

SHIELDING STUDIES FOR THE MUON COLLIDER TARGET
(From STUDY II to IDS120f Geometries)

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MUON COLLIDER TARGET STATION

COMPONENTS

1. PROJECTILES (PROTON BEAM).
2. TARGET (MERCURY JET).
3. SUPERCONDUCTING COILS (SC) FOR UP TO 14 T MAGNETIC FIELD AROUND INTERACTION AREA (NbSn, NbTi).
4. RESISTIVE COILS FOR ADDITIONAL 6 T MAGNETIC FIELD SO THAT $B \sim 20$ T AROUND THE INTERACTION AREA.
5. BEAM PIPE (STST Stainless Steel).
6. CRYOGENIC COOLING FOR THE SC SOLENOIDS.
7. MERCURY COLLECTING TANK (BEAM DUMP) AND REMOVAL SYSTEM.
8. SHIELDING CONFIGURATIONS (WC BEADS+H₂O).

TARGET REQUIREMENTS/ISSUES

- MAGNETIC FIELD OF 20 T AT TARGET.
- MINIMIZE DEMAND ON CRYOGENIC OPERATIONS.
- AVOID QUENCHING.
- RADIATION DAMAGE.
- STRUCTURAL/MECHANICAL LIMITS FOR SUPERCONDUCTING COILS.
- SHIELDING MATERIAL.

RESULTS OF DEPOSITED ENERGY AND PEAK VALUES FOR DIFFERENT GEOMETRIES WILL BE PRESENTED (MARS, MARS+MCNP). MCNP CROSS SECTION LIBRARIES USED FOR A MORE DETAIL STUDY OF LOW ENERGY NEUTRONS (<0.1 MeV).

Energy deposition from MARS, MARS+MCNP.

STUDY II GEOMETRY.

SHIELDING: 80%WC+20% H₂O

4MW proton beam.

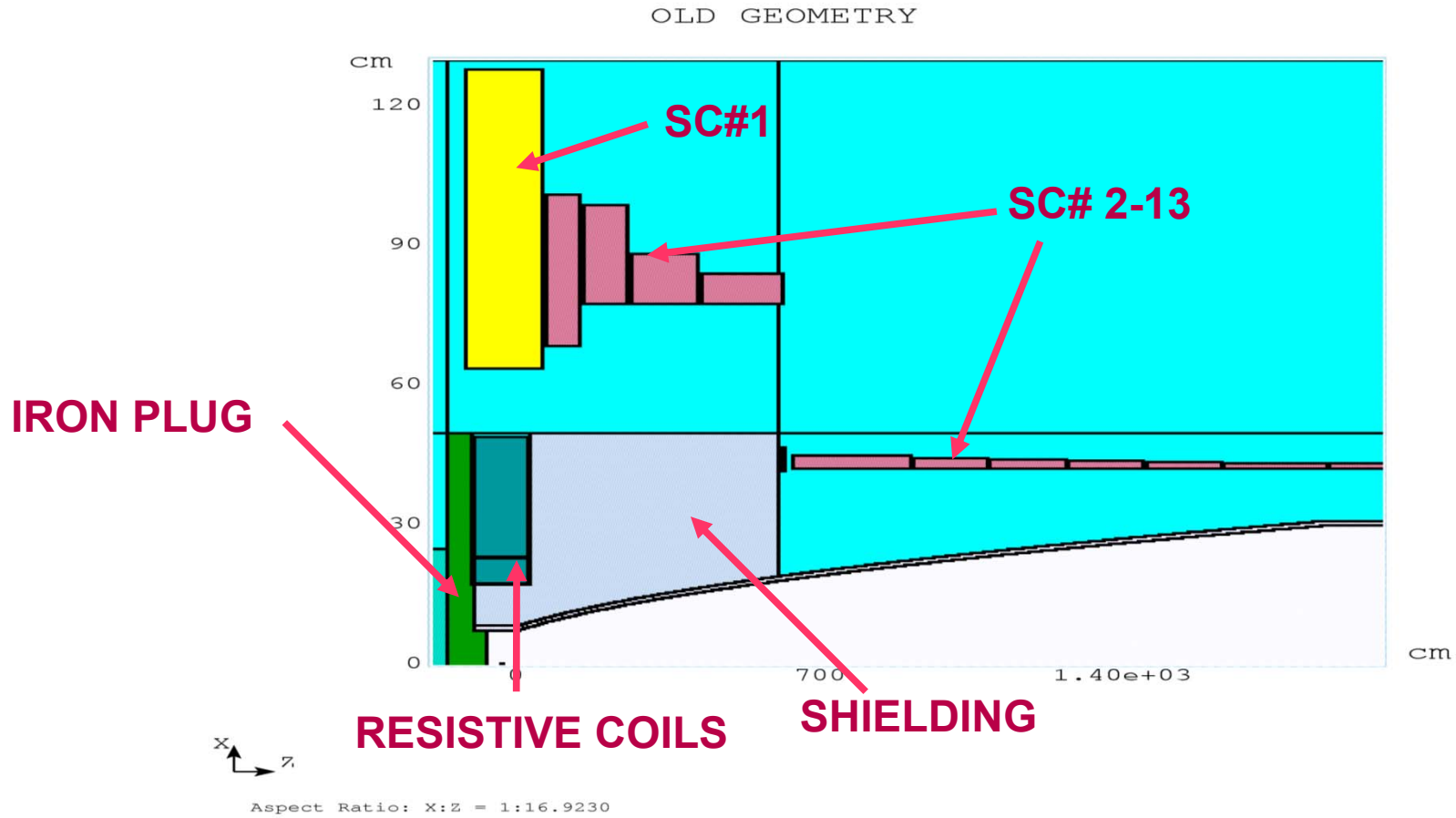
Initially E=24 GeV,

GAUSSIAN PROFILE: $\sigma_x = \sigma_y = 0.15$ cm.

Now E=8 GeV,

GAUSSIAN PROFILE: $\sigma_x = \sigma_y = 0.12$ cm.

STUDY II SOLENOID GEOMETRY, 13 SUPERCODUCTIN COILS (SC)



SC#1	-120 < z < 57.8 cm	$R_{in} = 63.3$ cm	$R_{out} = 127.8$ cm	
SC#2	67.8 < z < 140.7 cm	$R_{in} = 68.6$ cm	$R_{out} = 101.1$ cm	
SC#6-13	632.5 < z < 218.7 cm	$R_{in} = 42.2$ cm	$R_{out} = 45.1 \rightarrow 43.4$ cm	(TOTAL # SC=13)

DEPOSITED ENERGY WITH 24 GeV AND 8 GeV BEAM

MARS WITH 0.1 MeV DEFAULT NEUTRON ENERGY CUTOFF VS.

MARS+MCNP WITH 10^{-11} MeV NEUTRON ENERGY CUTOFF.

ENERGY DEPOSITED IN SOLENOIDS IN KW.

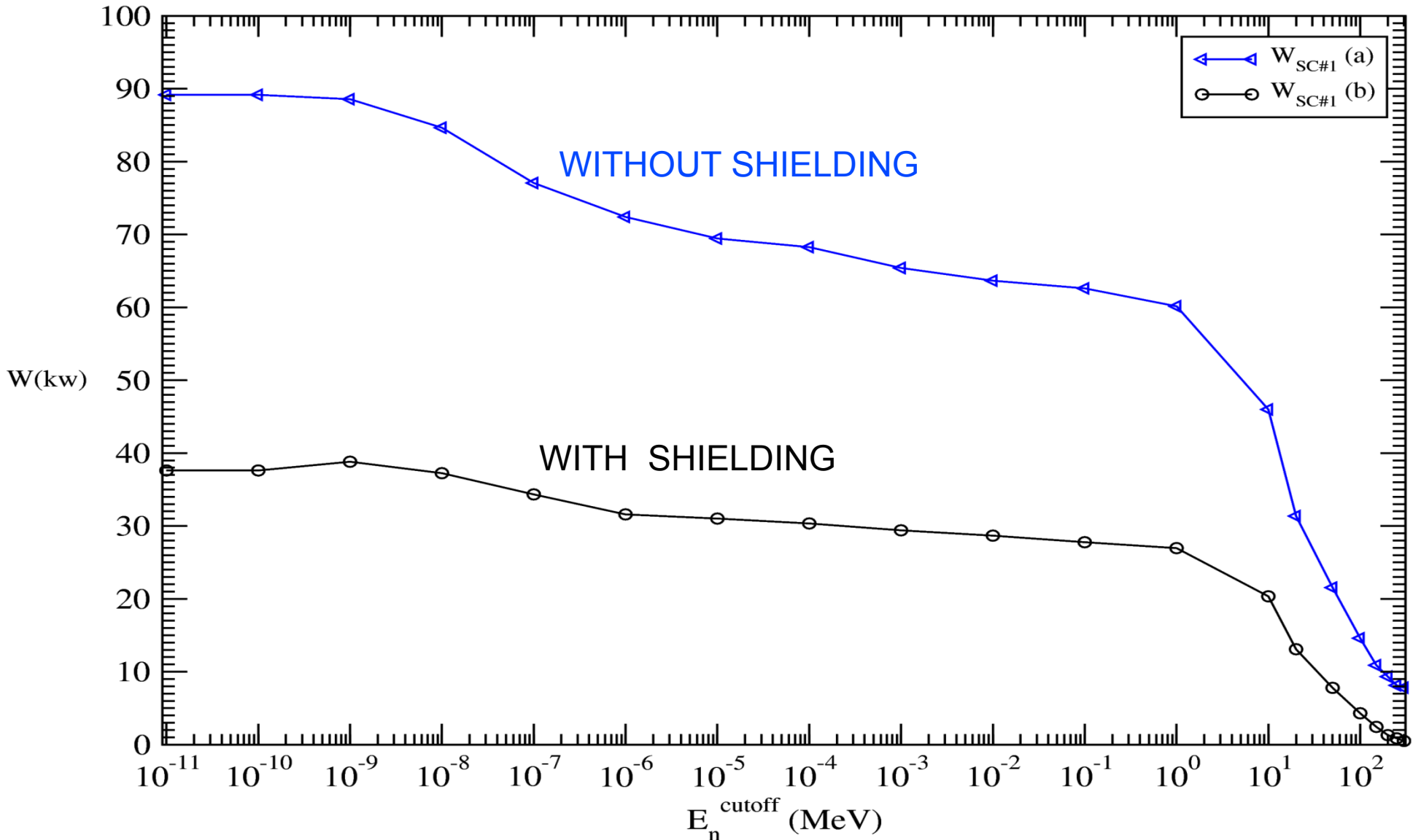
	SC#1	%	SC#2-13	%	Total	%		
24 GeV □	a	14.28	–	14.90	–	29.18	–	MARS
	b	22.06	+54.48	16.30	+9.40	38.36	+31.50	MARS+MCNP
8 GeV □	c	24.97	+74.86	11.84	-20.54	36.81	+26.15	MARS
	d	37.62	+50.66	12.46	+5.24	50.08	+36.05	MARS+MCNP

From 24 GeV to 8 GeV, and from a more detail treatment of low energy neutrons: from ~14 kW to ~38 kW power in SC1 and from ~29 kW to 50 kW in total power.

OFF/ON SHIELDING, DIFFERENT NEUTRON ENERGY CUTOFFS.

Deposited energy Power for SC#1, standard geom., different neutron energy cutoffs (10^{-11} to 300 MeV)

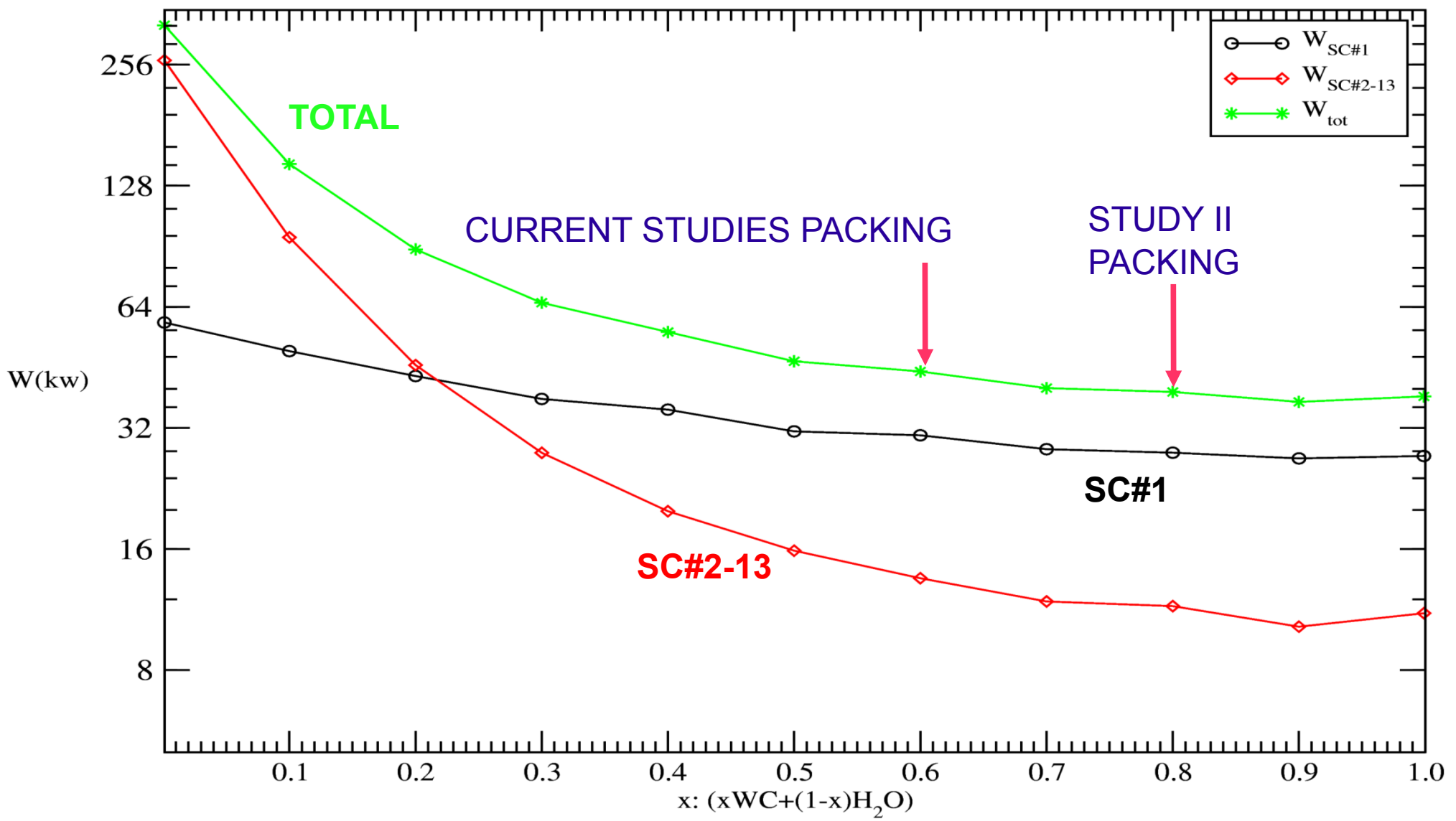
(MARS+MCNP) a=NO SHIELDING,b=80%WC+20H₂O, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x=\sigma_y=0.12$ cm



SAME RESULTS FOR SC#2-13

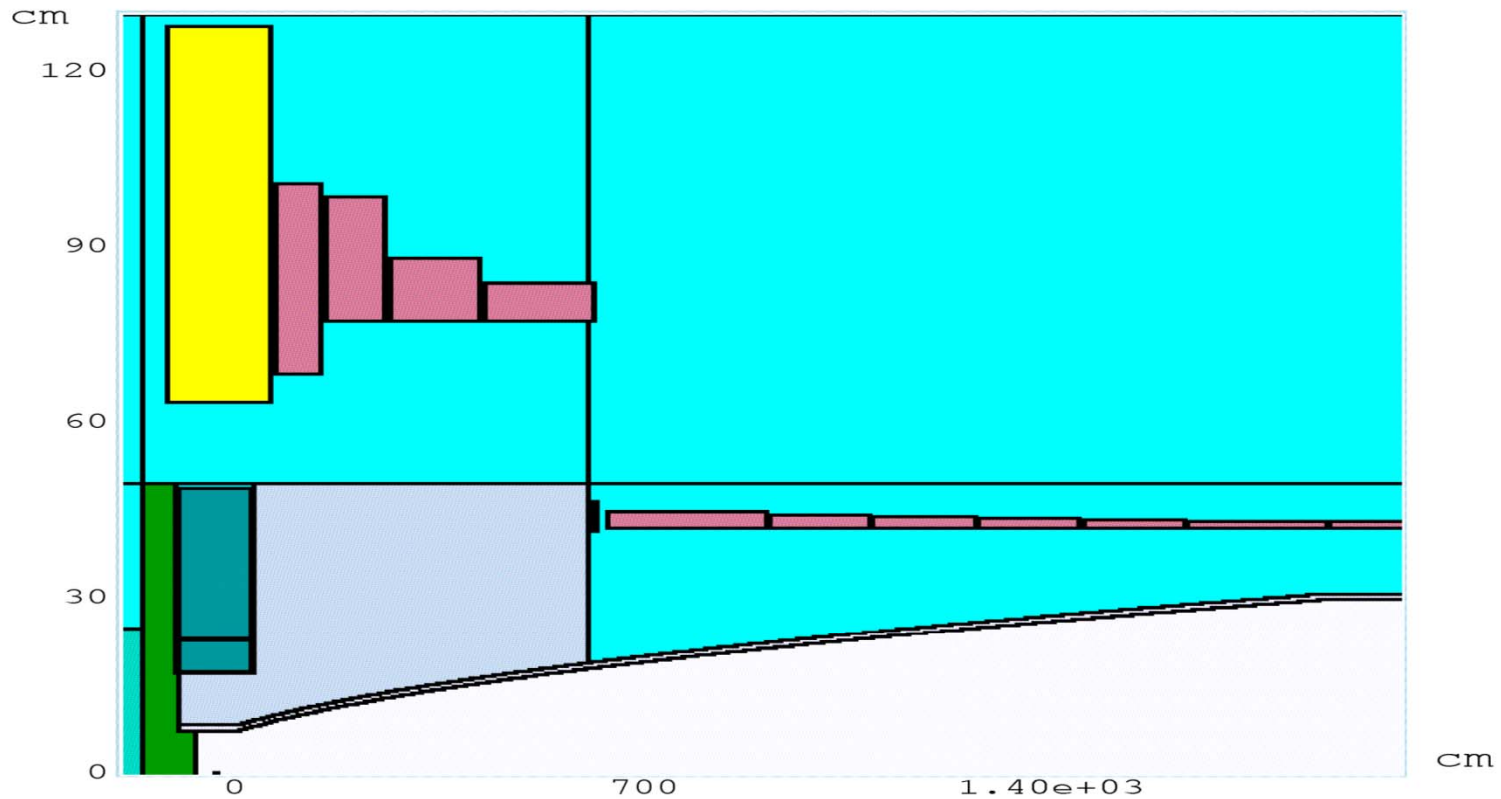
High energy neutrons are a problem even with shielding material.

Deposited energy Power for SC#1, SC#2-13 and total, standard geom., different shielding compositions.
 (MARS+MCNP), x WC+(1-x) H₂O shielding, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x = \sigma_y = 0.12$ cm



60% WC + 40% H₂O IS A MORE REALISTIC PACKING FRACTION FOR SHIELDING MATERIAL.

OLD GEOMETRY



Aspect Ratio: X:Z = 1:16.9230

REPLACING RESISTIVE MAGNET WITH SHIELDING MATERIAL (80%WC+20% H₂O) REDUCES DEPOSITED ENERGY IN SC#1 FROM ~38 kW TO ~13 kW (A FACTOR OF ~3). (MARS+MCNP WITH NEUTRON ENERGY CUTOFF OF 10⁻¹¹ MeV)

IDS80 (IR=80 cm)

TO PROVIDE MORE SPACE FOR SHIELDING, ESPECIALLY FOR SOLENOIDS AROUND THE INTERACTION AREA.

SHIELDING:60%WC+40% H₂O

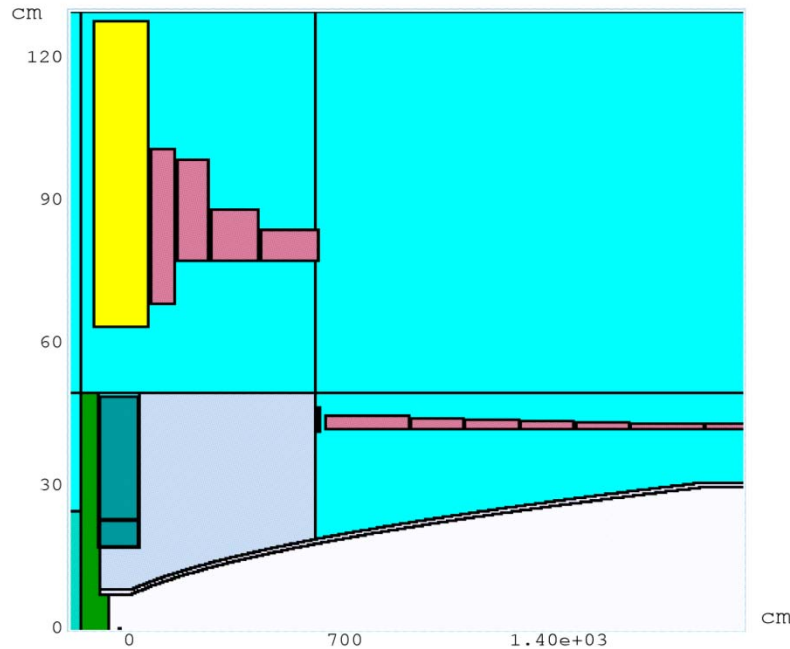
4MW proton beam.

PROTONS ENERGY E=8 GeV.

GAUSSIAN PROFILE: $\sigma_x = \sigma_y = 0.12$ cm.

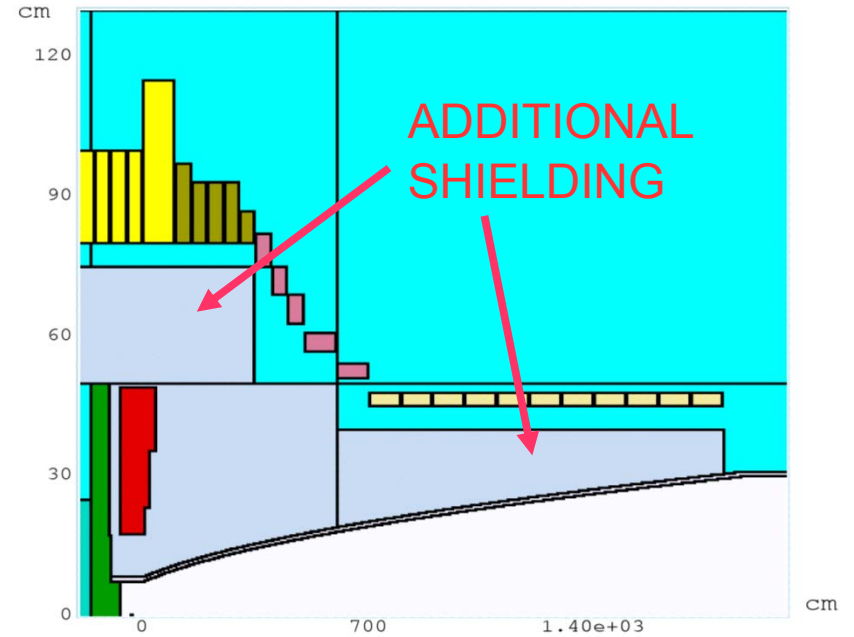
STUDY II VS. IDS80 SOLENOID GEOMETRY

OLD GEOMETRY



Aspect Ratio: X:Z = 1:16.9230

SUPER-ENHANCED GEOMETRY SC#1-10 (NBSN) SC#11-26 (SCON)



Aspect Ratio: X:Z = 1:16.9230

IDS80: SC#1-10 $-200 < z < 345$ cm $R_{in} = 80.0$ cm $R_{out} = 100$ (1-4)/115 (5)/97 (6)/93(7-9)/87(10)cm
 SC#11-15 $350 < z < 695$ cm $R_{in} = 75.0 \rightarrow 51$ cm $R_{out} = 82.0 \rightarrow 54$ cm
 SC#16-26 $700 < z < 1795$ cm $R_{in} = 45$ cm $R_{out} = 48$ cm **(TOTAL # SC=26)**

From 63.3 cm (SC#1) to 80 cm (SC#1-10) inner radius for solenoids around target area: more space for shielding.

MARS+MCNP(NEUTRON ENERGY CUTOFF 10^{-11} MeV)

60%WC+40% H₂O SHIELDING

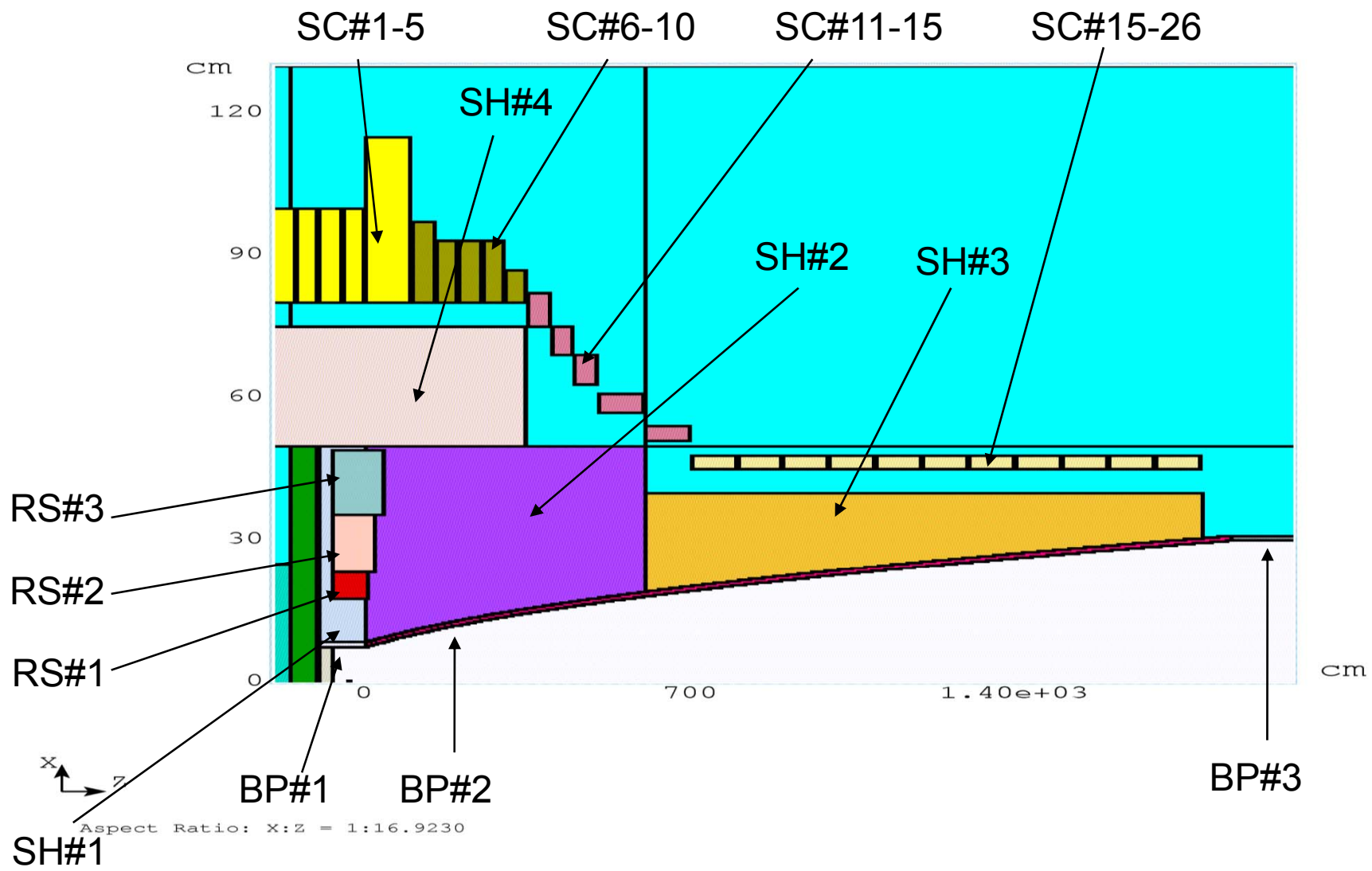
STUDY II

IDS80

SC#1: 42.5 kW ----->SC#1-5: 2.4 kW

SC#1-13: 58.1 kW----->SC#1-26: 3.4 kW

DETAIL STUDY OF IDS80 WITH IRON PLUG (MARS+MCNP, 10^{-11} MeV NEUTRON ENERGY)



ENERGY DEPOSITED IN SC SOLENOIDS (SC#), SHIELDING (SH#).

NiSn/NiTi	P(kW)	60/40	P(kW)
SC#1-5	2.42	SH#1	967.5
SC#6-10	0.57	SH#2	1107.5
SC#11-15	0.16	SH#3	36.04
SC#16-26	0.31	SH#4	31.83
SC#1-26	3.64	SH#1-4	2142.87

ENERGY DEPOSITED IN RESISTIVE COILS (RS#), BEAM PIPE (BP#), IRON PLUG (IP#).

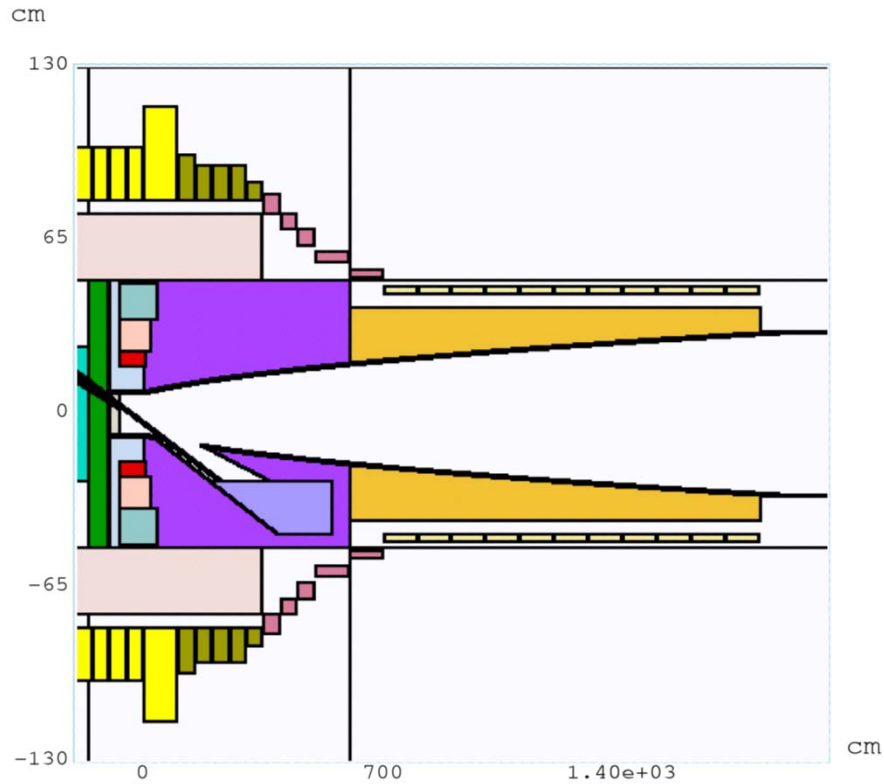
(Cu)	P(kW)	(STST)	P(kW)	(FeCo)	P(kW)
RS#1	68.25	BP#1	207.50	IP#1	0.24
RS#2	66.05	BP#2	238.40	IP#2	0.11
RS#3	36.50	BP#3	8.02	IP#3	11.35
RS#1-3	170.80	BP#1-3	453.92	IP#1-3	11.70

ENERGY DEPOSITED IN OTHER PARTS AND TOTALS .

TOTALS	P(kW)
SC#1-26	3.64
SH#1-4	2142.87
RS#1-3	170.80
BP#1-3	453.92
IP#1-3	11.70
Hg TARG.	379.90
Hg POOL	9.32
Be WIND.	0.62
TOTAL	3172.77

ABOUT 80% OF THE 4 MW IS ACCOUNDED FOR .

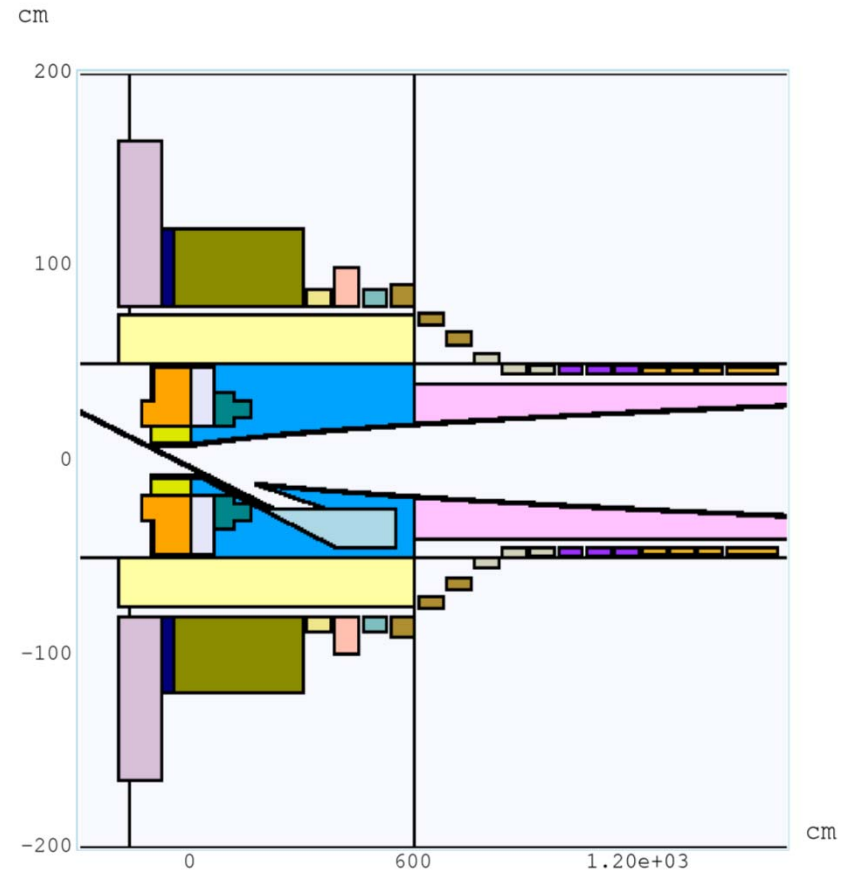
IDS80 GEOMETRY



Aspect Ratio: Y:Z = 1:8.46153

SC#1-5: 2.6 kW
 TOTAL: 3.47 kW
 Peak SC5: 0.36 mW/gr

IDS80f GEOMETRY

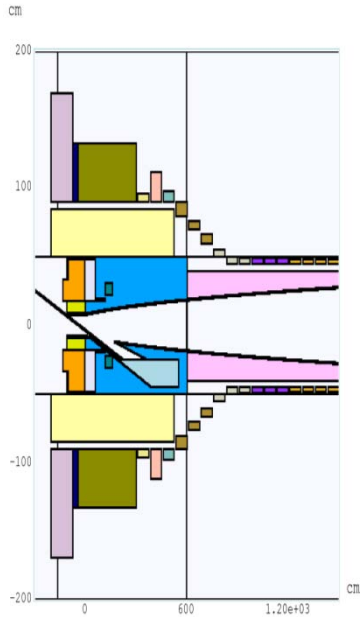


Aspect Ratio: Y:Z = 1:4.75

SC3: 4.15 kW
 TOTAL: 5.69 kW
 Peak SC3: 0.42 mW/gr

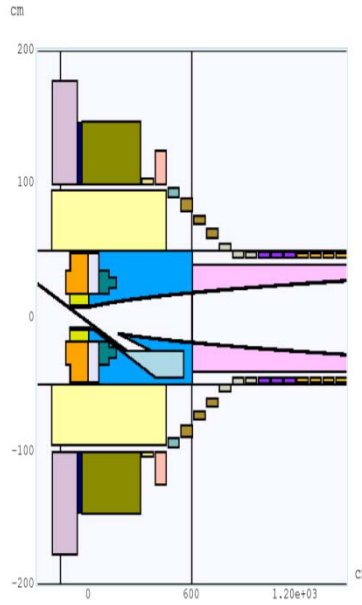
IDS90f-IDS120f GEOMETRIES:ENERGY DEPOSITION (kW), PEAK VALUES (mW/gr) (SC#1-9: NbSn, SC#10-19:NbTi).

IDS90f



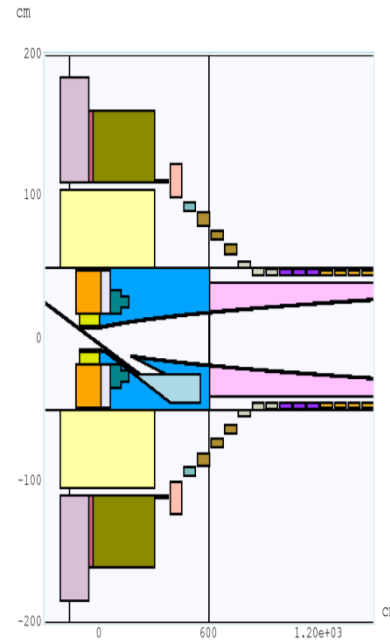
Aspect Ratio: Y:Z = 1:4.5

IDS100f



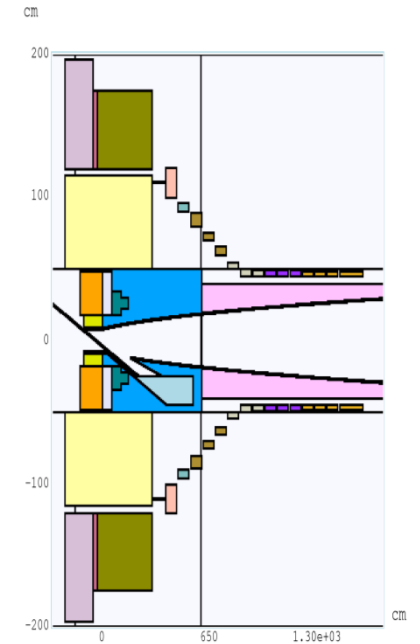
Aspect Ratio: Y:Z = 1:4.5

IDS110f



Aspect Ratio: Y:Z = 1:4.5

IDS120f



Aspect Ratio: Y:Z = 1:5.0

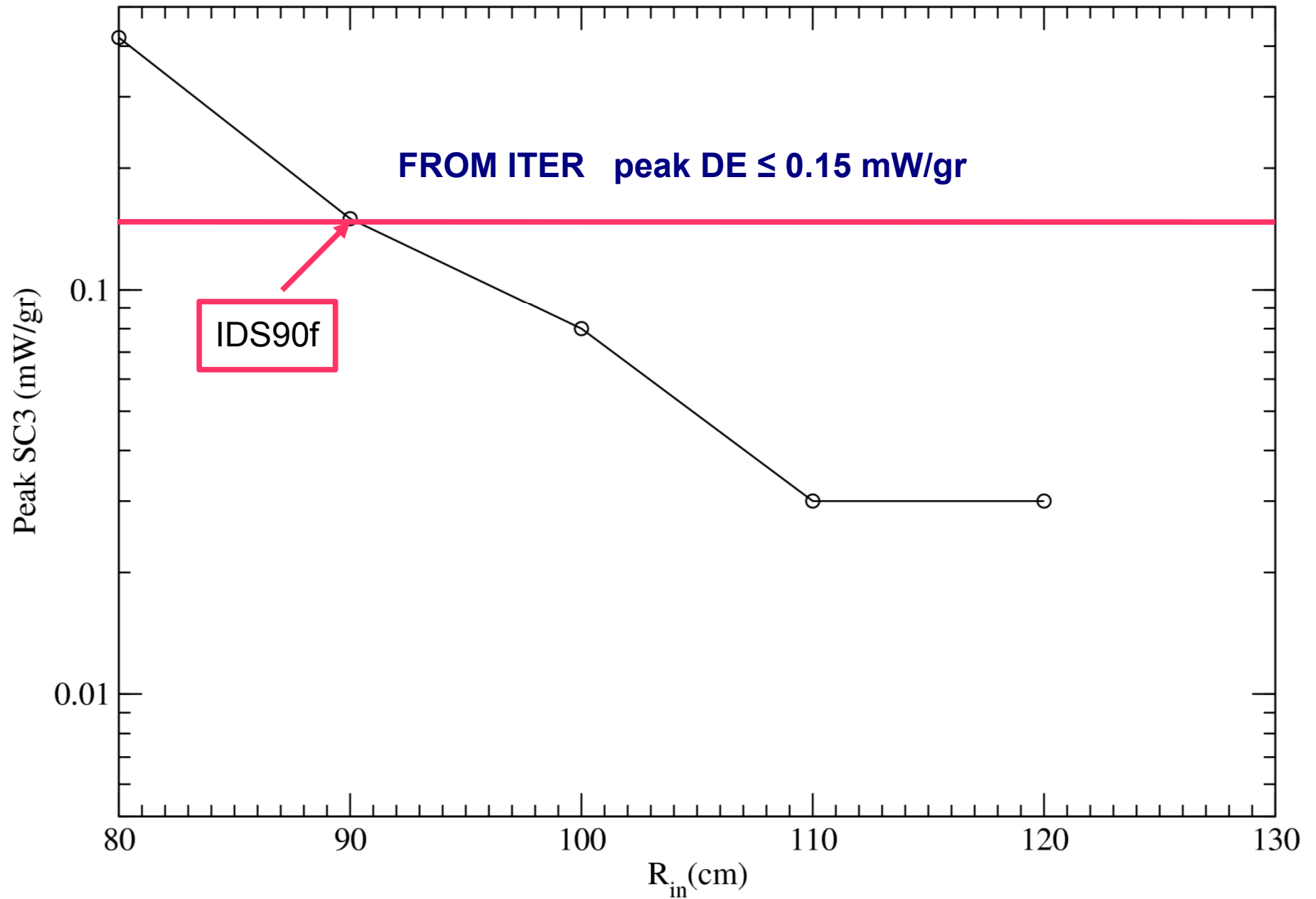
SC3: 2.07
 TOTAL: 2.45
 Peak SC3: 0.15
 SC10: 0.07

SC3: 1.01
 TOTAL: 1.41
 Peak SC3: 0.08
 SC9: 0.05
 SC10: 0.10
 SC11: 0.04

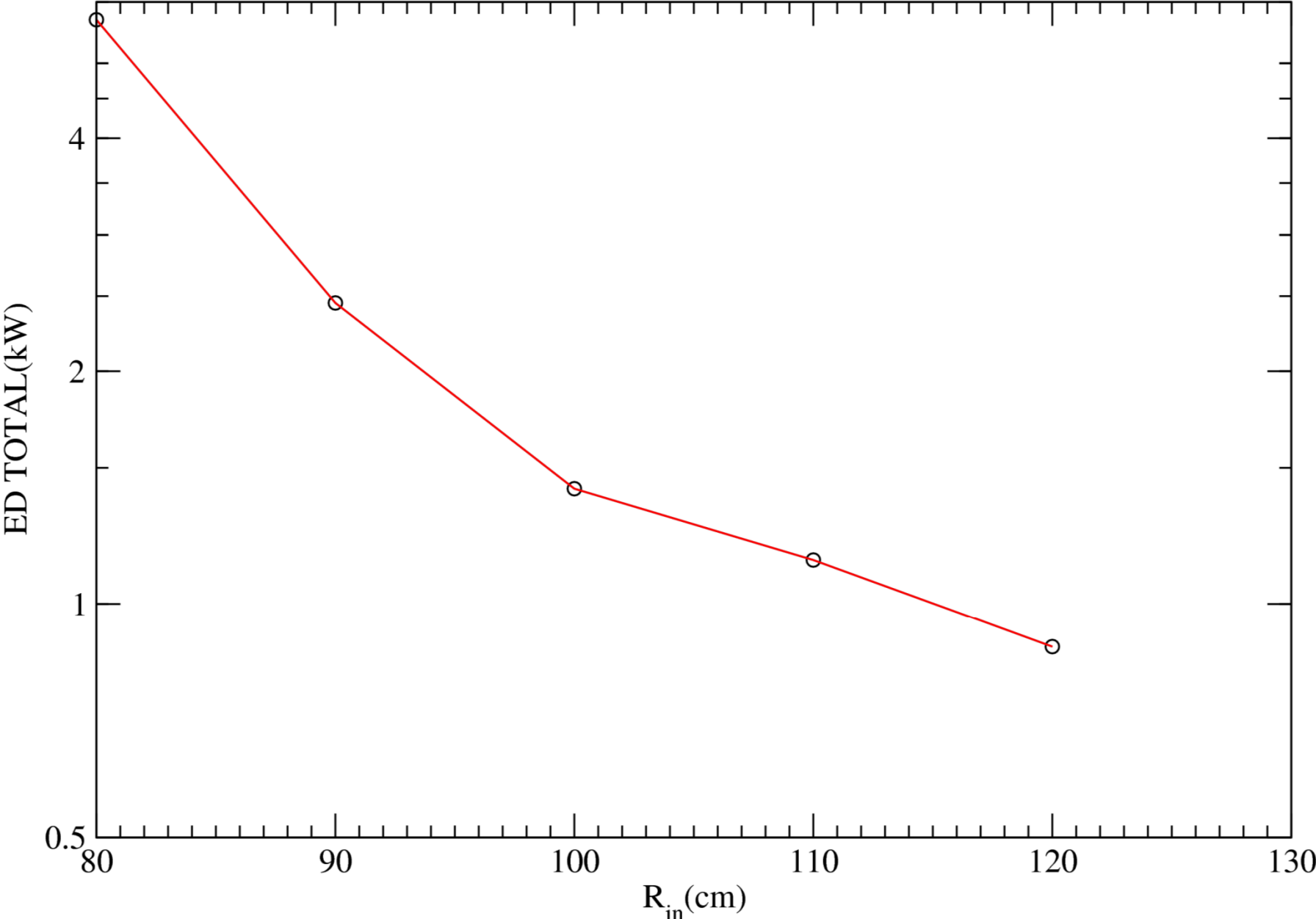
SC3: 0.49
 SC5: 0.20
 TOTAL: 1.14
 Peak SC3: 0.03
 SC5: 0.05
 SC12/19 : 0.09

SC3: 0.26
 SC5: 0.19
 TOTAL: 0.97
 Peak SC3: 0.03
 SC7: 0.07
 SC14: 0.08

**IDS80f-IDS120f GEOMETRIES:SC3 PEAK VALUES (mW/gr)
(semi-log scale).**

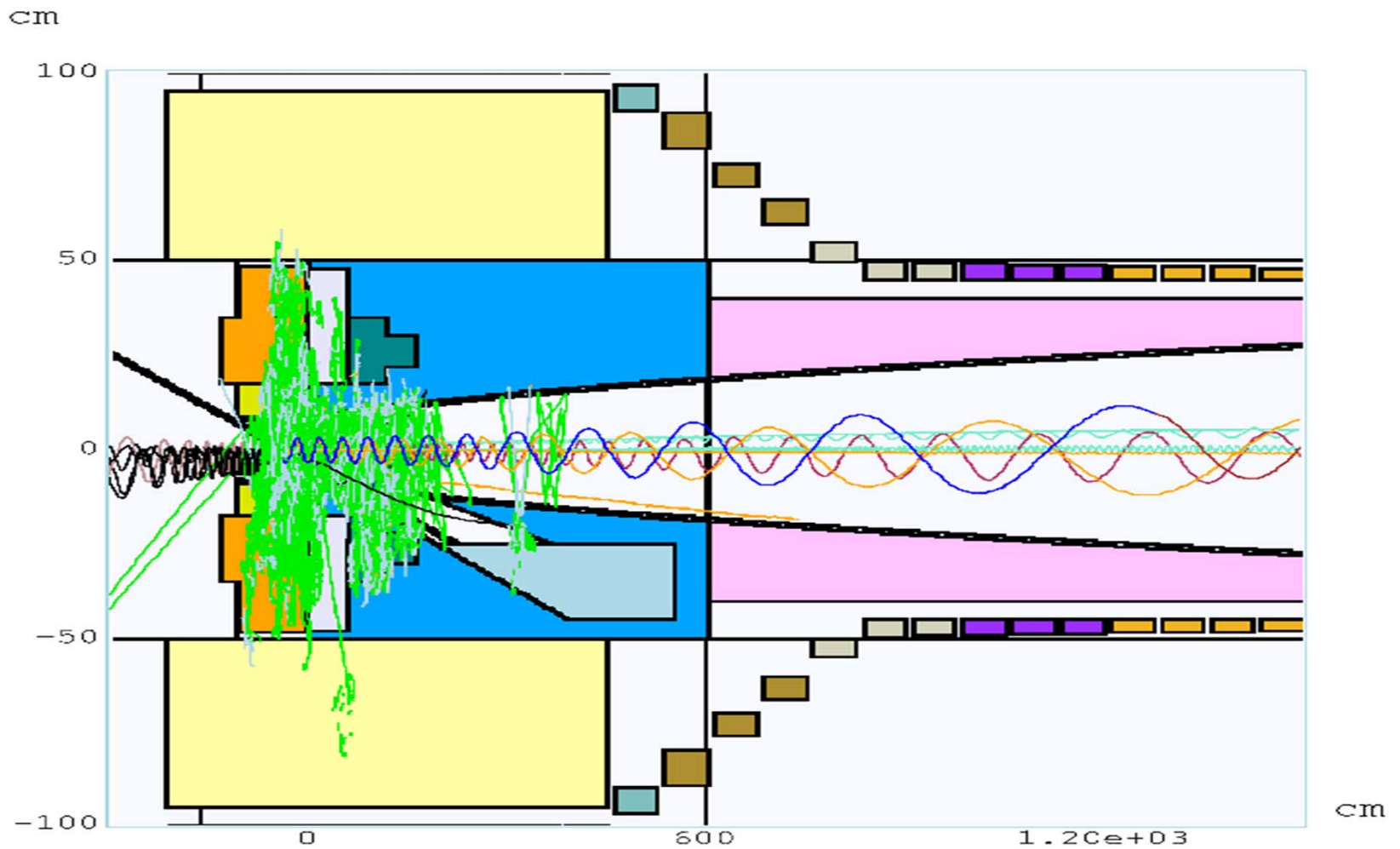


**IDS80f-IDS120f GEOMETRIES:TOTAL ENERGY IN SOLENOIDS (kW)
(semi-log scale).**



IDS100f GEOMETRY: FOR THE FIRST 9 EVENTS

Black=p, Green=n, Red/Blue= π^\pm , Orange/Turquoise= e^\pm , Gray= γ .



Aspect Ratio: Y:Z = 1:9.0

**Energy deposition from:
MARS+MCNP (400K EVENTS) AND FLUKA (100K EVENTS).**

IDS120f GEOMETRY.

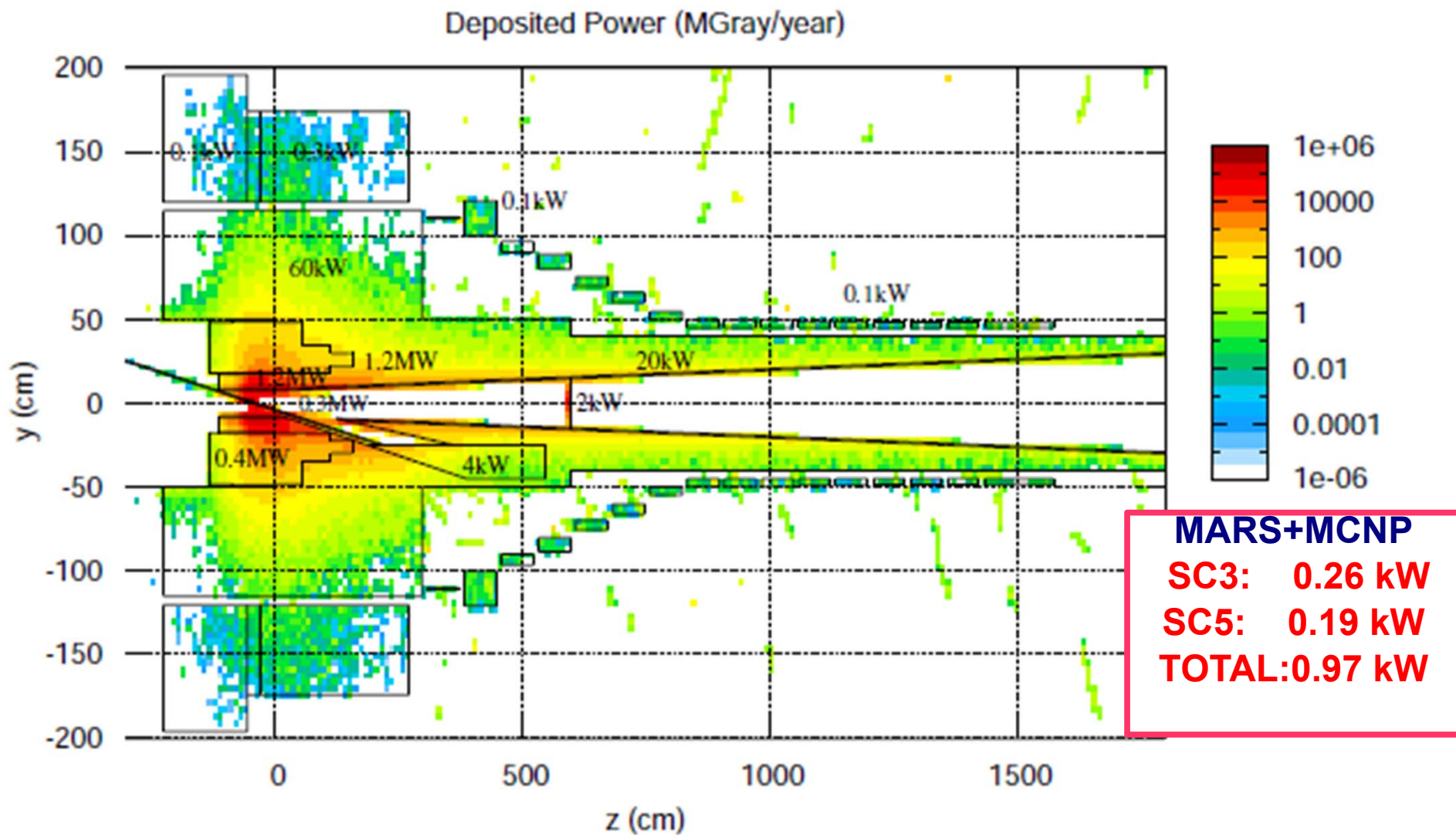
SHIELDING: 60%WC+40% H₂O

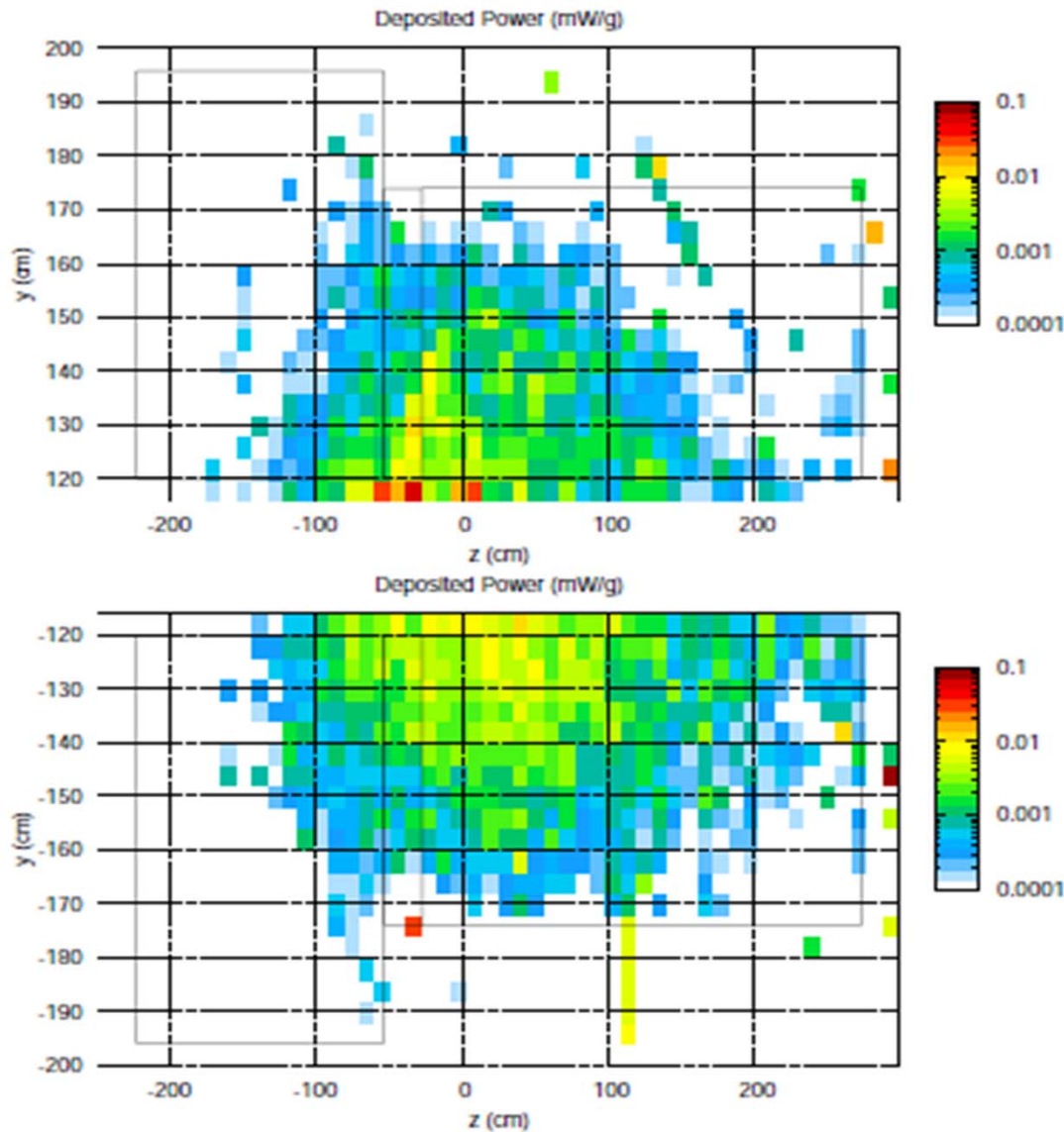
4MW proton beam.

E=8 GeV,

GAUSSIAN PROFILE: $\sigma_x = \sigma_y = 0.12$ cm.

Typical distribution of beam power





Specific power deposition in SC coils 1, 2 & 3

$$P_{\text{peak}} < 0.05 \text{ mW/g for SC3}$$

ITER requirement:
 $P_{\text{peak}} < 0.17 \text{ mW/g}$

MARS+MCNP

Peak SC3: 0.03 mW/gr

SC7: 0.07 mW/gr

SC14: 0.08 mW/gr

ENERGY (IN kW) DEPOSITED IN OTHER PARTS AND TOTALS.

TOTALS	MARS	FLUKA
SC#1-19	0.97	0.56
SH#1-4	2020.06	2148.9
RS#1-5	329.55	405.1
BP#1-3	458.39	482.8
Hg TARG.	376.5	319
Hg POOL	10.16	4.4
Be WIND.	0.53	2.1
TOTAL	3196.16	3362.86

CONCLUSIONS.

- Low energy neutrons require detail study provided by MCNP.
 - High energy neutrons are a problem even with the shielding material.
 - High Z material is required and as much as possible.
 - Additional space to accommodate access to different parts of the target station needed (GEOMETRIES WITHOUT IRON PLUG/YOKE).
 - Additional space for shielding material necessary for solenoids especially around the interaction area (IR \geq 90 cm GEOMETRIES TO REACH ITER CRITERION OF 0.15 mW/gr PEAK ENERGY DENSITY).
 - STUDY II geometry~ 50 kW in SC solenoids, 5.5 mW/gr peak values.
 - IDS120f geometry: <1kW in SC solenoids, <0.08 mW/gr peak values.
- Tolerance for additional necessary components in target station.

MANY THANKS TO THE PEOPLE BEHIND THIS WORK:

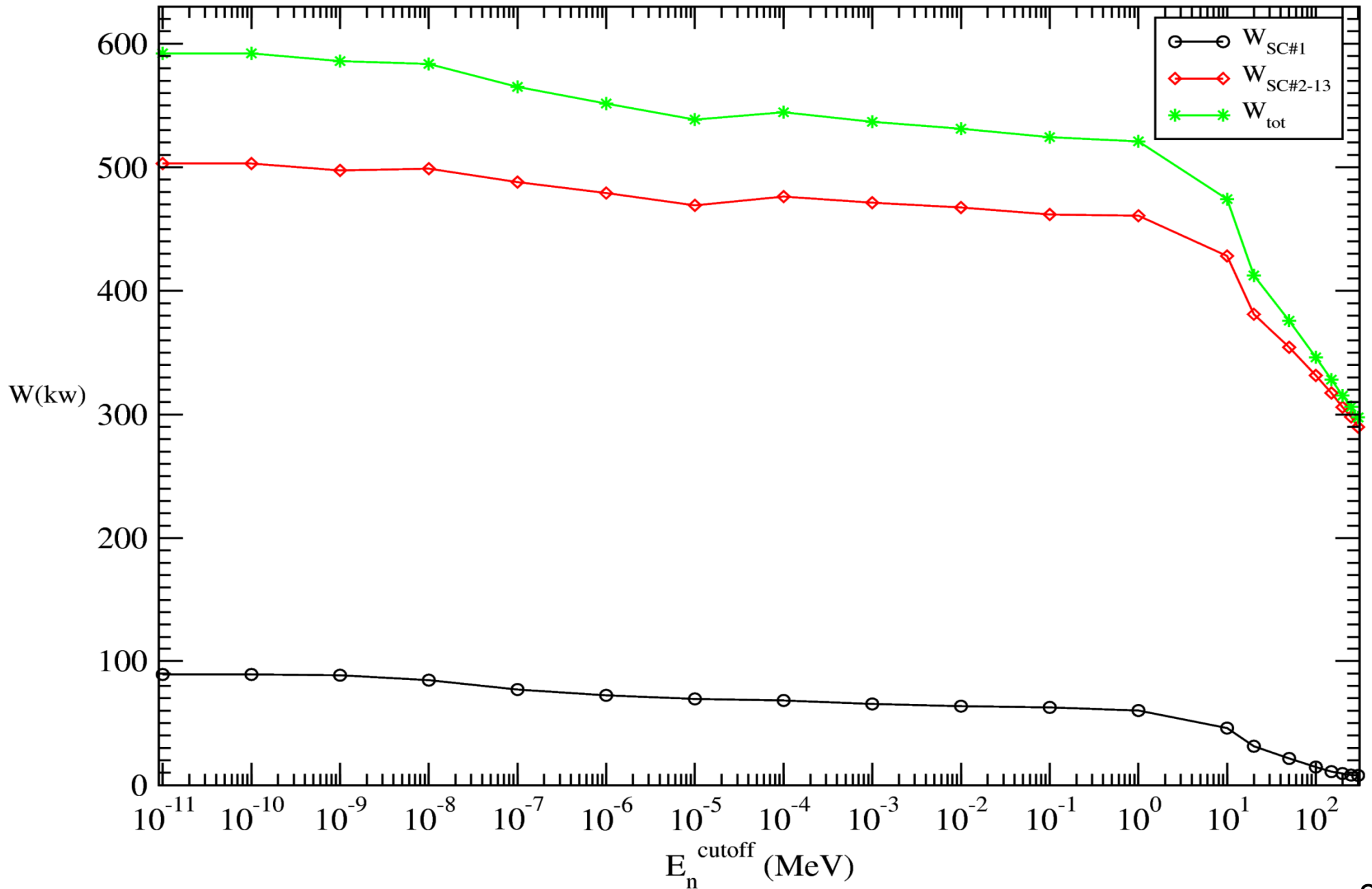
Dr. Harold Kirk, Dr. Kirk McDonald, Dr. Xiaoping Ding,
Dr. Stephen Kahn, Dr. Richard Fernow, Dr. Scott Berg.

BACKUP SLIDES

NO SHIELDING, DIFFERENT NEUTRON ENERGY CUTOFFS.

	$E_n \geq E_i(\text{MeV})$	SC#1	%	SC#2-13	%	Total	%
1	$1 \cdot 10^{-11}$	89.15	-	503.00	-	592.15	-
2	$1 \cdot 10^{-10}$	89.15	0	503.00	0	592.15	0
3	$1 \cdot 10^{-9}$	88.55	-0.67	497.40	-1.11	585.90	-1.06
4	$1 \cdot 10^{-8}$	84.64	-5.06	498.90	-0.82	583.55	-1.45
5	$1 \cdot 10^{-7}$	77.05	-13.57	488.00	-2.98	565.05	-4.58
6	$1 \cdot 10^{-6}$	72.40	-18.79	479.15	-4.74	551.55	-6.85
7	$1 \cdot 10^{-5}$	69.45	-22.10	469.15	-6.73	538.60	-9.04
8	$1 \cdot 10^{-4}$	68.25	-23.44	476.25	-5.32	544.50	-8.05
9	$1 \cdot 10^{-3}$	65.40	-26.64	471.35	-6.29	536.75	-9.36
10	$1 \cdot 10^{-2}$	63.65	-28.60	467.50	-7.06	531.15	-10.30
11*	$1 \cdot 10^{-1}$	62.60	-29.78	461.75	-8.20	524.35	-11.45
12	$1 \cdot 10^0$	60.15	-32.53	460.80	-8.39	520.95	-12.02
13	$1 \cdot 10^{+1}$	45.98	-48.42	428.25	-14.86	474.23	-19.91
14*	$2 \cdot 10^{+1}$	31.35	-64.83	381.10	-24.23	412.45	-30.35
15	$5 \cdot 10^{+1}$	21.54	-75.84	354.30	-29.56	375.84	-36.53
16	$10 \cdot 10^{+1}$	14.60	-83.62	331.60	-34.08	346.20	-41.54
17	$15 \cdot 10^{+1}$	10.89	-87.78	317.30	-36.92	328.19	-44.58
18	$20 \cdot 10^{+1}$	9.33	-89.53	305.90	-39.18	315.23	-46.77
19	$25 \cdot 10^{+1}$	8.13	-90.88	298.00	-40.76	306.13	-48.30
20	$30 \cdot 10^{+1}$	7.81	-91.24	289.80	-42.39	297.61	-49.74

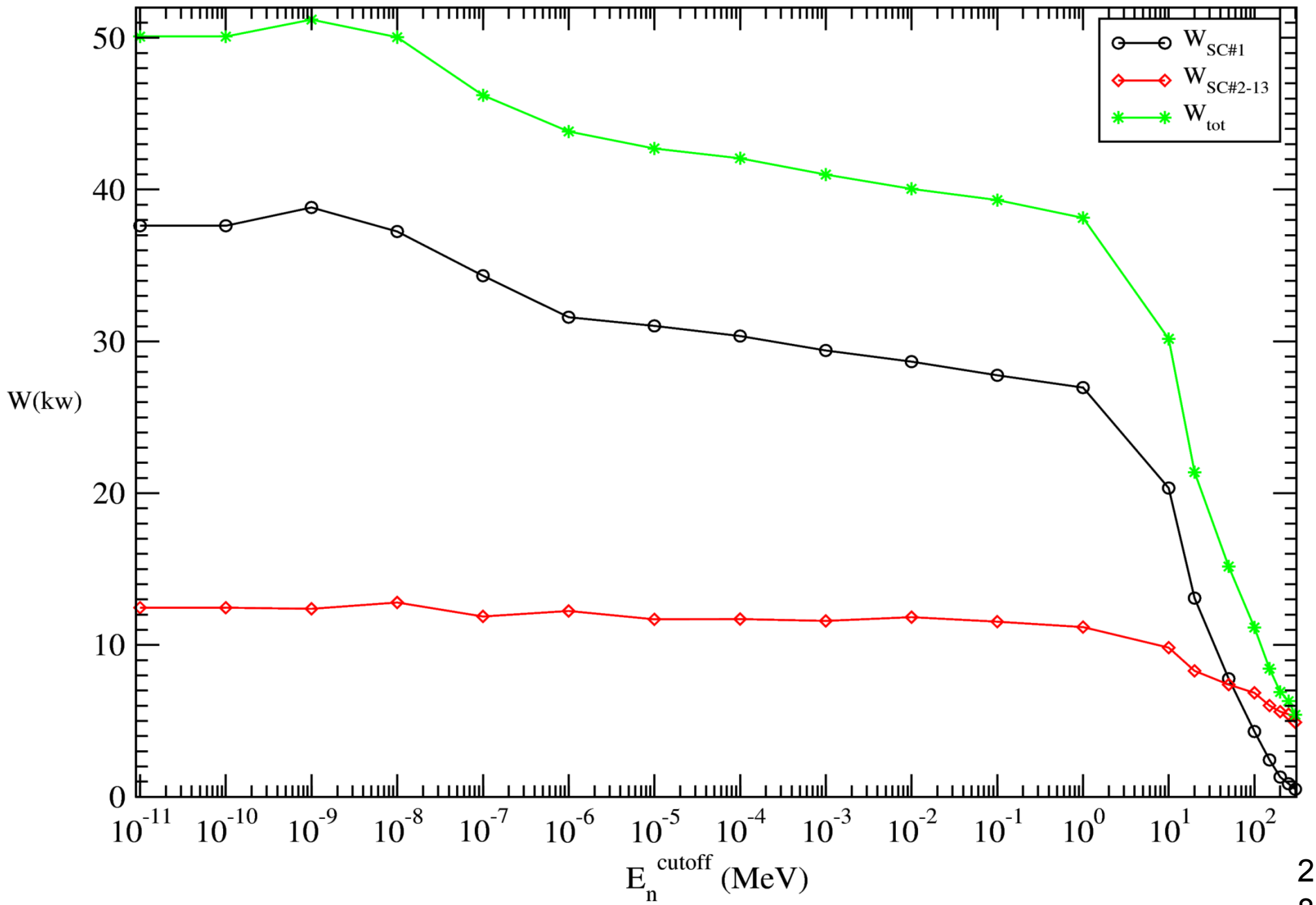
Deposited energy Power for SC#1, SC#2-13 and total, standard geom., different neutron energy cutoffs (10^{-11} to 300 MeV)
(MARS+MCNP) NO SHIELDING, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x = \sigma_y = 0.12$ cm



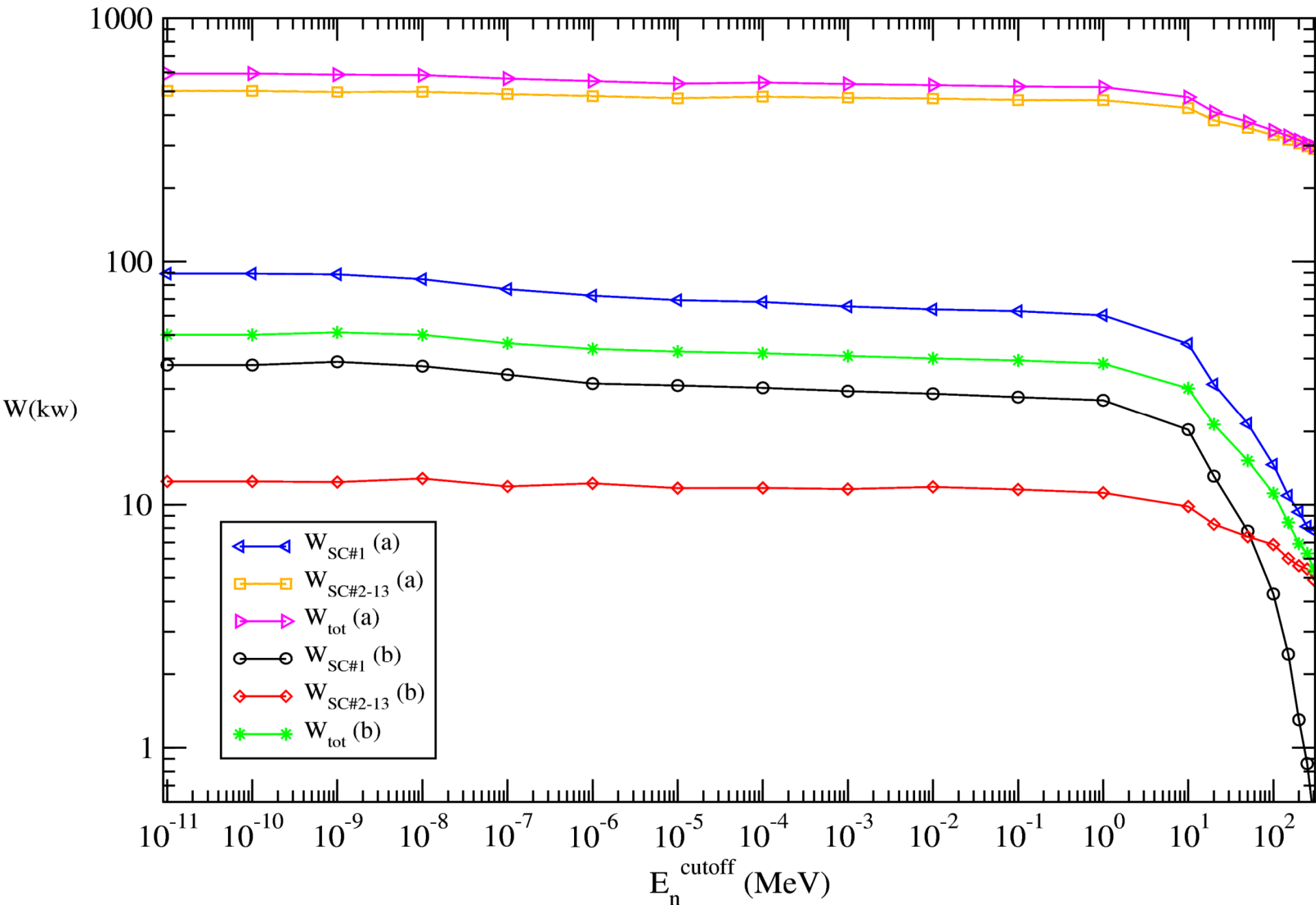
80%WC+20%H₂O SHIELDING, DIFFERENT NEUTRON ENERGY CUTOFFS.

	$E_n \geq E_t$ (MeV)	SC#1	%	SC#2-13	%	Total	%
1	$1 \cdot 10^{-11}$	37.62	-	12.46	-	50.08	-
2	$1 \cdot 10^{-10}$	37.62	0	12.46	0	50.08	0
3	$1 \cdot 10^{-9}$	38.82	+3.19	12.38	-0.64	51.20	+2.23
4	$1 \cdot 10^{-8}$	37.24	-1.01	12.80	+2.73	50.04	-0.08
5	$1 \cdot 10^{-7}$	34.33	-8.75	11.88	-4.65	46.21	-7.72
6	$1 \cdot 10^{-6}$	31.59	-16.03	12.24	-1.77	43.83	-12.48
7	$1 \cdot 10^{-5}$	31.02	-17.54	11.69	-6.17	42.71	-14.71
8	$1 \cdot 10^{-4}$	30.35	-19.32	11.71	-6.02	42.06	-16.01
9	$1 \cdot 10^{-3}$	29.40	-21.85	11.59	-6.98	40.99	-18.15
10	$1 \cdot 10^{-2}$	28.67	-23.79	11.83	-5.06	40.05	-20.03
11*	$1 \cdot 10^{-1}$	27.77	-26.18	11.54	-7.38	39.31	-21.51
12	$1 \cdot 10^0$	26.96	-28.34	11.18	-10.27	38.14	-23.84
13	$1 \cdot 10^{+1}$	20.34	-45.93	9.83	-21.11	30.17	-39.76
14*	$2 \cdot 10^{+1}$	13.09	-65.20	8.30	-33.39	21.39	-57.29
15	$5 \cdot 10^{+1}$	7.78	-79.31	7.39	-40.69	15.17	-69.71
16	$10 \cdot 10^{+1}$	4.30	-88.57	6.85	-45.02	11.15	-77.74
17	$15 \cdot 10^{+1}$	2.43	-93.54	6.01	-51.77	8.44	-83.15
18	$20 \cdot 10^{+1}$	1.30	-96.54	5.61	-54.98	6.91	-86.20
19	$25 \cdot 10^{+1}$	0.86	-97.71	5.44	-46.34	6.30	-87.42
20	$30 \cdot 10^{+1}$	0.50	-98.67	4.90	-60.67	5.40	-89.22

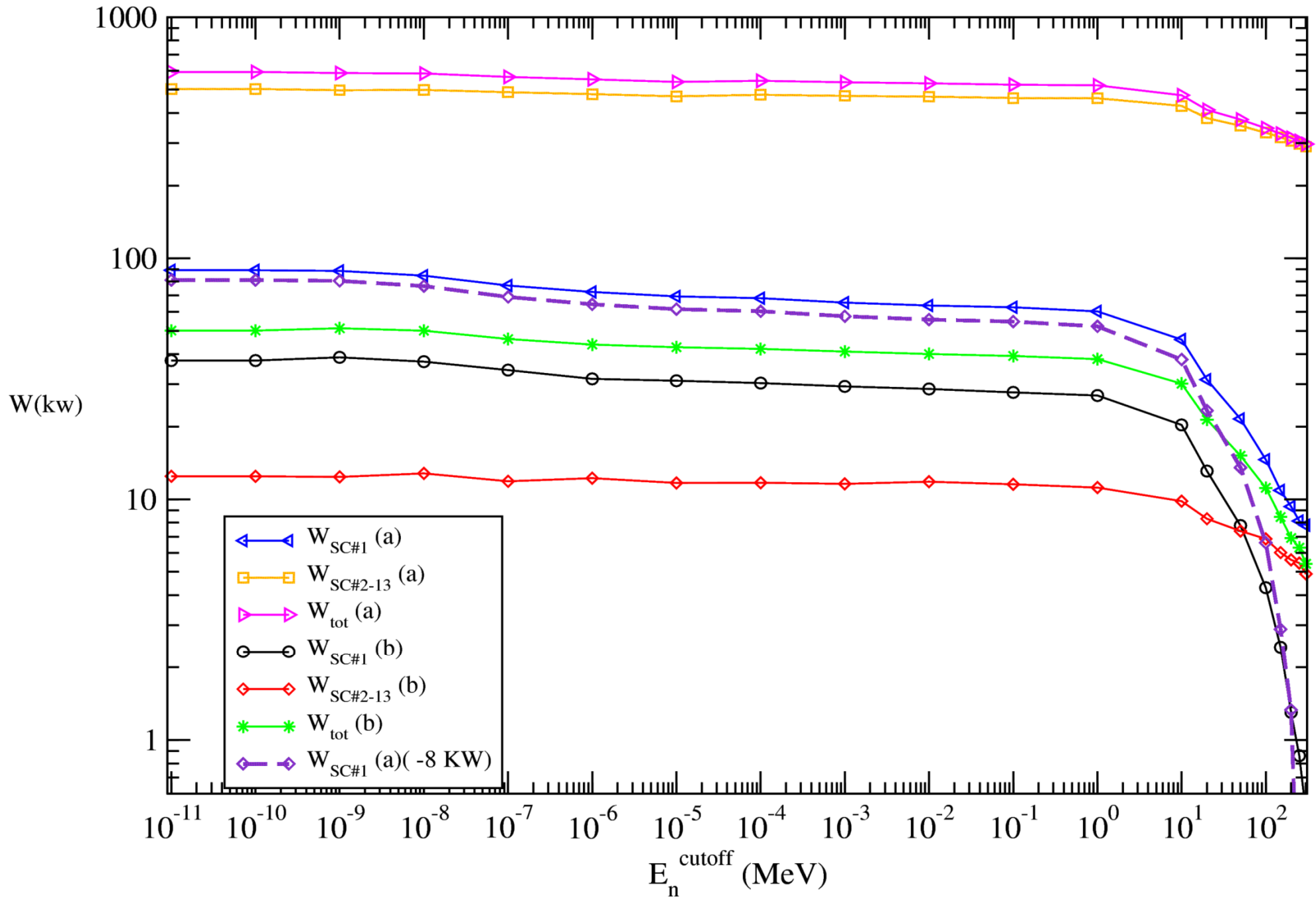
Deposited energy Power for SC#1, SC#2-13 and total, standard geom., different neutron energy cutoffs (10^{-11} to 300 MeV)
(MARS+MCNP) 80% WC+20% H₂O shielding, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x = \sigma_y = 0.12$ cm



Deposited energy Power for SC#1, SC#2-13 and total, standard geom., different neutron energy cutoffs (10^{-11} to 300 MeV)
(MARS+MCNP) a=NO SHIELDING,b=80%WC+20H₂O, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x=\sigma_y=0.12$ cm



Deposited energy Power for SC#1, SC#2-13 and total, standard geom., different neutron energy cutoffs (10^{-11} to 300 MeV)
 (MARS+MCNP) a=NO SHIELDING,b=80%WC+20H₂O, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x=\sigma_y=0.12$ cm



ENERGY DEPOSITED FOR DIFFERENT COMPOSITIONS OF THE SHIELDING (x WC+(1-x) H_2O)

	SHIELDING	ρ (g/cc)	G1	%	G2	%	Total	%
1	0.1% WC+99.9% H_2O	1.0148	58.50	-	262.30	-	320.80	-
2	10% WC+90% H_2O	2.48	49.67		95.20		144.87	
3	20% WC+80% H_2O	3.96	43.06		45.84		88.90	
4	30% WC+70% H_2O	5.44	37.78		27.75		65.53	
5	40% WC+60% H_2O	6.92	35.53		19.87		55.40	
6	50% WC+50% H_2O	8.4	31.38		15.85		46.85	
7	60% WC+40% H_2O	9.88	30.67		13.54		44.21	
8	70% WC+30% H_2O	11.36	28.34		11.85		40.19	
9	80% WC+20% H_2O	12.84	27.77		11.54		39.31	
10	90% WC+10% H_2O	14.32	26.88		10.26		37.14	
11	99.9% WC+0.1% H_2O	15.79	27.25		11.08		38.33	
1C	0.1% WC+99.9% H_2O	1.0148	31.90	-	221.70	-	253.60	-
2C	10% WC+90% H_2O	2.48	25.35		71.10		96.45	
3C	20% WC+80% H_2O	3.96	21.48		31.46		52.94	
4C	30% WC+70% H_2O	5.44	18.77		18.80		37.57	
5C	40% WC+60% H_2O	6.92	17.02		13.79		30.80	
6C	50% WC+50% H_2O	8.4	15.21		10.62		25.83	
7C	60% WC+40% H_2O	9.88	14.10		9.58		23.68	
8C	70% WC+30% H_2O	11.36	13.26		8.98		22.24	
9C	80% WC+20% H_2O	12.84	13.09		8.30		21.39	
10C	90% WC+10% H_2O	14.32	12.45		8.14		20.58	
11C	99.9% WC+0.1% H_2O	15.79	11.95		7.94		19.89	

**DEPOSITED ENERGY BY REMOVING THE MAGNETIC FIELD,
USING TWO WAYS: (4=F, B≠0) (4=T, B=0)**

Table 0.4: (10/23/2010)

YES/NO MAGNETIC FIELD (SET 4=F OR B=(0,0)) (****)
$N_p=100,000$, STANDARD GEOMETRY,13 SC COILS, 2 SC groups:G1=1, G2=2-13
STANDARD SHIELDING WITH: 80% WC+20% H_2O, MARS+MCNP
SOLENOID MATERIALS: SC#1-13=SCON (NiTi+Cu+..)
$E_p=8$ GeV, 4 MW BEAM, $\sigma_x=\sigma_y=0.12$ cm Gaussian distr.
a= $E_n \geq 0.1$ MeV (DEFAULT)
b= $E_n \geq 20$ MeV
c=B FIELD OFF(SET PARAM. 4=F IN THE .INP FILE), $E_n \geq 0.1$ MeV (DEFAULT)
d=B FIELD OFF(SET PARAM. 4=F IN THE .INP FILE), $E_n \geq 20$ MeV
e=B FIELD OFF(SET B=0, 4=T IN THE .INP FILE), $E_n \geq 0.1$ MeV (DEFAULT)
f=B FIELD OFF(SET B=0, 4=T IN THE .INP FILE), $E_n \geq 20$ MeV

Table 0.5: POWER OF DEPOSITED ENERGY IN KW, DW/W %= $((W_x-W_a)/W_a) \times 100$ where x=b,c,e, in d and f are the percentage differences with c and e correspondingly (10/23/2010)

	G1	%	G2	%	Total	%
a	27.77	-	11.54	-	39.31	-
b	13.09	-52.86	8.30	-28.08	21.39	-45.59
c	23.27	-16.20	12.63	+9.45	35.90	-8.67
d	11.06	-52.47	8.88	-29.69	19.94	-44.46
e	22.03	-20.67	12.42	+7.63	34.45	-12.36
f	10.87	-50.66	8.61	-30.68	19.48	-43.45

DEPOSITED ENERGY WHEN RESISTIVE COIL IS REPLACED BY SHIELDING MATERIAL.

Table 0.10: (10/18/2010)

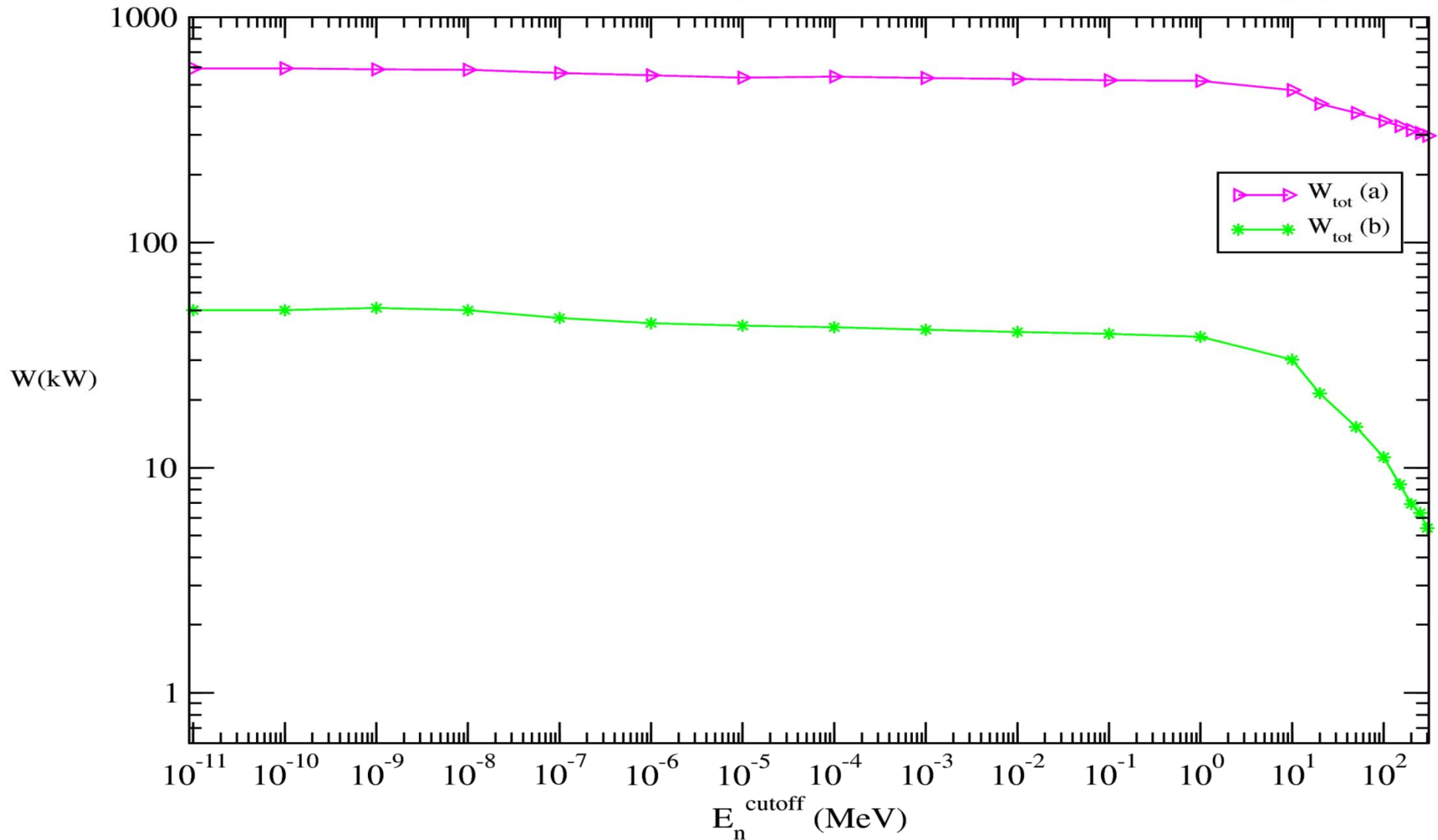
REPLACING RC WITH 80% WC+20% H ₂ O (****)
N _p =100,000 , STANDARD GEOMETRY,13 SC COILS, 2 SC groups:G1=1, G2=2-13
STANDARD SHIELDING WITH: 80% WC+20% H ₂ O, MARS+MCNP
SOLENOID MATERIALS: SC#1-13=SCON (NiTi+Cu+..)
E _p =8 GeV, 4 MW BEAM, σ _x =σ _y =0.12 cm Gaussian distr.
a= E _n ≥0.1 MeV (DEFAULT)
b= E _n ≥20 MeV
c=REPLACING RC WITH 80% WC+20% H ₂ O, E _n ≥0.1 MeV (DEFAULT)
d=REPLACING RC WITH 80% WC+20% H ₂ O, E _n ≥20 MeV

Table 0.11: POWER OF DEPOSITED ENERGY IN KW, DW/W %=((W_x-W_a)/W_a) x100 where x=b,c, in d the percentage difference is with c. (10/18/2010)

	G1	%	G2	%	Total	%
a	27.77	-	11.54	-	39.31	-
b	13.09	-52.86	8.30	-28.08	21.39	-45.59
c	9.83	-64.60	10.45	-9.45	20.28	-48.41
d	4.41	-58.28	7.97	-23.73	12.38	-38.95

OFF/ON SHIELDING, DIFFERENT NEUTRON ENERGY CUTOFFS.

Deposited energy Power total, standard geom., different neutron energy cutoffs (10^{-11} to 300 MeV)
(MARS+MCNP) a=NO SHIELDING,b=80%WC+20H₂O, 8 GeV protons, 4 MW, Gaussian Distribution $\sigma_x=\sigma_y=0.12$ cm



High energy neutrons are a problem even with shielding material.

**Energy deposition from MARS+MCNP.
(10^{-11} MeV NEUTRON ENERGY CUTOFF).**

**IDS80 GEOMETRY WITHOUT IRON PLUG AND YOKE
MATERIAL (TO ACCOMODATE ACCESS TO DIFFERENT
PARTS OF THE TARGET STATION).**

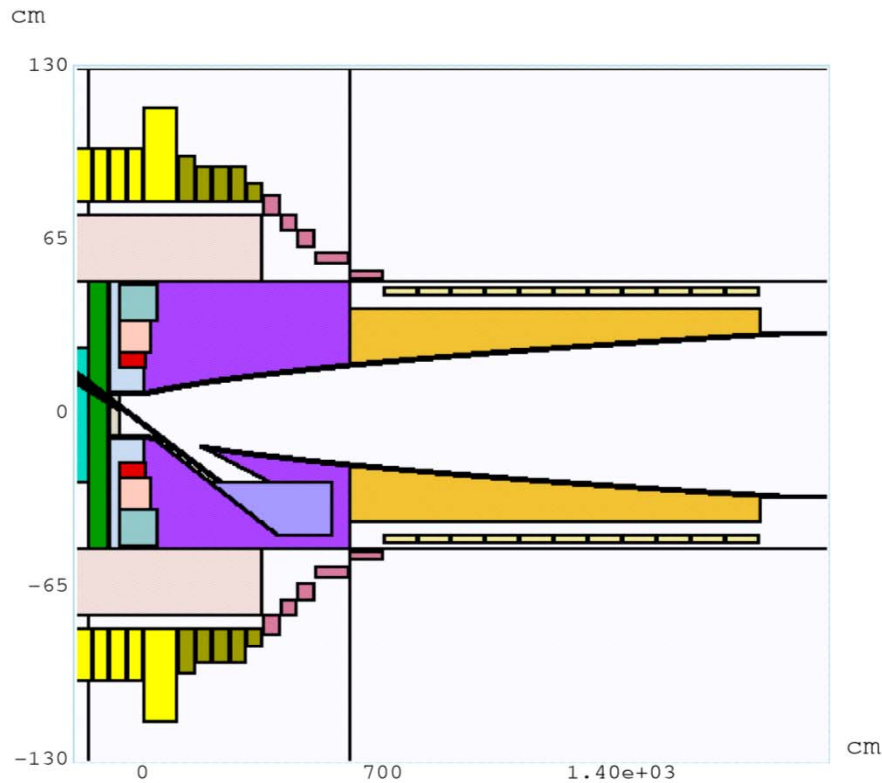
SHIELDING (60%WC+40% H₂O).

4MW proton beam.

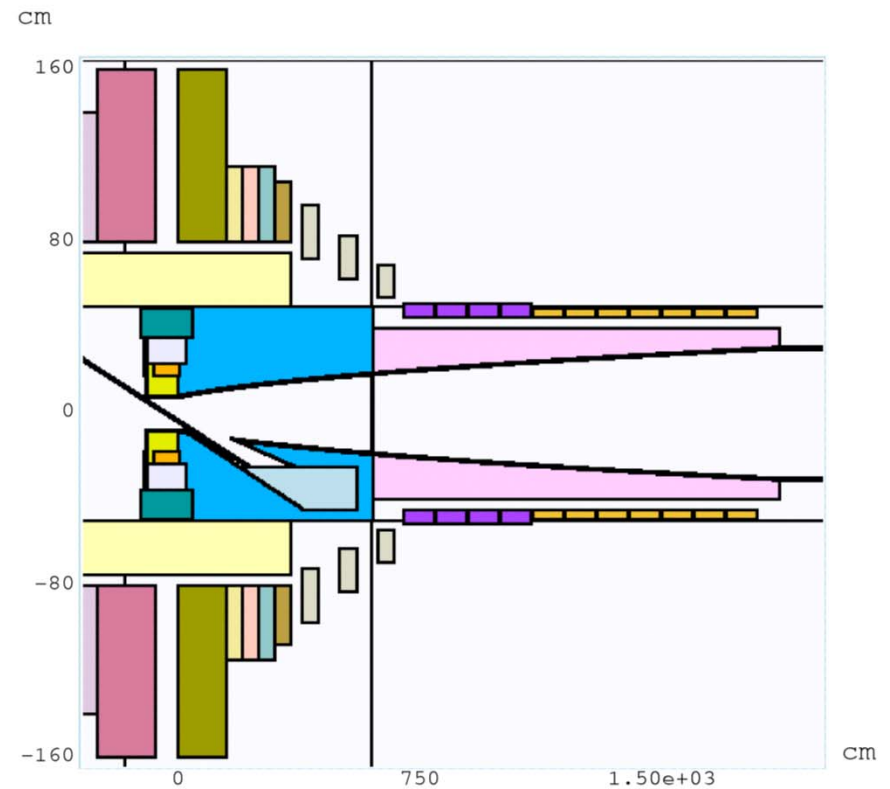
PROTONS ENERGY E=8 GeV.

GAUSSIAN PROFILE: $\sigma_x = \sigma_y = 0.12$ cm.

IDS80 GEOMETRY WITH AND WITHOUT IRON PLUG AND YOKE.



Aspect Ratio: Y:Z = 1:8.46153



: Ratio: Y:Z = 1:6.96969

NEW: SC#1-7 $-300 < z < 345$ cm $R_{in} = 80.0$ cm $R_{out} = 140$ (1)/160 (2,3)/115 (5-6)/108(7) cm (NbSn)
 SC#8-10 $383 < z < 667$ cm $R_{in} = 72/63/54$ cm $R_{out} = 97.0/83/69$ cm (NbTi)
 SC#11-14 $700 < z < 1090$ cm $R_{in} = 45$ cm $R_{out} = 51$ cm (NbTi)
 SC#15-21 $7190 < z < 1090$ cm $R_{in} = 45$ cm $R_{out} = 49$ cm (NbTi) (TOTAL # SC=21)

ENERGY DEPOSITED IN SC SOLENOIDS (SC#), SHIELDING (SH#).

NiSn/NiTi	P(kW)
SC#1	7.48 10^{-4}
SC#2	0.37
SC#3	2.38
SC#4	0.27
SC#5	0.20
SC#6	0.09
SC#7	0.06
SC#1-7	3.37
SC#8-10	0.27
SC#11-14	0.29
SC#15-21	0.18
SC#1-21	4.11

NiSn/NiTi	P(kW)	60/40	P(kW)
SC#1-7	3.37	SH#1	956.0
SC#8-10	0.27	SH#2	1145.0
SC#11-14	0.29	SH#3	37.15
SC#15-21	0.18	SH#4	33.17
SC#1-21	4.11	SH#1-4	2171.32

ENERGY DEPOSITED IN RESISITVE SOLENOIDS (RS#), BEAM PIPE(BP#).

(Cu)	P(kW)	(STST)	P(kW)
RS#1	64.30	BP#1	204.20
RS#2	68.65	BP#2	253.05
RS#3	37.82	BP#3	5.51
RS#1-3	170.77	BP#1-3	462.76

ENERGY DEPOSITED IN OTHER PARTS AND TOTALS:

WITH IRON PLUG

TOTALS	P(kW)
SC#1-26	3.64
SH#1-4	2142.87
RS#1-3	170.80
BP#1-3	453.92
IP#1-3	11.70
Hg TARG.	379.90
Hg POOL	9.32
Be WIND.	0.62
TOTAL	3172.77

WITHOUT IRON PLUG/YOKE

TOTALS	P(kW)
SC#1-21	4.11
SH#1-4	2171.32
RS#1-3	170.77
BP#1-3	462.76
Hg TARG.	374.90
Hg POOL	9.73
Be WIND.	0.53
TOTAL	3194.11

SHIELDING MATERIAL, RESISTIVE COILS, BEAM PIPE, Be WINDOW, MERCURY TARGET AND POOL: ABOUT SAME ENERGY FOR BOTH CASES.