

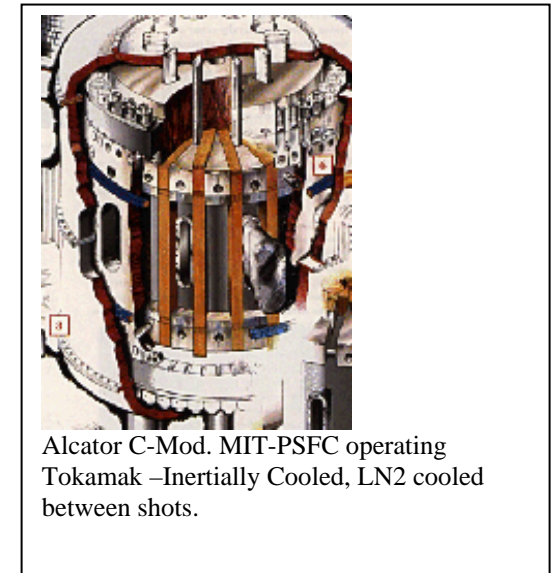
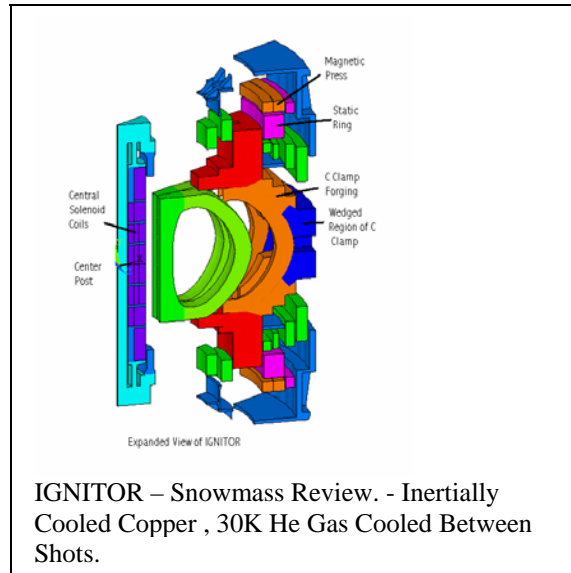
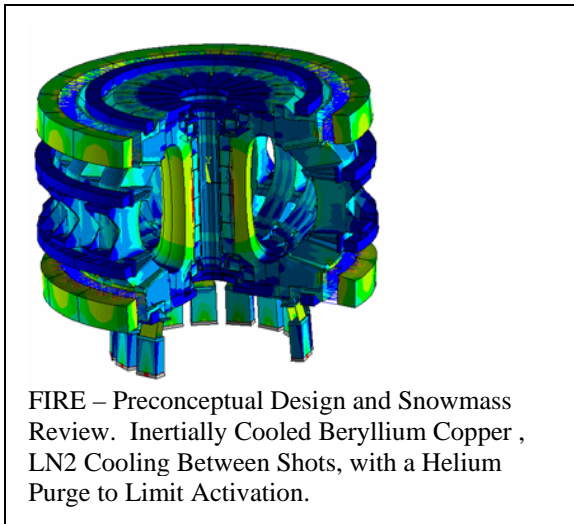
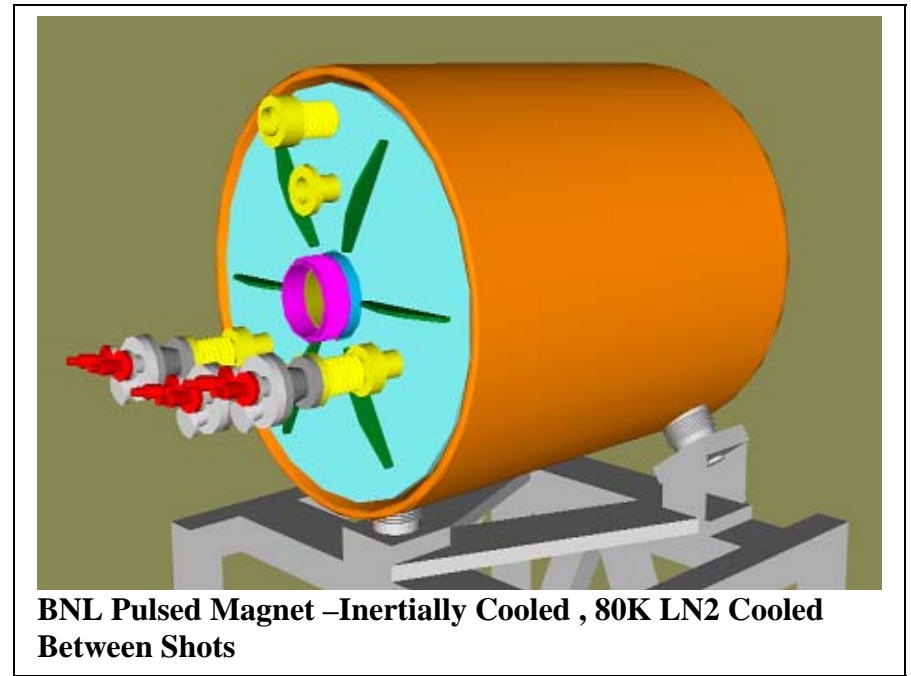
MC Collaboration Meeting
February 14 - 17, 2005
LBL Berkeley, California
nTOF11 15-T Pulsed Magnet for
Mercury Target Development
Neutrino Factory and Muon Collider
Collaboration
Peter H. Titus



MIT Plasma Science and Fusion Center
 (617) 253 1344, titus@psfc.mit.edu,
<http://www.psfc.mit.edu/people/titus>

With Contributions from CVIP, Dave Rakos of Everson, and Bob Weggel

BNL pulsed magnet design builds off of copper magnet experience in fusion research:



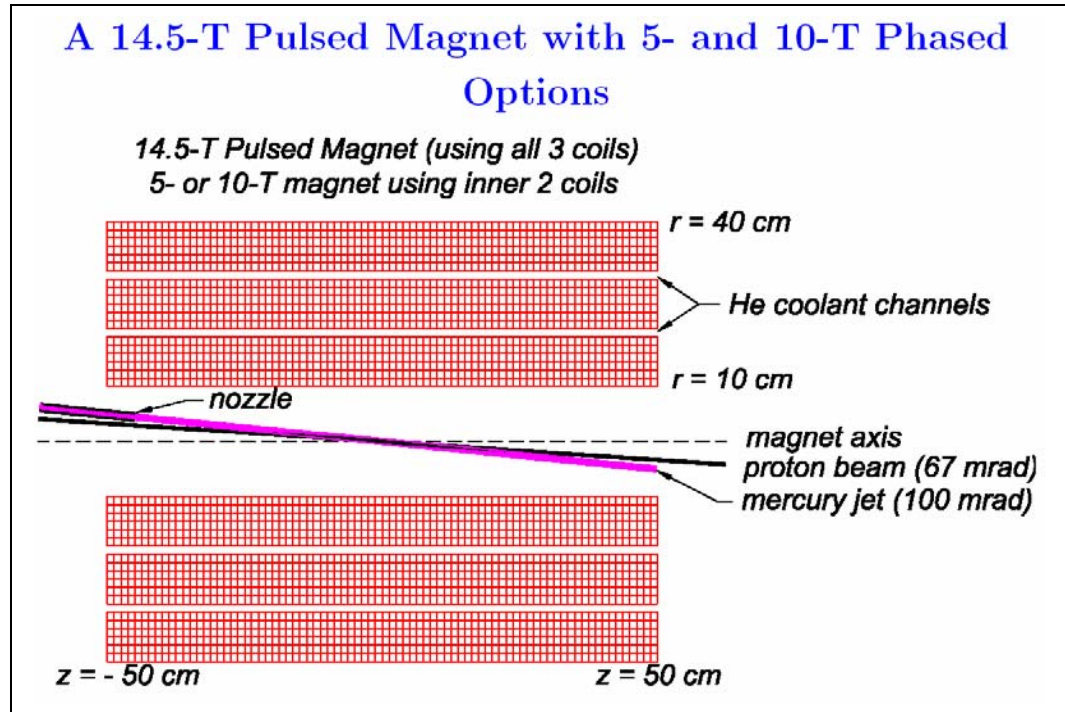
Cost issues dictated a modest coil design.

Power supply limitations dictate a compact, low inductance, high packing fraction design.

A three segment, layer wound solenoid is used for the pulsed magnet. External segment leads allow series and parallel connections.

The conductor is half inch square, cold worked OFHC copper.

The coil is inertially cooled with options for liquid nitrogen or gaseous Helium cooling between shots. Coolant flows through axial channels in the coil.



**Draft Test plan, Pictures, Drawings and Calculations at:
<http://www.psfc.mit.edu/people/titus/#BNL%20Memos>**

Bob Weggel performed the coil/power supply simulations. He has picked operating temperatures, and basic coil build.

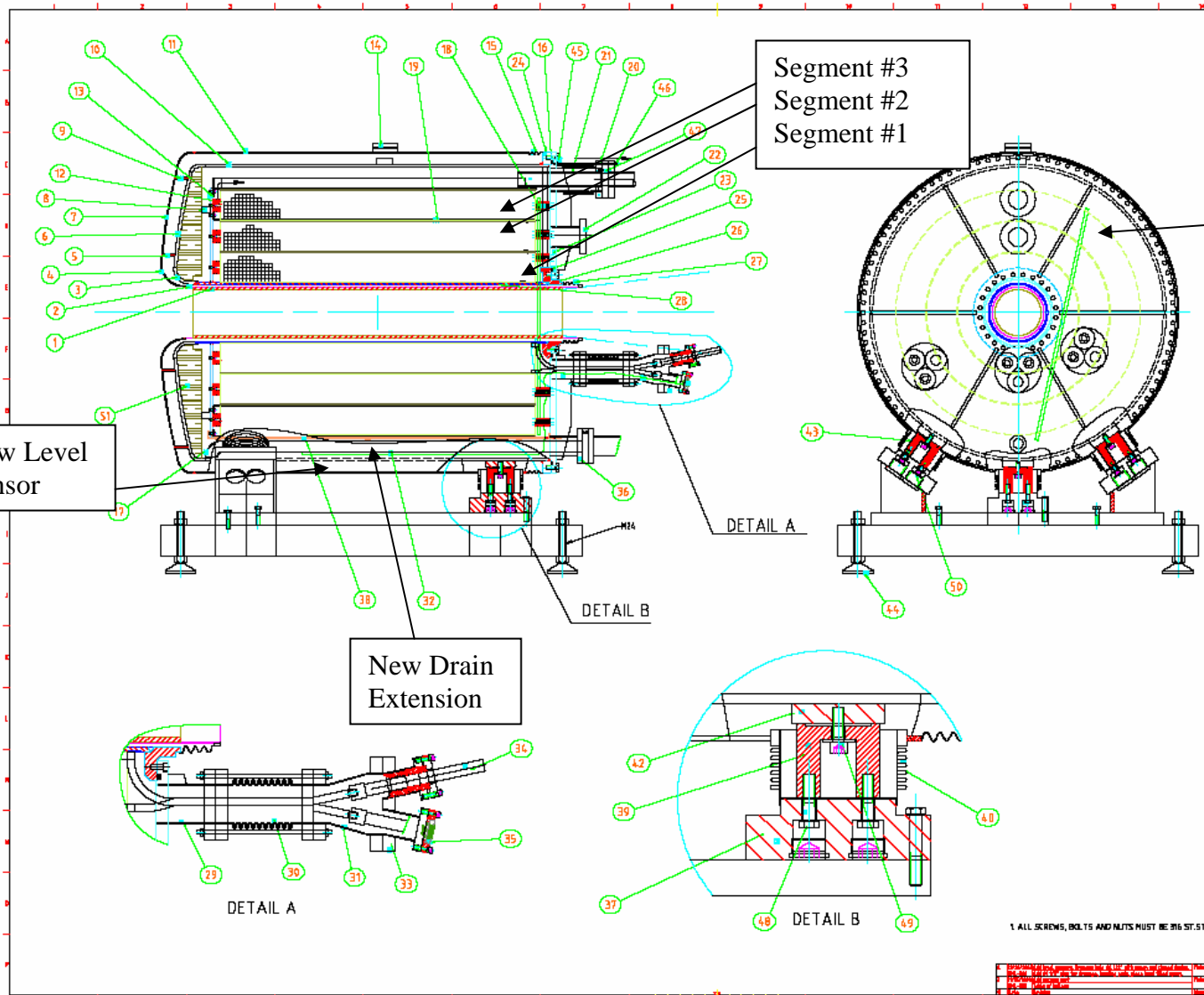


New Level Sensor

Segment #3
Segment #2
Segment #1

New Level Sensor

New Drain Extension



Item	Location	Quantity	Part Name	Material	Notes
1	Top	1	Cap Screw	304	
2	Top	1	Cap Screw	304	
3	Top	1	Cap Screw	304	
4	Top	1	Cap Screw	304	
5	Top	1	Cap Screw	304	
6	Top	1	Cap Screw	304	
7	Top	1	Cap Screw	304	
8	Top	1	Cap Screw	304	
9	Top	1	Cap Screw	304	
10	Top	1	Cap Screw	304	
11	Top	1	Cap Screw	304	
12	Top	1	Cap Screw	304	
13	Top	1	Cap Screw	304	
14	Top	1	Cap Screw	304	
15	Top	1	Cap Screw	304	
16	Top	1	Cap Screw	304	
17	Top	1	Cap Screw	304	
18	Top	1	Cap Screw	304	
19	Top	1	Cap Screw	304	
20	Top	1	Cap Screw	304	
21	Top	1	Cap Screw	304	
22	Top	1	Cap Screw	304	
23	Top	1	Cap Screw	304	
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25	Top	1	Cap Screw	304	
26	Top	1	Cap Screw	304	
27	Top	1	Cap Screw	304	
28	Top	1	Cap Screw	304	
29	Detail A	1	Cap Screw	304	
30	Detail A	1	Cap Screw	304	
31	Detail A	1	Cap Screw	304	
32	Detail A	1	Cap Screw	304	
33	Detail A	1	Cap Screw	304	
34	Detail A	1	Cap Screw	304	
35	Detail A	1	Cap Screw	304	
36	Detail A	1	Cap Screw	304	
37	Detail B	1	Cap Screw	304	
38	Detail B	1	Cap Screw	304	
39	Detail B	1	Cap Screw	304	
40	Detail B	1	Cap Screw	304	
41	Detail B	1	Cap Screw	304	
42	Detail B	1	Cap Screw	304	
43	Top View	1	Cap Screw	304	
44	Top View	1	Cap Screw	304	
45	Top View	1	Cap Screw	304	
46	Top View	1	Cap Screw	304	

Item	Location	Quantity	Part Name	Material	Notes
34	Detail A	1	Cap Screw	304	
35	Detail A	1	Cap Screw	304	
36	Detail A	1	Cap Screw	304	
37	Detail B	1	Cap Screw	304	
38	Detail B	1	Cap Screw	304	
39	Detail B	1	Cap Screw	304	
40	Detail B	1	Cap Screw	304	
41	Detail B	1	Cap Screw	304	
42	Detail B	1	Cap Screw	304	
43	Top View	1	Cap Screw	304	
44	Top View	1	Cap Screw	304	
45	Top View	1	Cap Screw	304	
46	Top View	1	Cap Screw	304	

1. ALL SCREWS, BOLTS AND NUTS MUST BE 316 ST. ST.

Item	Location	Quantity	Part Name	Material	Notes
47	Top View	1	Cap Screw	304	
48	Top View	1	Cap Screw	304	
49	Top View	1	Cap Screw	304	
50	Top View	1	Cap Screw	304	

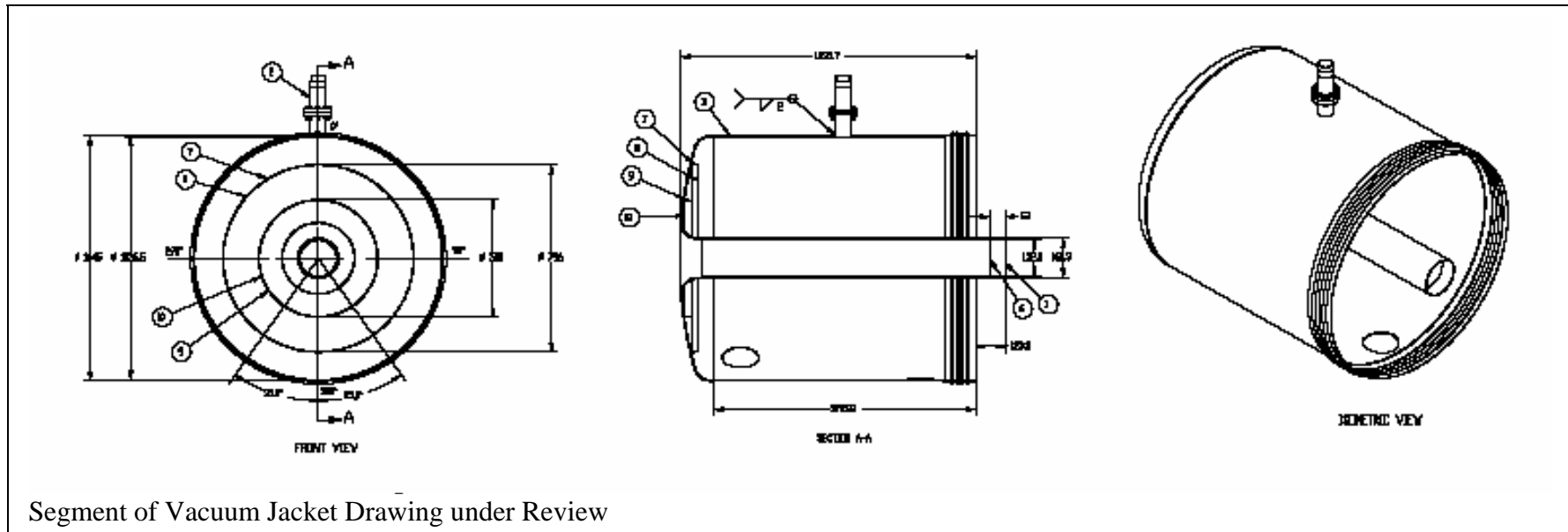
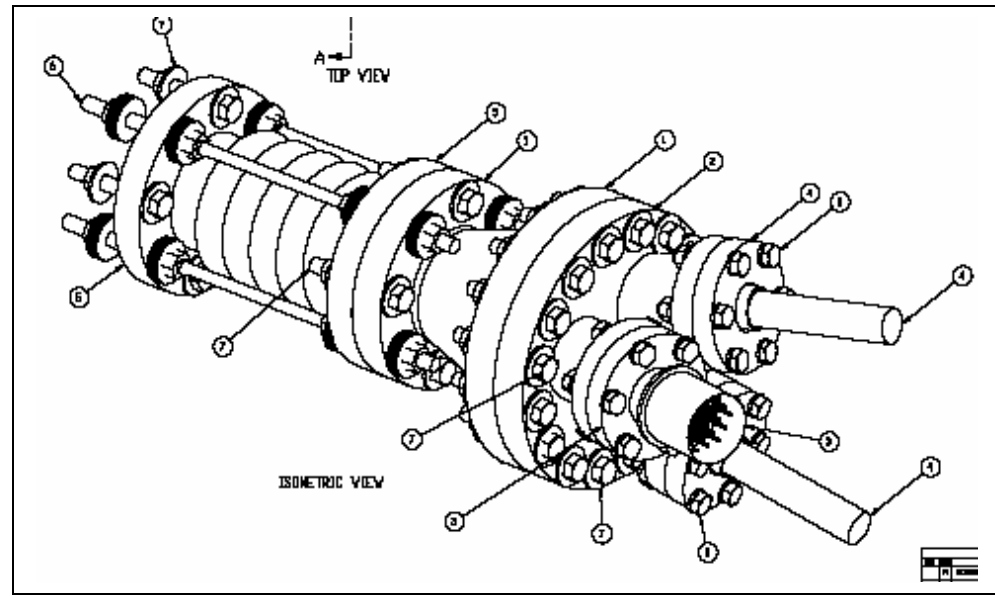
PSFC/MIT
BNL IS T PIA BED MAGNET
ASSEMBLY AND
BILL OF MATERIALS
BNL-602

Status of Vessel Drawing Submittal by CVIP

Inner Vessel drawings complete and all approved.
Outer vessel drawings Complete and approved
Final manufacturing procedure is approved, but there are some additions.

Major dished heads have been manufactured and delivered to CVIP. Large cover has been partially machined.

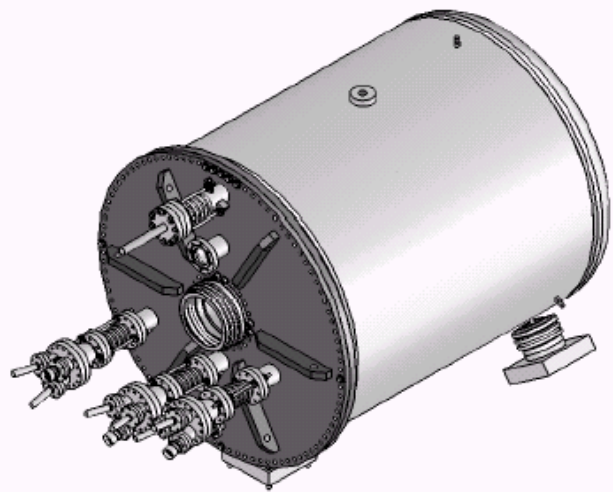
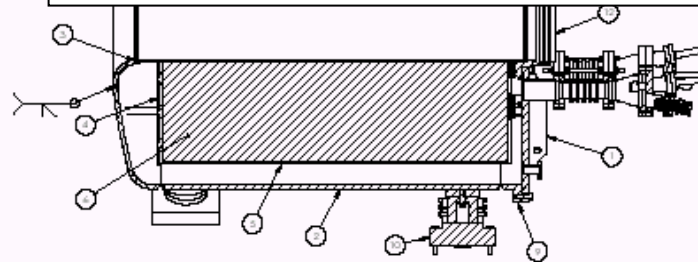
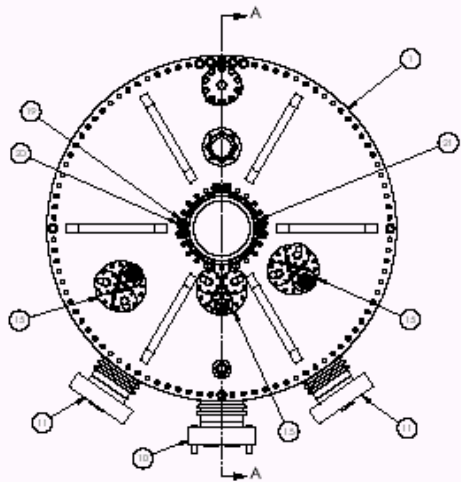
Change Order Items Not yet Submitted to CVIP



CVIP Drawings - Continued

Experimental Volume Spec:

150 mm bore , 1200mm long centered on the magnetic center of the solenoid, with 7 degree conical exclusion zones at either end. This has been expanded to the CVIP as-specified bore tube ID – Removing the G-10 liner. New Geometry has been supplied to ORNL



SECTION A-A
SCALE 1:4

ITEM NO.	QTY	PART NUMBER	MATERIAL	DESCRIPTION
1	1	04021005A	STAINLESS STEEL 316L/316L	CLOSURE COVER PLATE ASSEMBLY
2	1	04021000A	STAINLESS STEEL 316L/316L	HE PRESSURE VESSEL SHELL
3	1	040210001	STAINLESS STEEL 316L/316L	SPLINE SHAFT
4	1	04021005A	STAINLESS STEEL 316L/316L	PLENUM PLATE ASSEMBLY
5	1	040210017	STAINLESS STEEL 304/304L	SHROUD FOR 3rd MAGNET
6	1	MAGNET		
7	1	04021005A	STAINLESS STEEL 304/304L	HEATN OUTLET TUBE ASSEMBLY
8	1	04021005A	STAINLESS STEEL 304/304L	HEATN OUTLET BELLOW ASSEMBLY
9	1	040210001	STAINLESS STEEL 316L/316L	PRESSURE VESSEL MATING FLANGE
10	1	0402300A	STAINLESS STEEL 304/304L G-10	FRONT SUPPORT ASSEMBLY
11	2	0402301A	STAINLESS STEEL 304/304L G-10	SIDE SUPPORT ASSEMBLY
12	1	040210005	STAINLESS STEEL 316L/316L	INNER BELLOW
13	1	040210005	STAINLESS STEEL 304/304L	PRESSURE VESSEL F-HEAD PAD
14	1	04021015A	STAINLESS STEEL 316L/316L	PRESSURE VESSEL COIL ASSEMBLY
15	3	0402300A	STAINLESS STEEL 316L/316L	JOINT PENETRATION ASSEMBLY
16	3	0402004A	STAINLESS STEEL 304/304L G-10	SPACER SUPPORT ASSEMBLY
17	96	HEX CAP SCREWS	STAINLESS STEEL 316L/316L	HEX CAP SCREWS, M12 x 1.75 x 40
18	96	WASHER	STAINLESS STEEL 316L/316L	1/2" SCREW SIZE, 1.25" O.D. x .25" ID x .042 THK
19	36	WASHER	STAINLESS STEEL 316L/316L	1/2" SCREW SIZE, .25" O.D. x .25" ID x .029 THK
20	36	SOCKET HEX CAP SCREW	STAINLESS STEEL 316L/316L	SOCKET HEX CAP SCREW, M12 x 1.75 x 35
21	1	040210011	STAINLESS STEEL 316L/316L	INNER FLANGE

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CASTER
 874 15 T PULSED MAGNET PRESSURE VESSEL ASSEMBLY AND BILL OF MATERIAL
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 TOTAL SHEETS 1 SHEET 1 OF 1

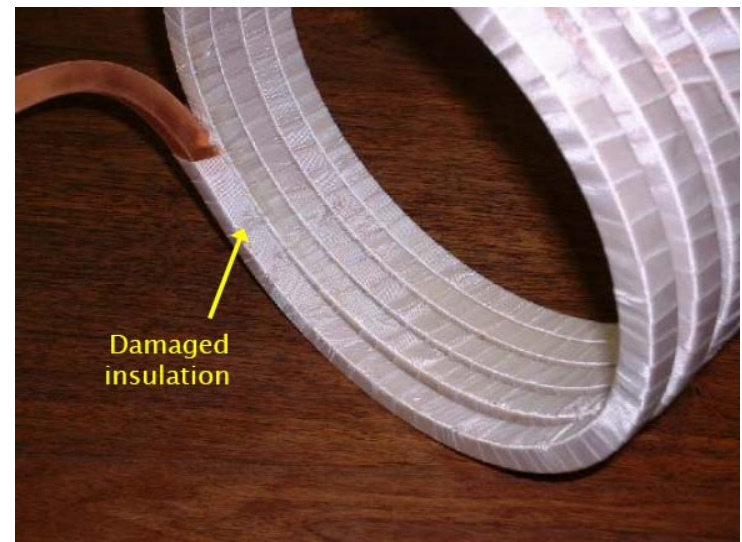
Fabrication Status



Everson autoclave (Box with Doors) Epoxy pumping equipment, and vacuum pumps) – Used for all three coil segments



Winding Machine with the beginnings of segment #1



Results of the test bend. Roller geometry was improved to avoid fiberglass tape cuts.

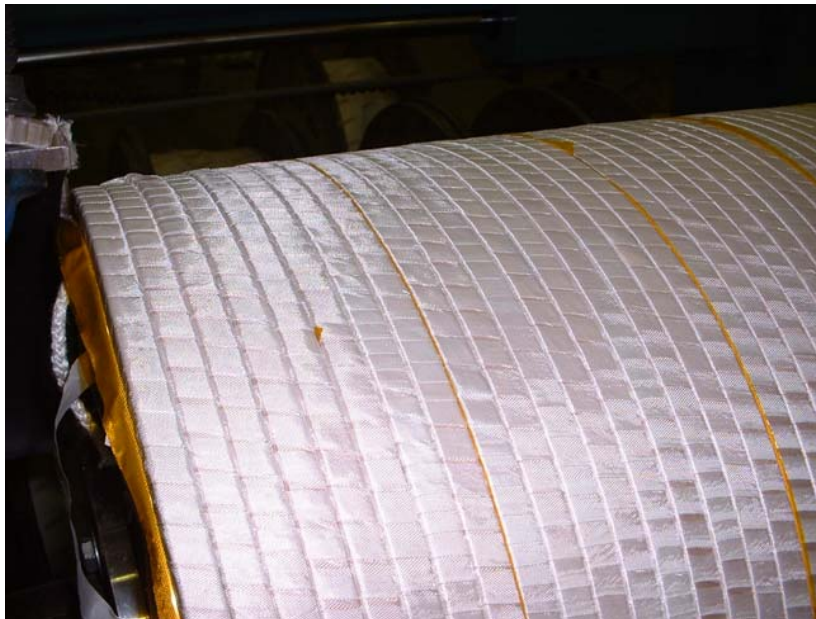
Segment #1

As of Thursday January 27th :



Kapton arc sections inserted between every eighth turn on those layers that face the cooling channels

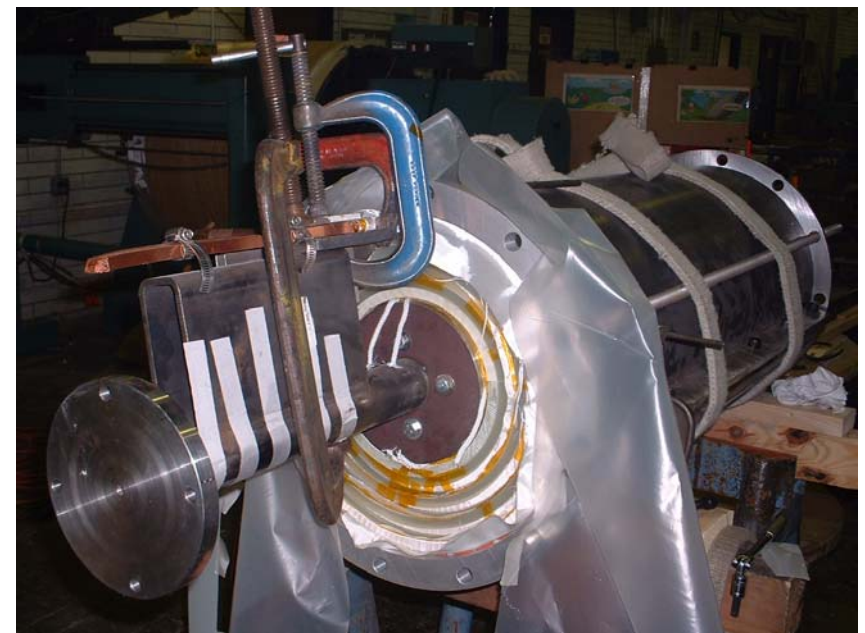
The inner segment (Segment #1) has been impregnated at Everson and has been sent out for final machining of the OD. – This will be the first test on machinability of the outer rib geometry



Segment #1 being wound. Photo taken by Dave Rakos at Everson 09-08-04. Kapton layer spaced at every eighth turn relieves axial tension in the layers near the cooling channels. First Layer, Coil Segment#2



Coil Mold for Segment #1. Successfully used for its impregnation



Segment 1 showing formed leads and portions of the mold

Segment #1 – Continued

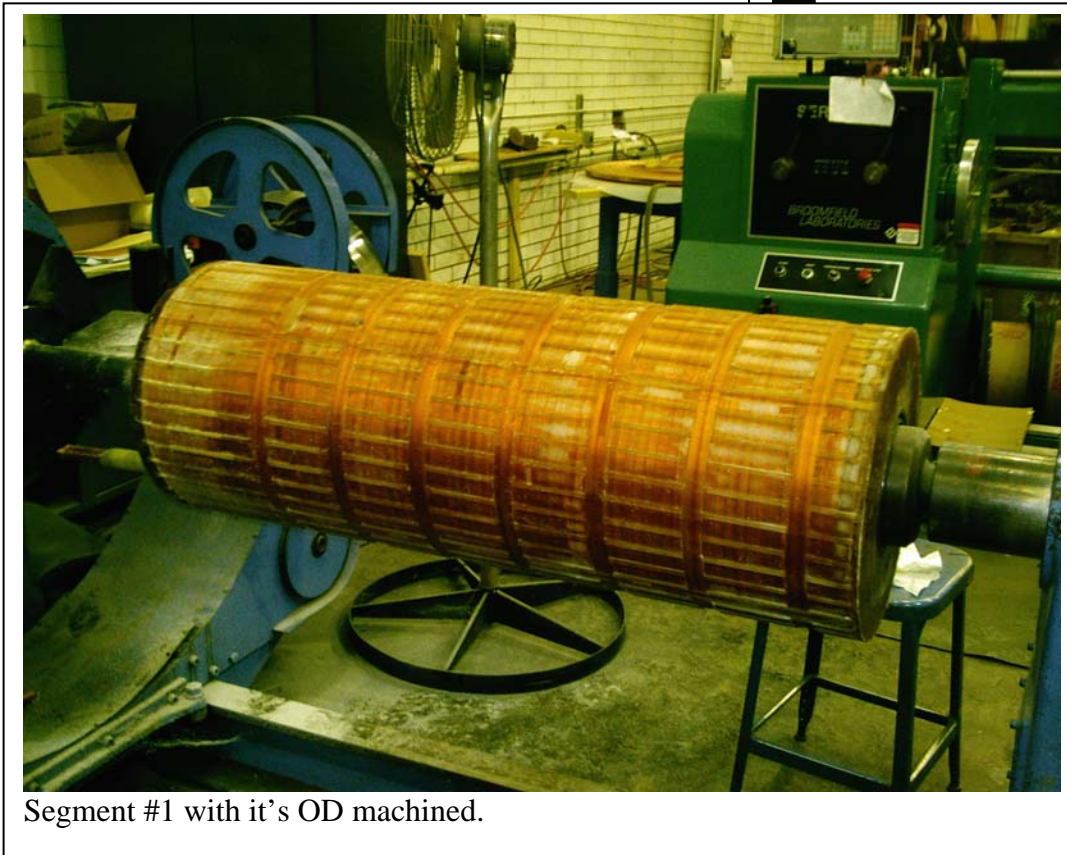
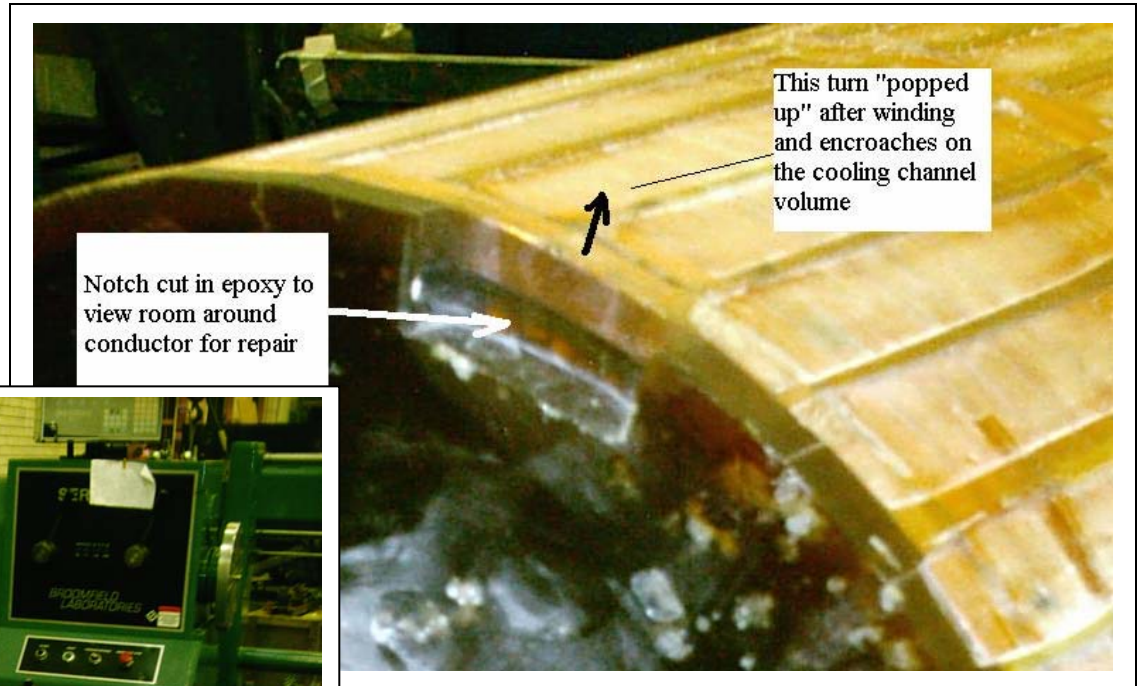


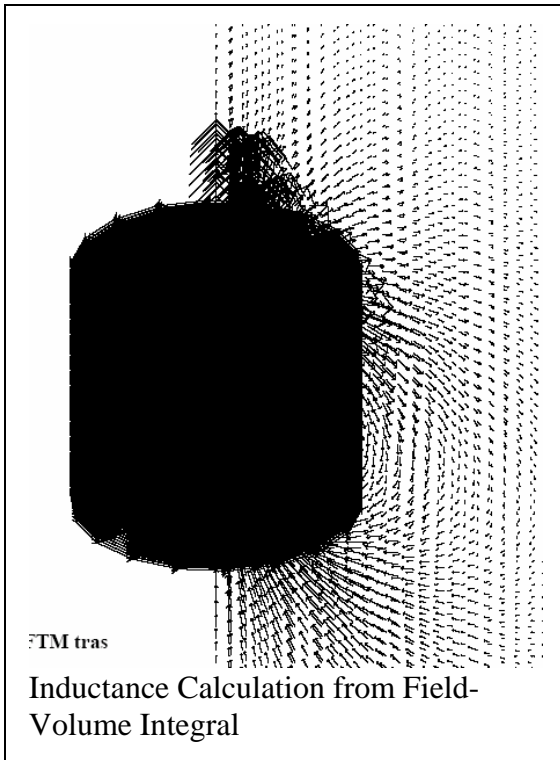
Segment #1 out of the mold. External Silicon fillers that form the “waffle” pattern have not yet been removed

Conductor Non-Conformance Simulation Circuit Simulation for the Displaced Segment #1 Conductor

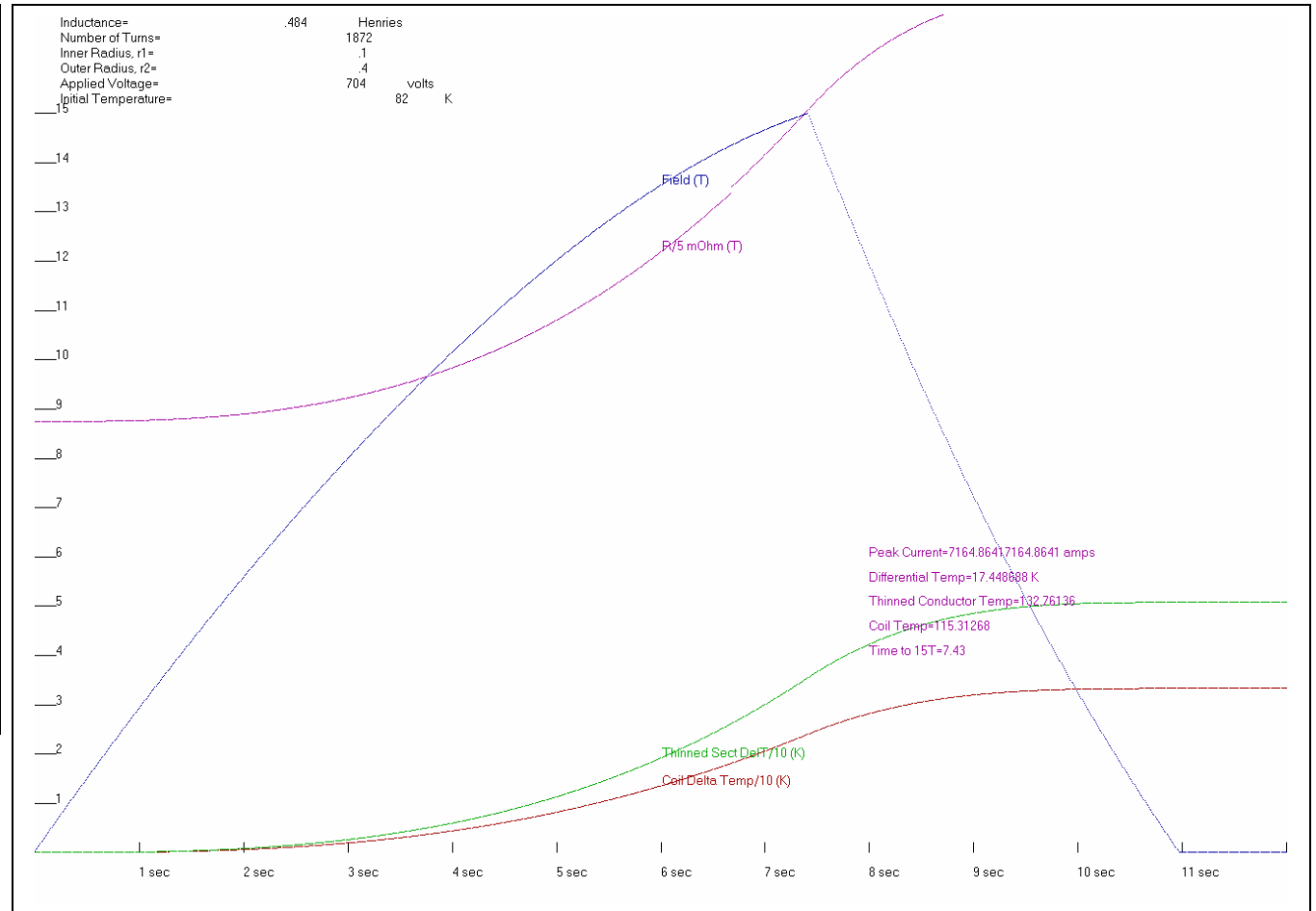
A conductor in segment 1 shifted radially outward and encroached on the channel spaces. It was damaged during the machining operation.

Ribs were knocked off during an initial attempt to machine the coil on a lathe. They switched to a vertical mill





Bob Weggels electrical simulations are the simulations of record. However a coil simulation was run with a local conductor cross section reduced by 25%.



The local temperature went 17.4K higher than the rest of the coil.

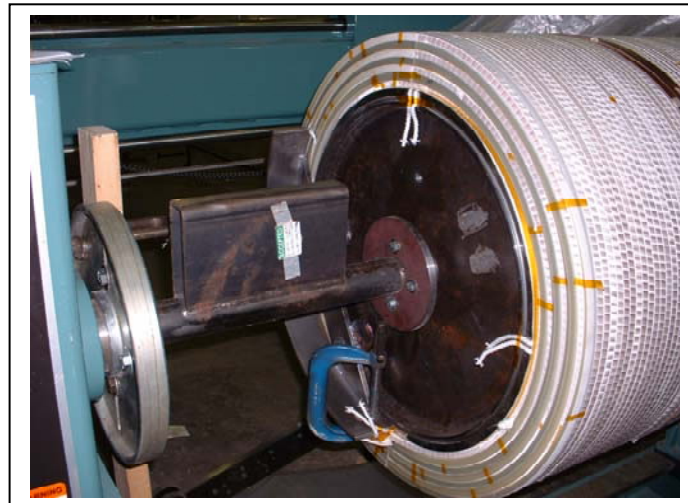
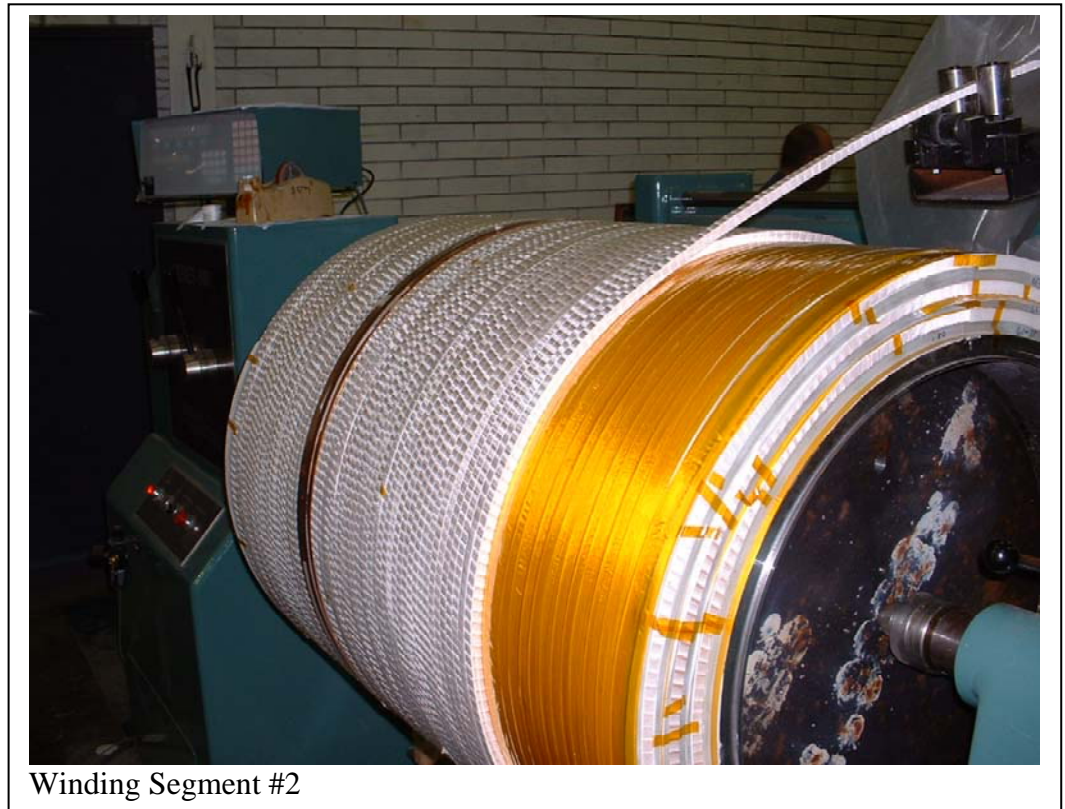
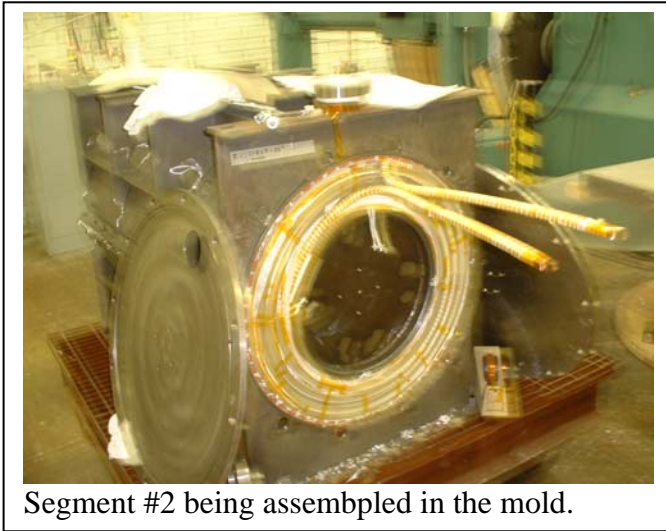
The hoop compressive stress is $E \cdot \alpha \cdot \Delta T$ or $100\text{GPa} \cdot 10e-6 \cdot 17.4$ or 17.4 MPa. This is compression and offsets the Lorentz force hoop tensile stress.

The outer turn R/t ratio is 20 so the radial tensile stress is 17.4/20 or less than 1.0 MPa. Remove the copper in the way of the cooling channels

Segment #2

As of Thursday January 27th :

Segment #2 has been impregnated and is cooling. It has not yet been removed from the mold.



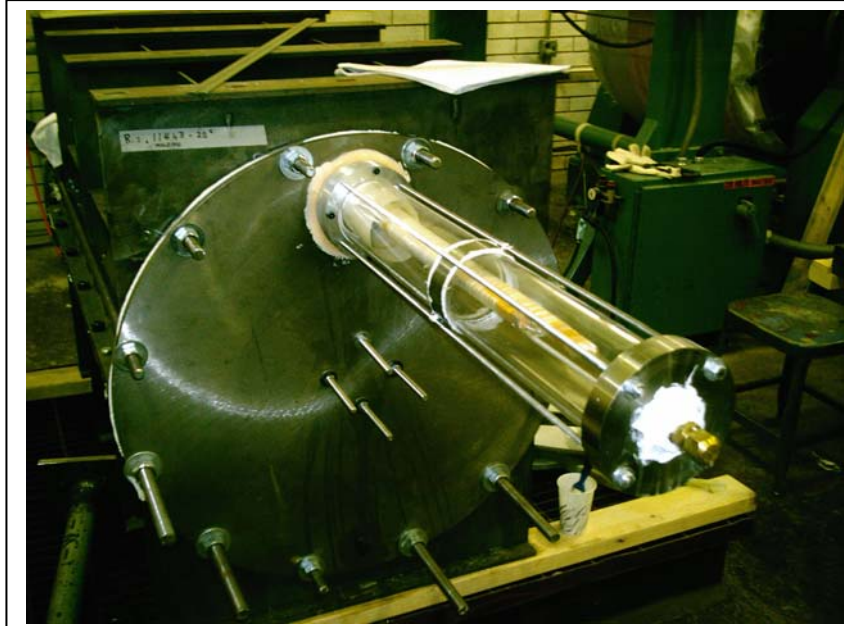
There was a leak in the longitudinal seam weld. This required application of RTV caulk and additional time to wait for the cure. This was to be held at 2 atm for 12 hrs prior to impregnation



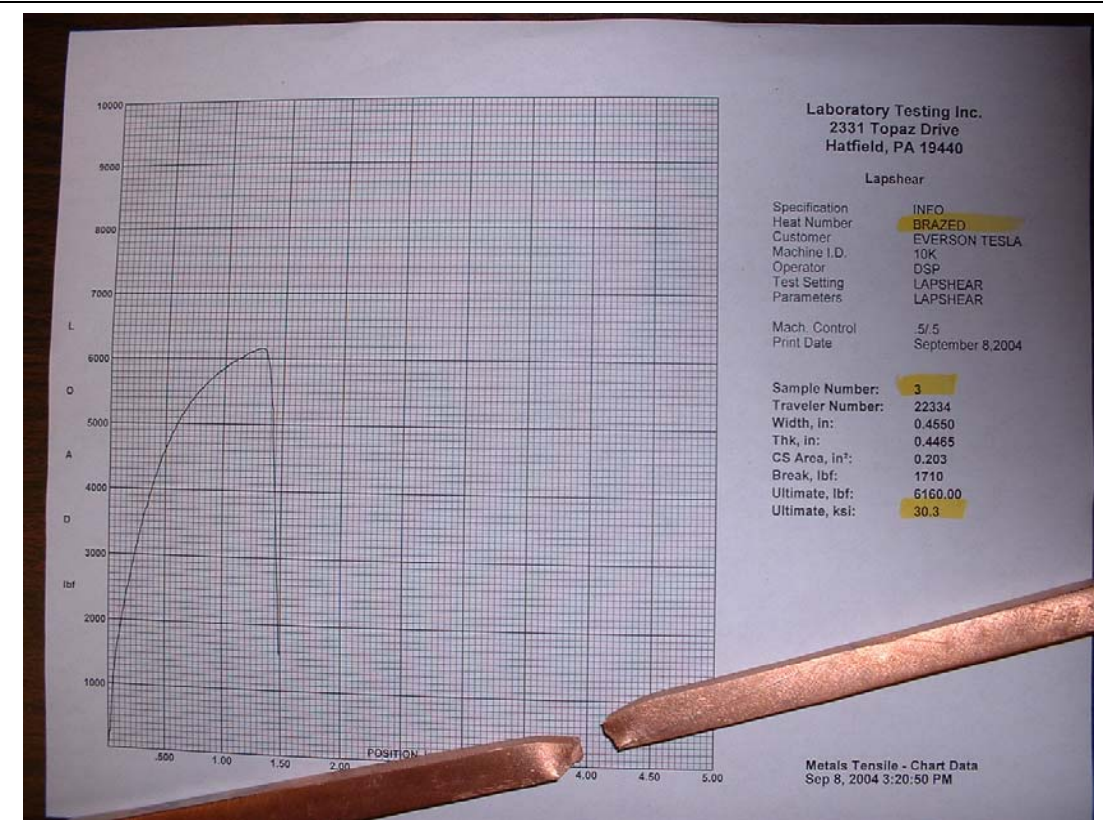
Segment #2 Lower Half of Mold



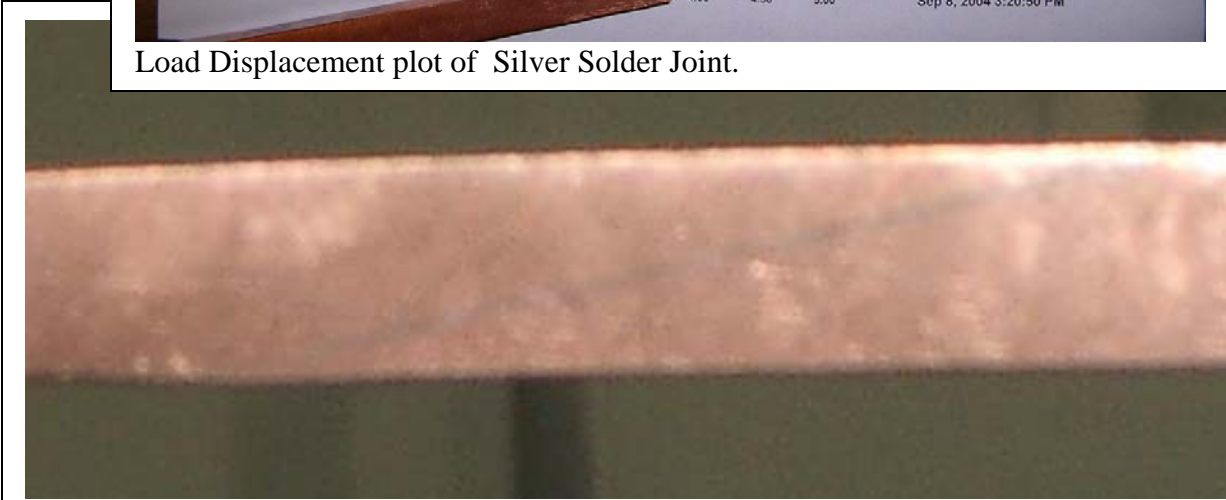
Segment #2 Mold (with Coil enclosed)



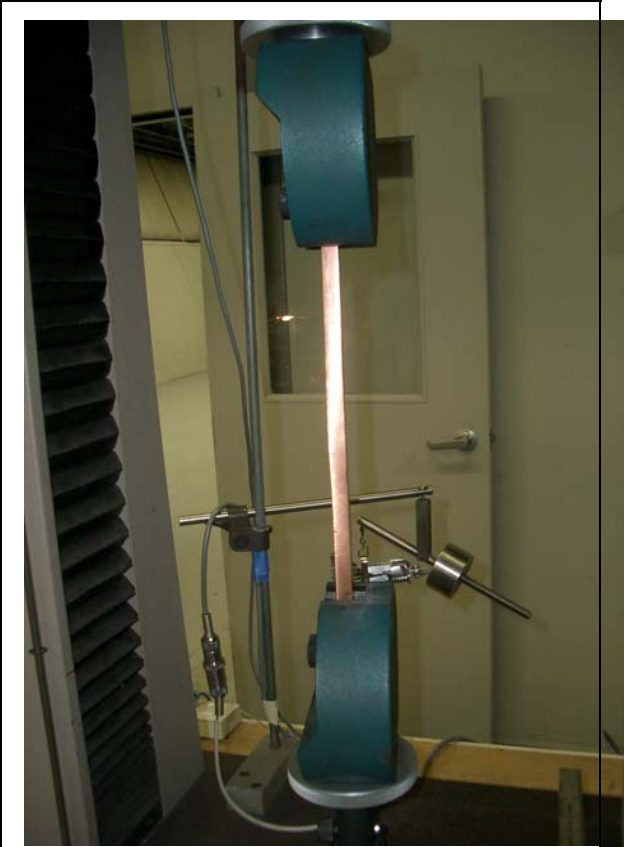
Segment #3 has Silver Solder Joints and these needed to be qualified prior to winding.



Load Displacement plot of Silver Solder Joint.



Faint indication of silver soldered scarf joint



Silver Solder Joint Tensile Test

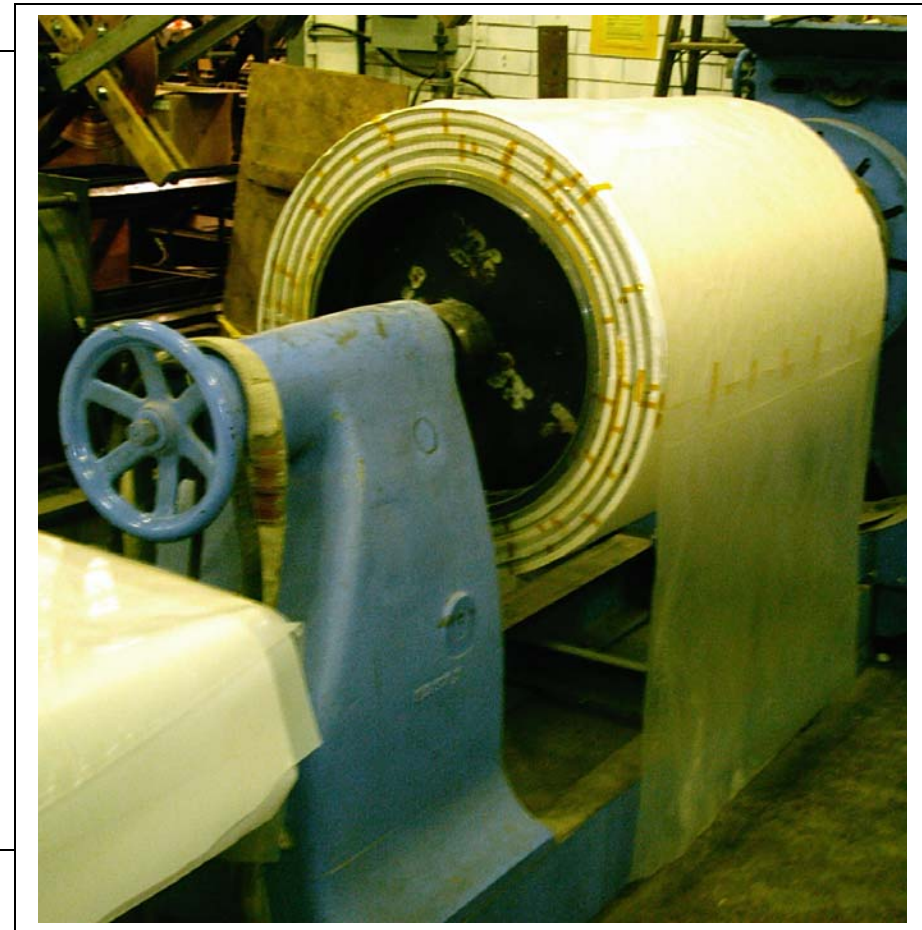
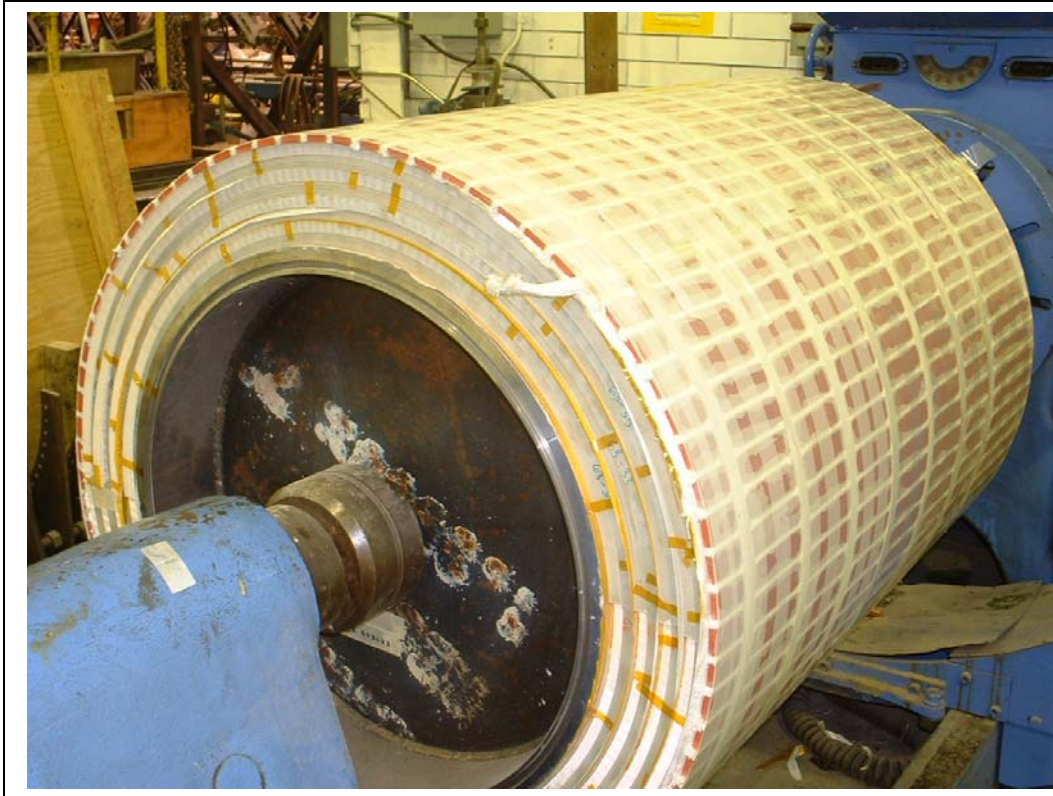
Segment #3

As of Thursday January 27th :

Segment #3 has been wound and the outer “waffle” pattern has been applied. This is scheduled for impregnation Feb 2 to 4



Segment #3 with Dave Rakos standing next to the coil for scale



Segment #3 - As of Feb 7 2005 it was epoxy filled and the cure process was begun

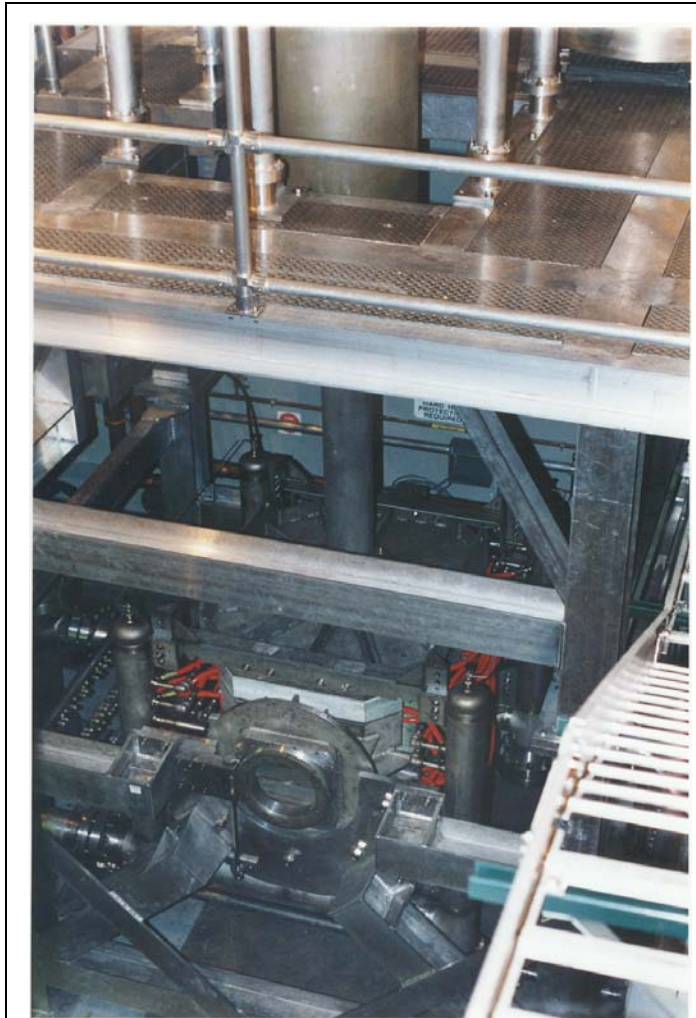


A vacuum is maintained on the mold (inside the autoclave box) with a vacuum pump (not shown) to the right of the autoclave). The epoxy tank is at an atmosphere gage. Ron adjusts epoxy flow manually. After the mold is filled, pressure is cycled to drive off bubbles. The mold is under pressure during the cure cycle to minimize the remaining bubbles.



Epoxy fill site glass. Everson doesn't have a good method to measure the flow going into the coil

Plans for Testing at MIT:



Lower Water Cooled Split Pair Copper Magnet - The BNL Pulsed Magnet will be in front of this, where the HXC Prototype cryostat is now positioned.

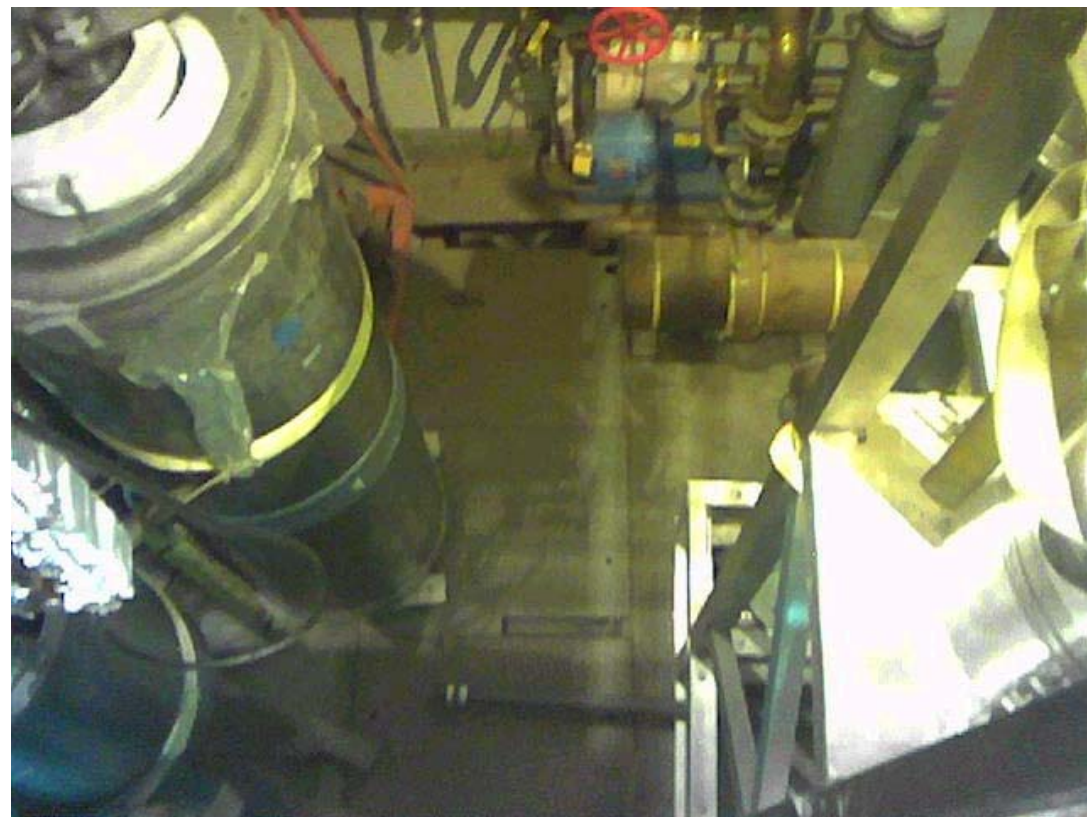
A formal proposal for testing has been submitted to BNL, and approval is imminent. The test location is the Pulsed Test Facility (PTF) at MIT-PSFC primarily used for testing of superconducting joints in a transient high field background. The test area will need to be cleared of extraneous equipment. Magnetic materials and tools will be removed.



PTF Upper Cryostat

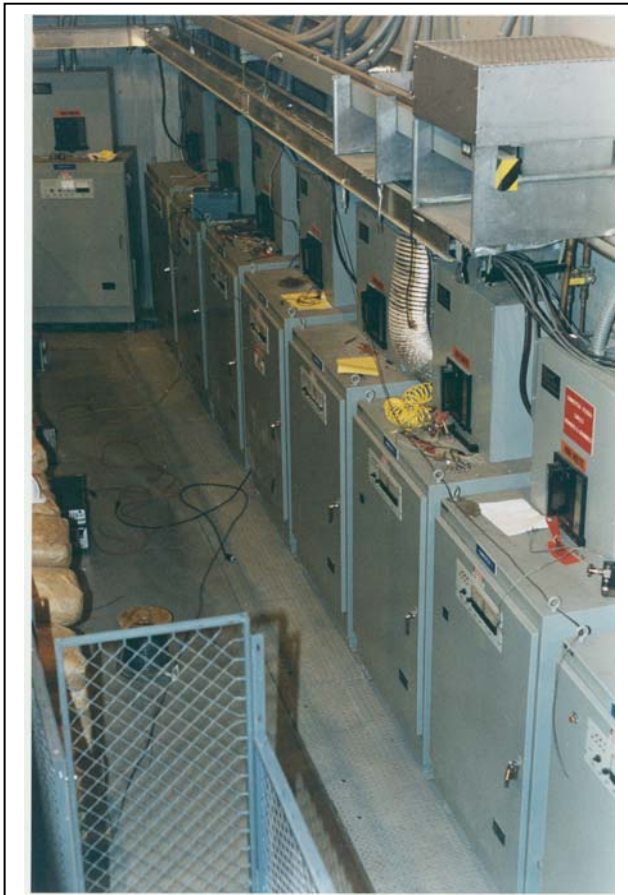
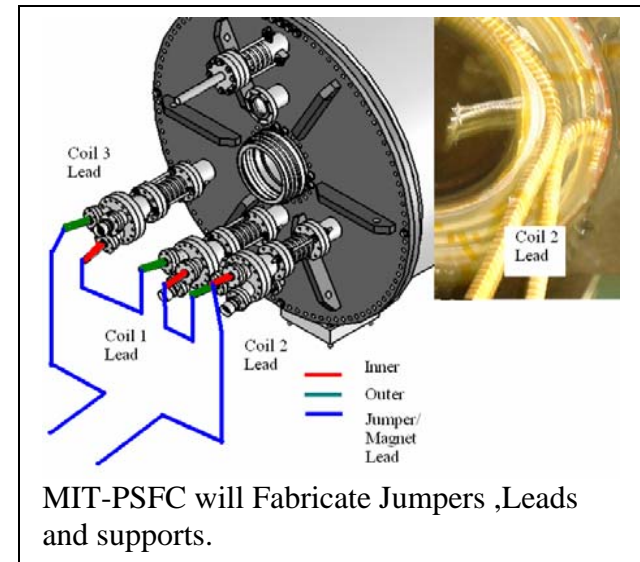


View of test area at floor level

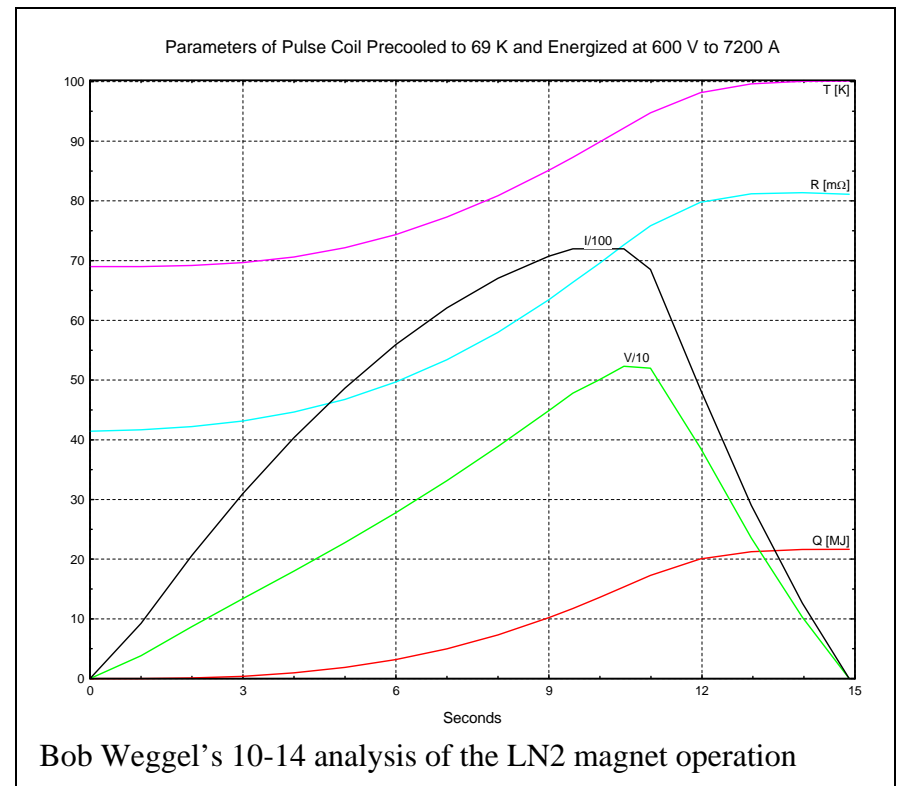


View of the test area floor. The dewars at left and HCX components at right need to be removed

Review of the current /voltage profiles indicates that the PTF power supplies will meet the test requirements. Modifications/Repairs are needed and will progress with approval of the Test plan proposal.



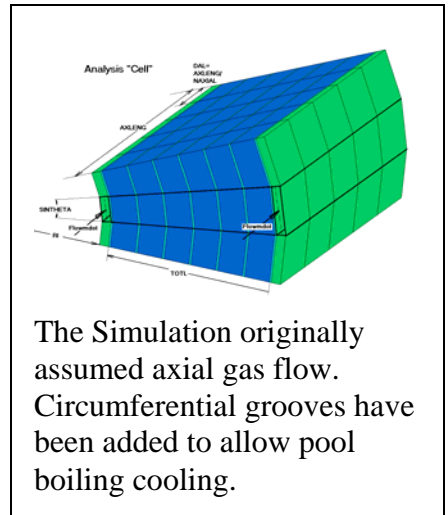
PTF Power Supplies



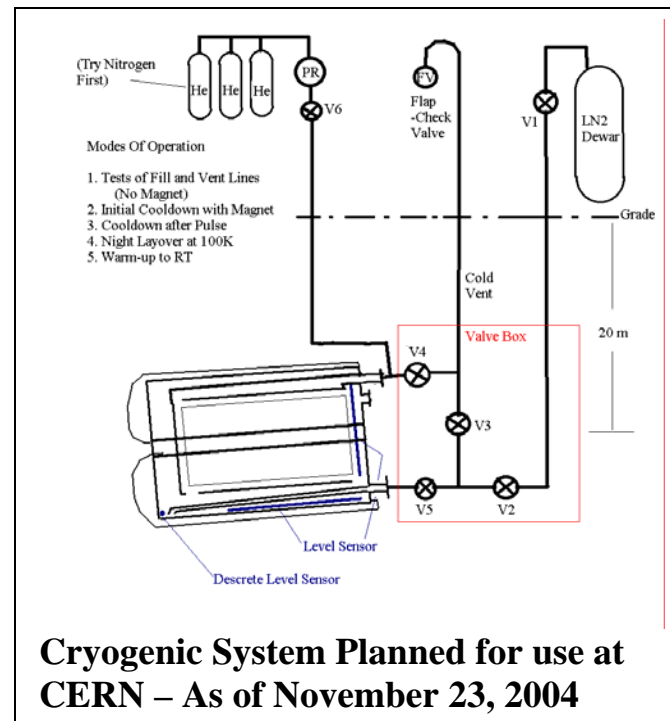
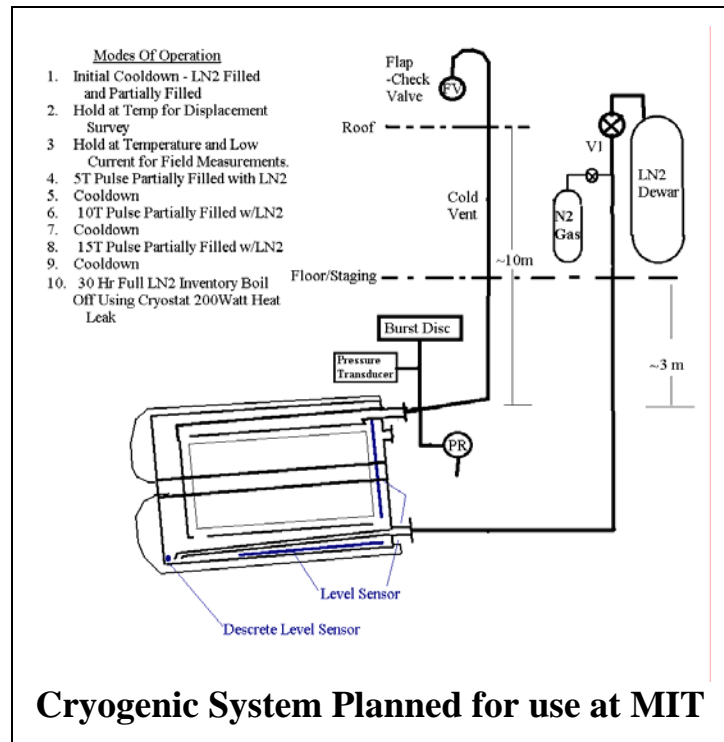
Cryogenic System for the Test

Only atmospheric liquid nitrogen cooling will be employed during pre-operational testing at MIT, although the system is intended to retain the capability to be cooled using gaseous Helium, or sub-cooled LN2.

The requirement to remove the LN2 during the experiments in CERN stems from the radiation environment causing activation of Nitrogen, and the creation of Ozone. Neither of these problems exists during preoperational testing. This allows a further simplification of the system planned for CERN. The system at MIT will simply be a feed and exhaust, and will pulse with remnants of LN2 in the magnet.



The Simulation originally assumed axial gas flow. Circumferential grooves have been added to allow pool boiling cooling.



Main Elements of the Planned Test Procedure

Initial Set-Up

Baseline data for CERNOX sensors at RT

First Room Temperature Electrical Tests

Hipot the coils.

Initial Cooldown, Dimensional Characterization

Stabilize at 80 to 77K. Check instrumentation, Baseline data for CERNOX sensors at LN₂ temperature. Check Level sensors. Compare Capacitive and discrete sensors.

Boil-Off – Heat Leak Test

At ½ fill height, measure level change with respect to time, Calculate heat leak

Record Cold Dimensional Changes

Map bore dimensional changes due to cooldown.

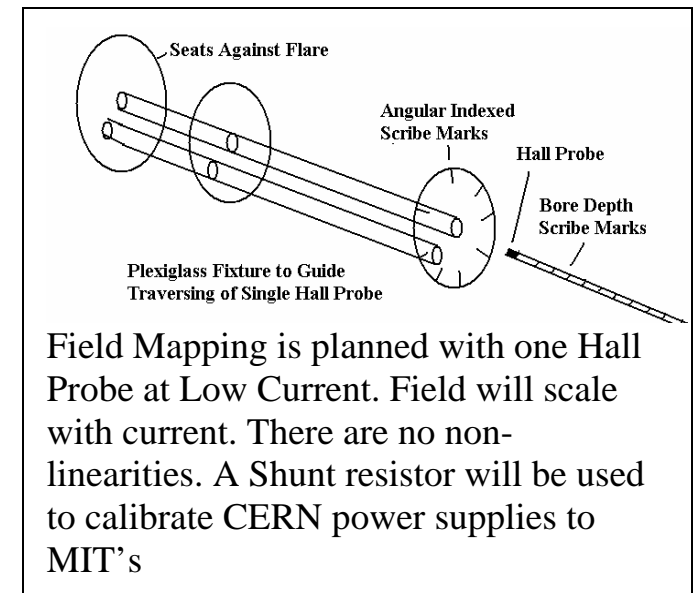
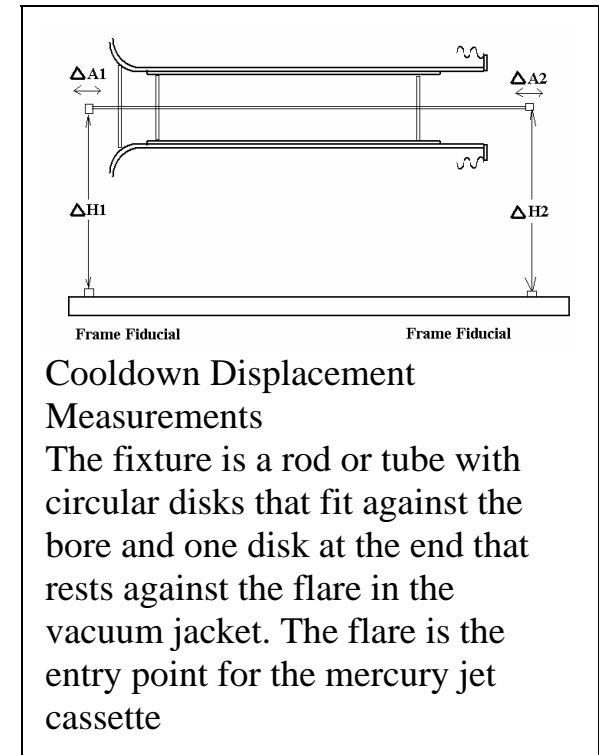
Inductance Measurement

Measure 3 coil low current static resistance. Measure constant-Low Voltage current ramp

5T Test

Demonstrate temperature uniformity in the three coil segments. Check target current time traces. Obtain final temperatures for the three coil segments. Check against predictions.

10T Test (First)



Demonstrate temperature uniformity in the three coil segments. Check target current time traces. Obtain final temperatures for the three coil segments. Check against predictions.
Time to cool with primarily gaseous cooling (1/3 fill height of LN2)

10T Test (Second)

Demonstrate temperature uniformity in the three coil segments
Time to cool with primarily pool boiling cooling (2/3 fill height of LN2)

Second Room Temperature Electrical Tests
Warm to RT. Conduct Electrical tests

10T Test (Third)

Slow cool to 80K, Run 10T test. Check target current time traces. Obtain final temperatures for the three coil segments. Check against predictions.
Cool with LN2 1/3 fill height to 80 K. Stabilize temperatures in 3 coils.

15T Test (First)

Demonstrate 15T operational capability. Check target current time traces. Obtain final temperatures for the three coil segments. Check against predictions.

15T Test (Second)

Demonstrate 15T operational capability. Check target current time traces. Obtain final temperatures for the three coil segments. Check against predictions.
Cooling Behavior 2/3 immersed, Obtain Time temperature plot for cooldown

Third Room Temperature Electrical Tests

Report Test Results