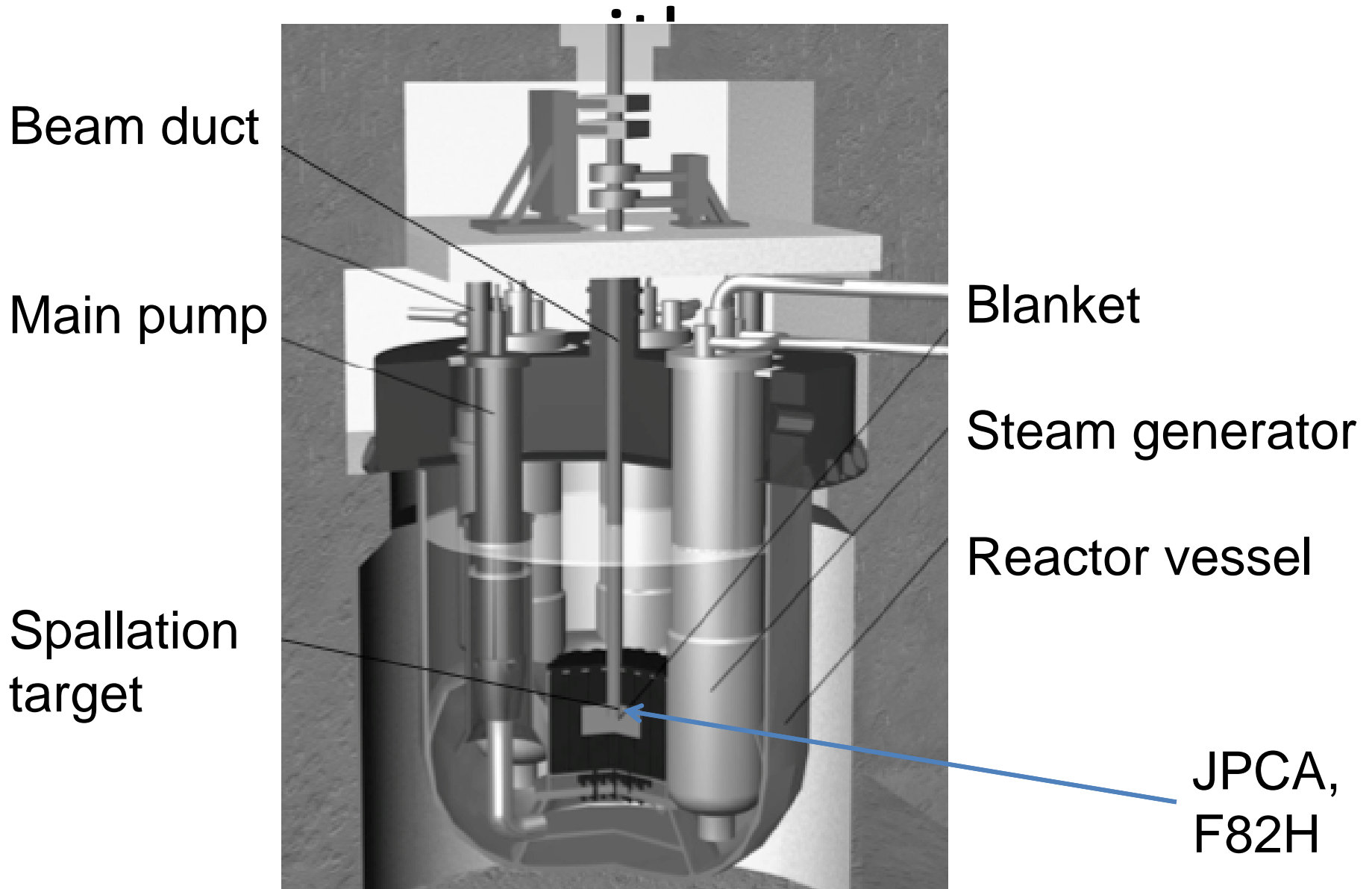


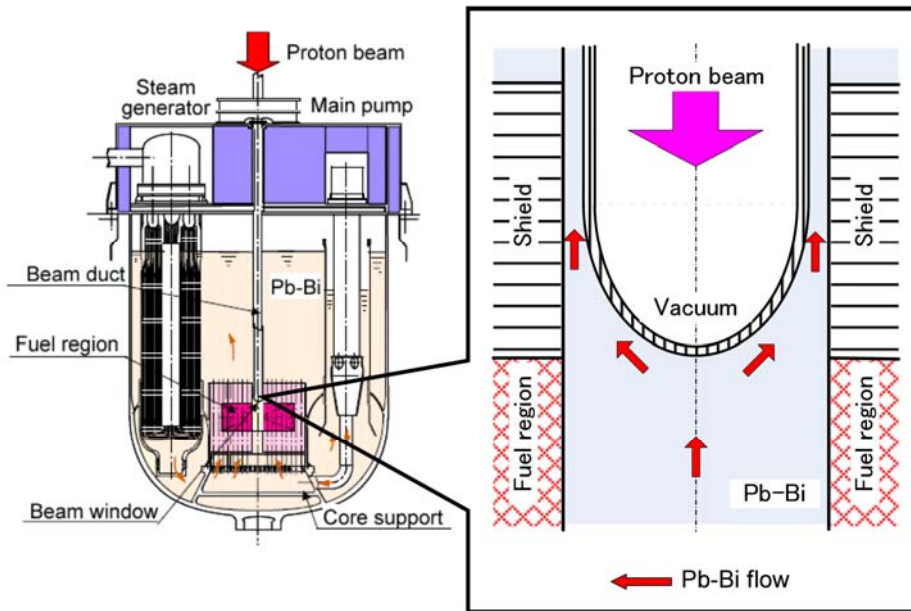
1. inner vessel
 2. guard vessel
 3. cooling tubes
 4. cover
 5. diaphragm
 6. spallation loop
 7. sub-critical core
 8. primary pumps
 9. primary heat exchangers
 10. emergency heat exchangers
 11. in-vessel fuel transfer machine
 12. in-vessel fuel storage
 13. coolant conditioning system
- 316L
- T91



Bosch SCK·CEN

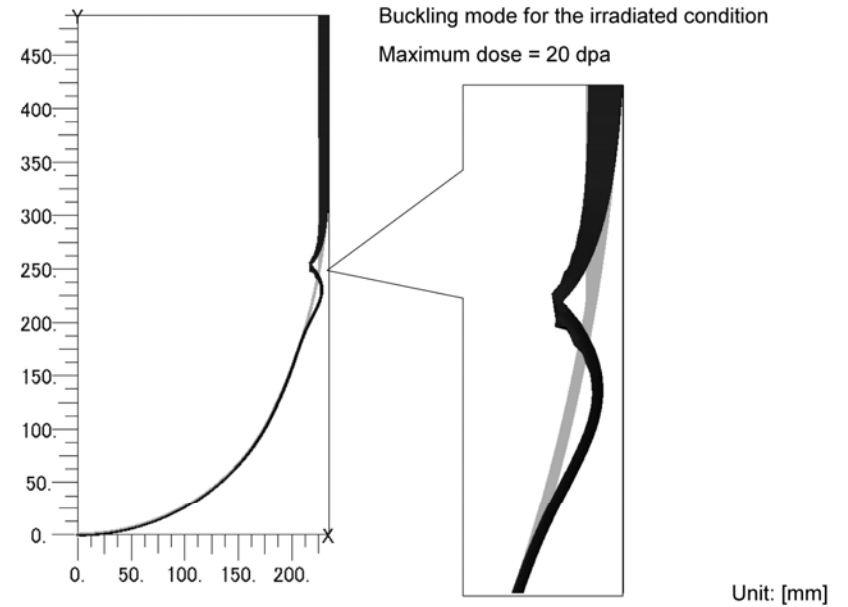
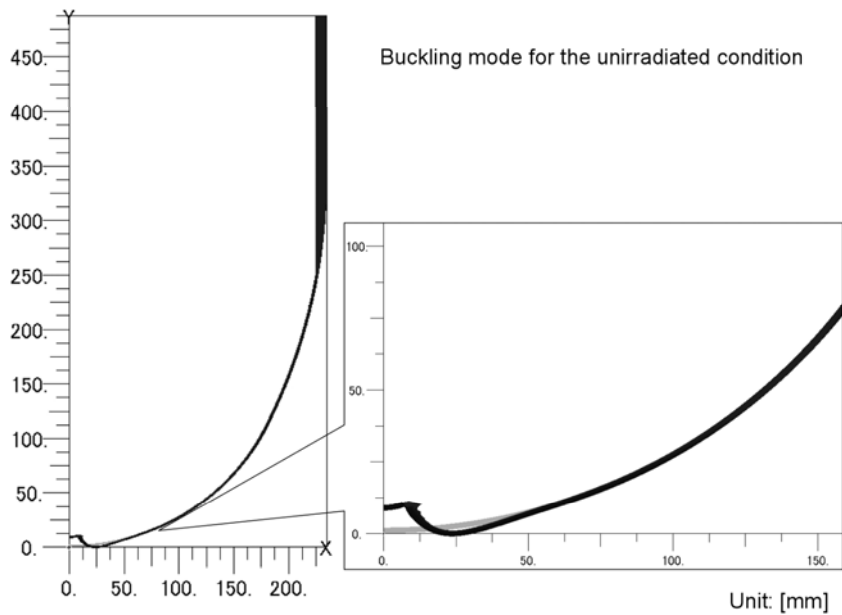
Image of ADS with window



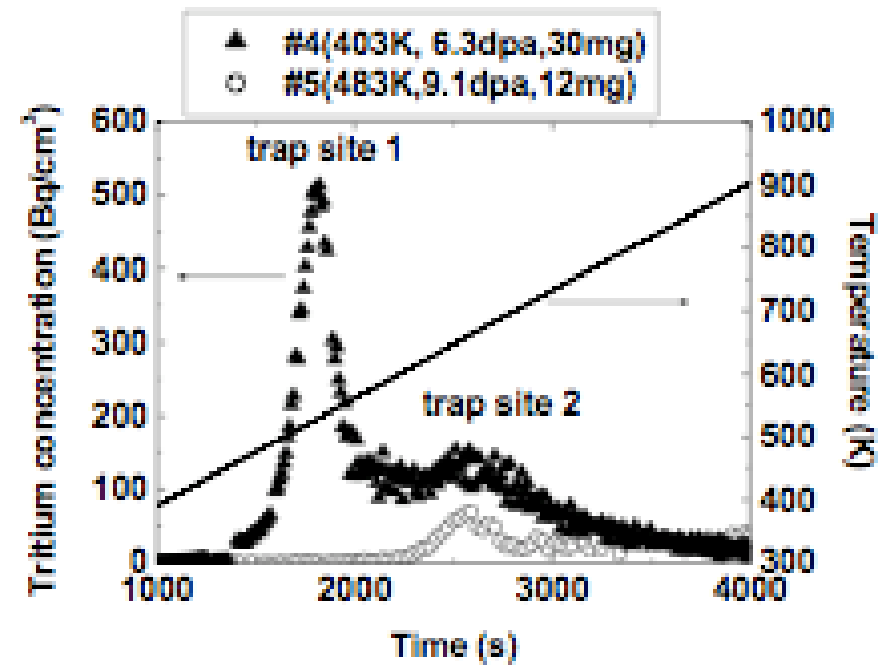
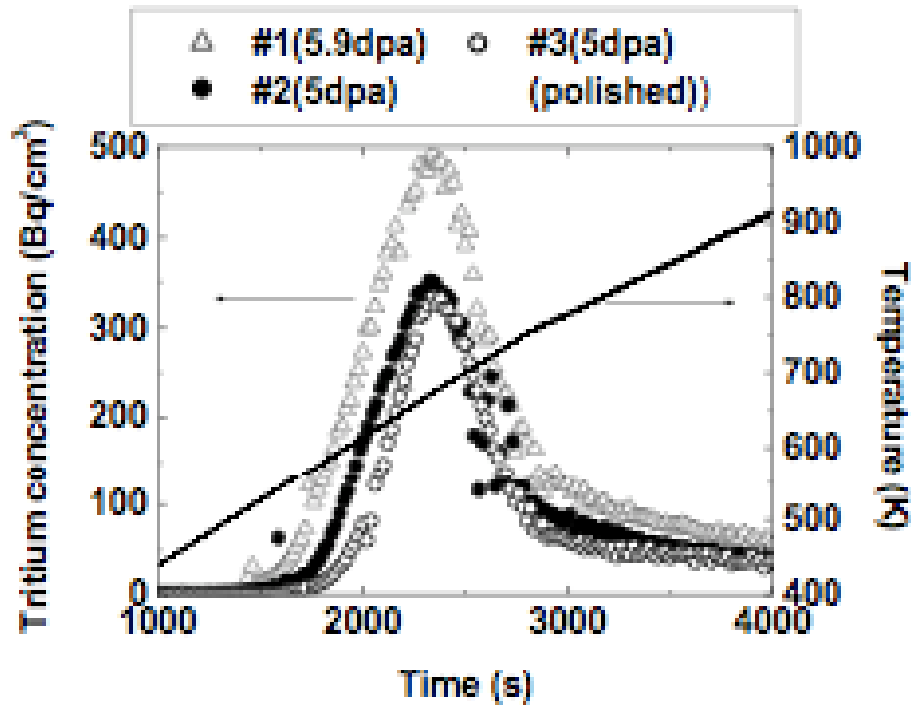


Buckling mode of the beam window

Sugawara et al. NUMA

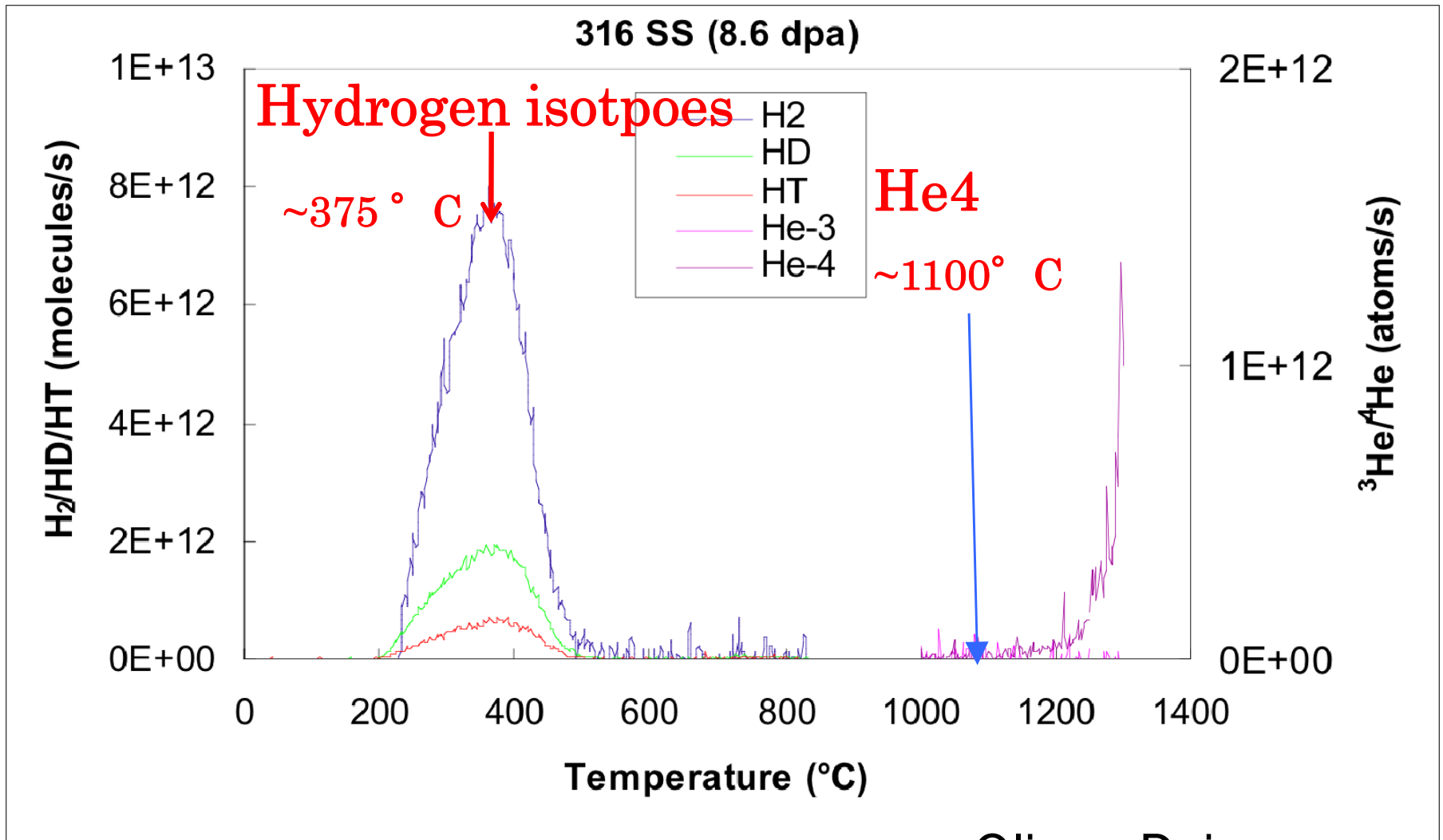


T releases from SS316(L) and F82H(R) by TDS method



SS316 showed peak and F82 showed two peaks in release curves.

Thermal desorption behavior of light gases from STIP samples



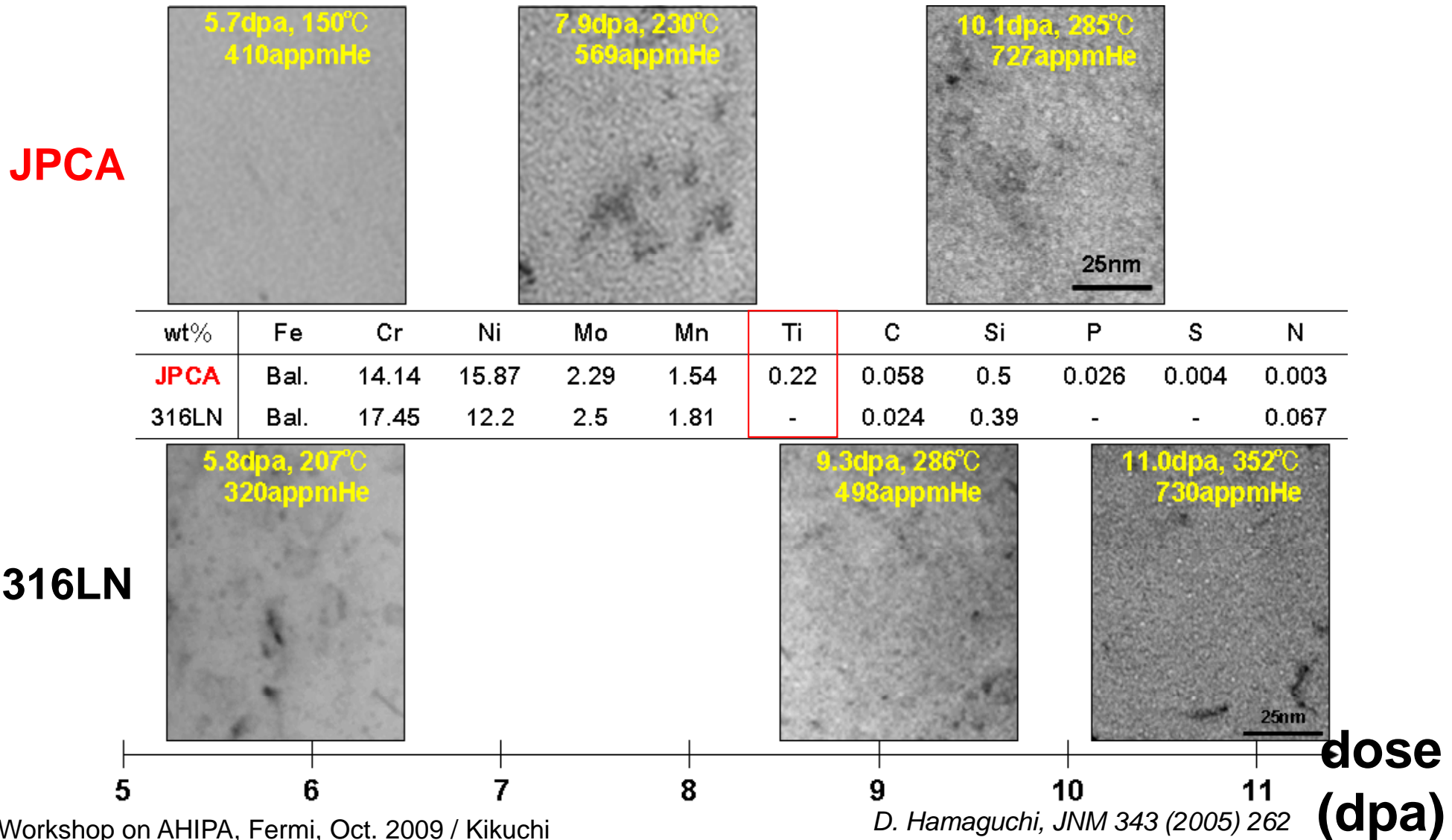
Oliver, Dai,
IWSMT7

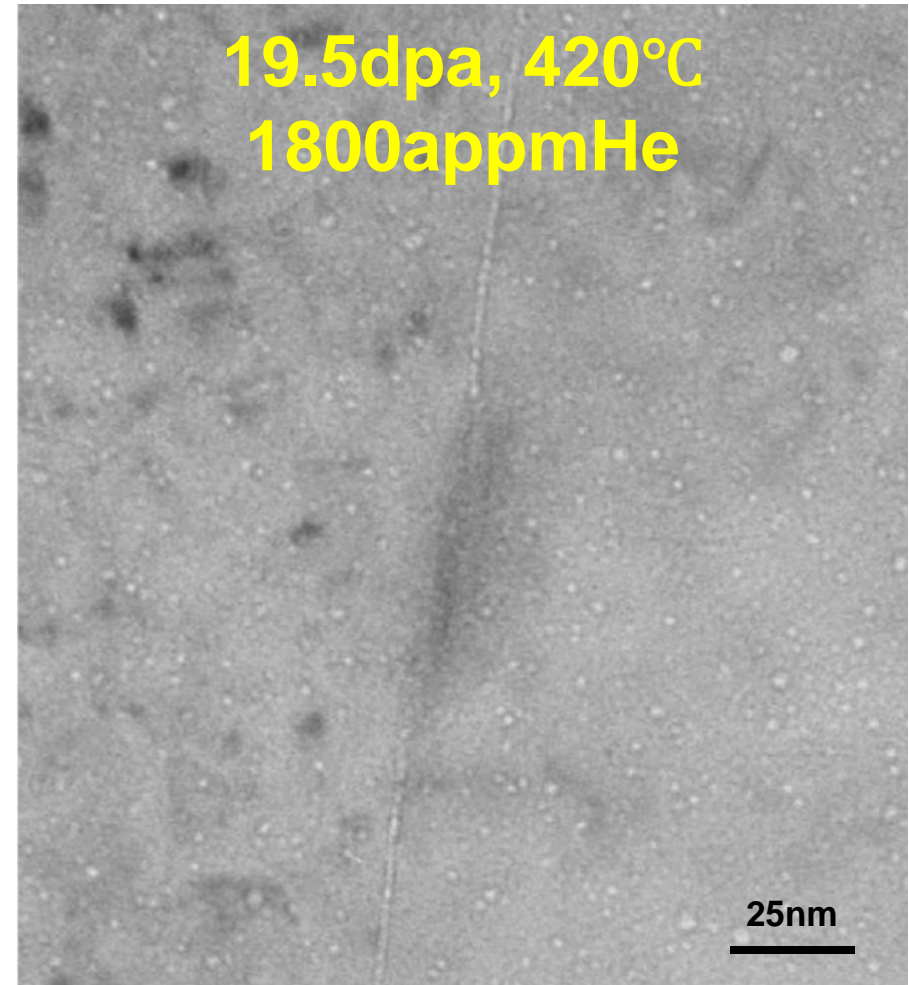
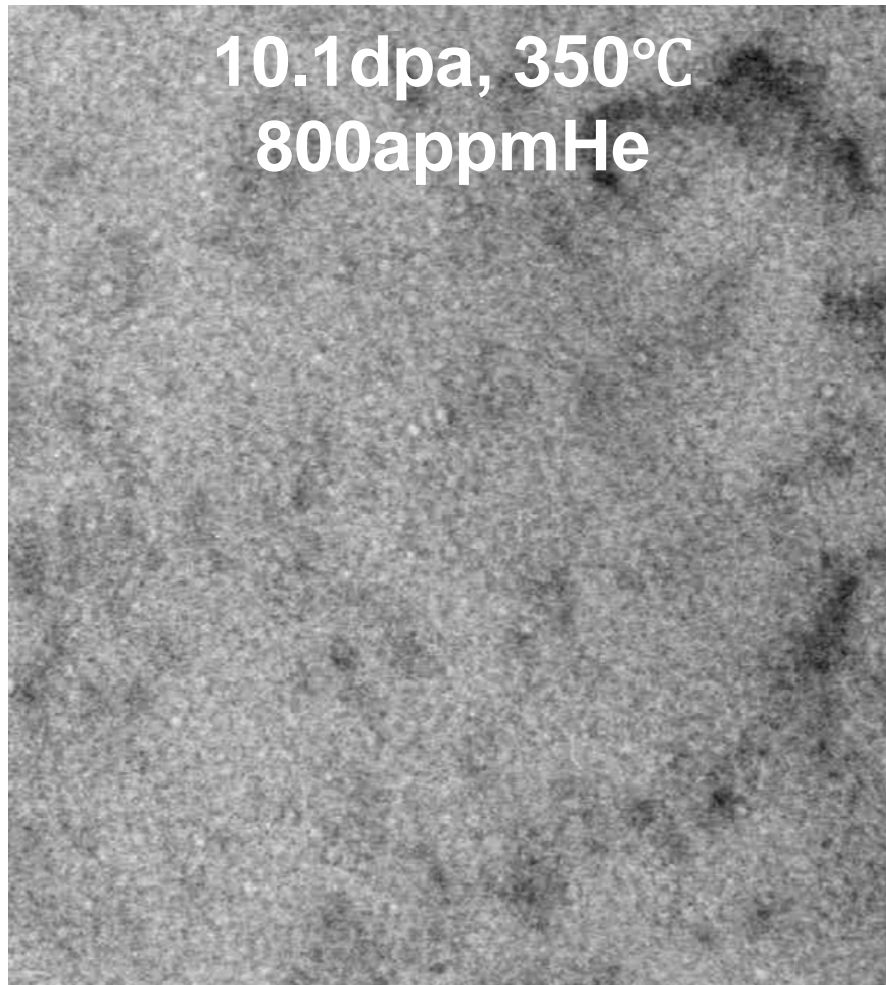
Irradiation Damage on the window in the 800MWth ADS after 300 FPDs

Nishihara, Kikuchi, NUMA 2008

Particle		<i>I</i>	<i>P</i>	<i>N</i>	<i>C</i>	Total
Flux (/cm ² /s)		7.57E+13	5.53E+12	8.28E+13	4.32E+15	4.49E+15
Averaged energy (MeV)		1500	107	42	0.75	
Cross section (b)	Heat (MeV b)	224	1010	6.4	1.1	
	DPA	2155	2148	1697	419	
	¹ H	1.59	12.78	0.338	4.5E-3	
	² H	0.37	0.013	3.3E-3	7.3E-7	
	³ H	0.083	1.9E-3	3.4E-4	4.9E-7	
	³ He	0.066	1.4E-3	1.3E-4	3.5E-11	
	⁴ He	0.36	0.039	0.021	5.8E-4	
Reaction	Heat (W/cm ³)	229	75	7.2	63	375
	DPA (300 FPDs)	4.2	0.31	3.6	47	55
	¹ H (appm,300 FPDs)	3119	1831	725	503	6179
	² H (appm,300 FPDs)	727	1.8	7.2	0.082	736
	³ H (appm,300 FPDs)	163	0.27	0.72	0.054	164
	³ He (appm,300 FPDs)	130	0.20	0.28	3.9E-6	130
	⁴ He (appm,300 FPDs)	709	5.5	45	65	825

- ◆ He bubble formation on JPCA was observed at lower temperature compared to EC316LN on STIP-I irradiated samples
- ◆ Effect of Ti modification?
- ◆ **Ti as an over sized atom lowers the mobility of vacancies**





- ◆ In the sample irradiated to 19.5 dpa to 450°C, some bubble agglomeration to boundaries is observed
- ◆ Agglomeration was not observed on the sample irradiated to 10.1 dpa, 350°C
- ◆ Any influence on mechanical properties ?

DBTT shift of F/M steels

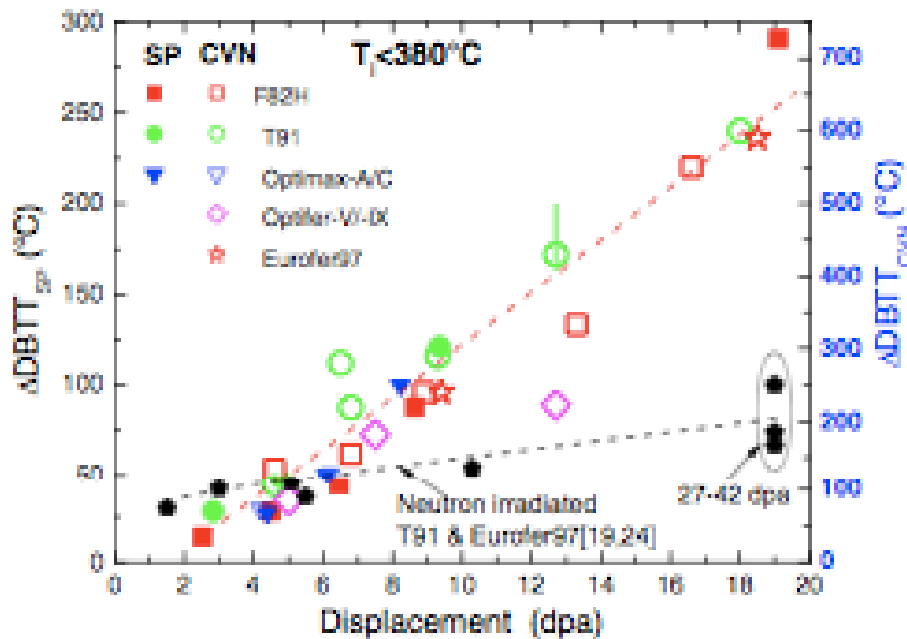


Fig. 5. DBTT shift as a function of irradiation dose for different FM steels irradiated in STIP.

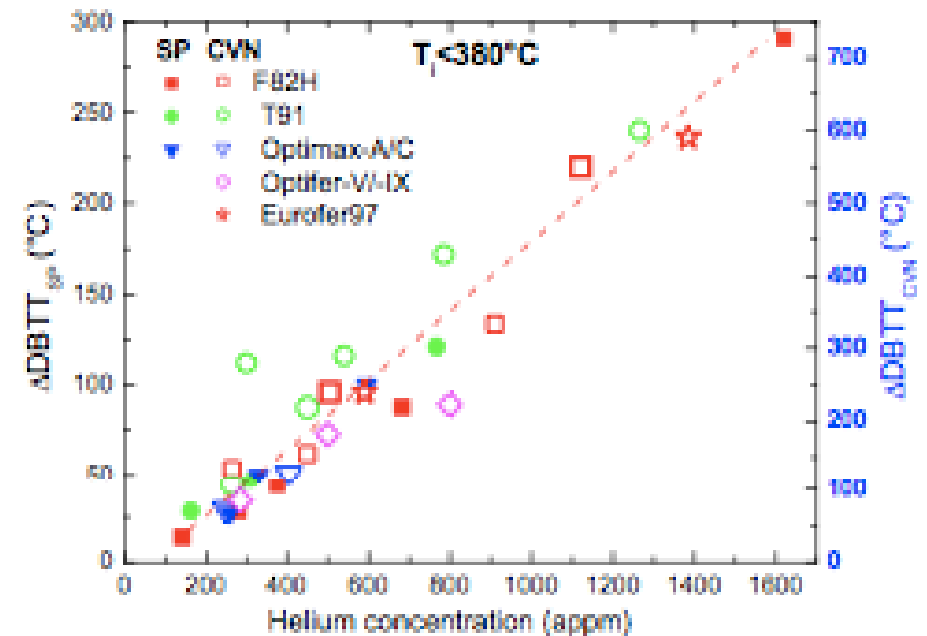


Fig. 6. DBTT shift as a function of helium concentration for both the previous small punch tests [17] and the present Charpy tests.

Dai and Wagner, NUMA

Topics of material issues

- Spallation neutron source design needed proton irradiation data
- IWSMT1、1996、ORNL
- STIP started in PSI、1997
- Pressure wave and neutronic test were done at AGS/BNL, 24GeV, 1997
- Ductility remains in Ta spent target at ISIS, 8dpa
- Ductility loss in SS316L irradiated by proton at LANL, 4-5dpa
- Pitting found in Hg container for short pulse source
- Life time of Hg container is decided by pitting damage > irradiation damage
- Guideline for exchange is 5dpa in Hg target vessel

continued

- Modified SS316, JPCA, kept ductility up to 12dpa, AccApp03
- Compressive test of W LANSCE spent target shows no collapse
- STIP-III data for 19dpa stainless steels remains ductility and no intergranular fracture
- ORNL-SNS decided extension of life to 10 dpa at IWSMT9
- Consideration of weight balance in pitting and irradiation under full power
- A short pulsed target issue needs to deal with high intensity and neutron flux
- Solid target approach for high intensity power at CSNS, SNS-T2, ESS-BIBAO?
- LANL evaluation on W erosion