#### A Coupled Level Set/Volume-of-Fluid (CLSVOF) Method for Target Flow Simulation

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# **Outline**

- What is CLSVOF?
- Why CLSVOF?
- How to implement CLSVOF?

## What is CLSVOF?



# Why CLSVOF?



Menard, International Journal of Multiphase Flow, 33, 5 (2007)

# Why CLSVOF?



#### Development of the liquid jet (time step is 2.5 μm) (Menard, 2007)



#### Why CLSVOF?



Liquid jet surface and break-up near the jet nozzle







Liquid parcels

- Couple LS with VOF within the CFD code FLUENT by implementing user defined functions (UDF)
- UDF
	- User written program that can be linked with FLUENT at run-time
	- Programmed in C and FLUENT defined macros
	- User-defined scalar (UDS) transport modeling customize FLUENT for level set equation





B. A. Nichita, 2010, PhD thesis, An improved CFD tool to simulate adiabatic and diabatic two-phase flows

- <span id="page-9-0"></span>• B.A. Nichita's test case
	- A bubble rising in a viscous fluid due to gravity



Level set contour (red) and volume-of-fluid contour (green) without coupling between LS and VOF (with large loss of mass).



 $(t = 0.2s)$ 

Level set contour (red) and volume-of-fluid contour (green) after solving the coupling equation between LS and VOF.

• Setup UDS for LS in FLUENT

Scalar ø Transport Equation

$$
\frac{\partial \rho \phi}{\partial t} + \nabla \cdot (\rho \widetilde{U} \phi) = 0
$$

 $\nabla \cdot (\rho \widetilde{U} \phi)$ 

0

0

∂*t*

∂ρφ

- Unsteady term
- Convection term
- Diffusive term
- Source term

Additional term appear for turbulent flow such as

$$
-\rho \overline{u'_j \phi'} = \Gamma_j \frac{\partial \overline{\phi}}{\partial x_j}
$$

- Setup UDS for LS in FLUENT
	- Set number of UDS
	- Set UDS terms ([Appendix A](#page-9-0))
		- DEFINE\_UDS\_UNSTEADY
			- Get unsteady term for scalar equation
		- DEFINE\_UDS\_FLUX
			- Returns user specified flux
		- DEFINE DIFFUSIVITY
			- Returns user diffusion coefficient (Γ)
		- DEFINE SOURCE
	- Set UDS boundary conditions
		- Constant
		- UDF: DEFINE\_PROFILE

#### Appendix Equations

- Incompressible two-phase flow
	- $\nabla \cdot U = 0$

$$
U_{i} + U \cdot \nabla U = -\frac{\nabla p}{\rho(\phi)} + \frac{1}{\rho(\phi)} \nabla \cdot (2\mu(\phi)D) - \frac{1}{\rho(\phi)} \gamma \kappa(\phi) \nabla H(\phi) + F
$$

$$
\phi_t + U \cdot \nabla \phi = 0
$$

$$
F_{\iota}+\nabla\cdot(UF)=0
$$

Density *ρ*(*Ф*), viscosity *μ* (*Ф*), and curvature *κ* (*Ф*) are written as,

 $|\phi|$  $\kappa(\phi) = \nabla \cdot \frac{\nabla \phi}{\nabla \phi}$  $\mu(\phi) = \mu_{s}(1 - H(\phi)) + \mu_{t}H(\phi)$  $\rho(\phi) = \rho_{\rm g} (1 - H(\phi)) + \rho_{\rm g} H(\phi)$ ∇ ∇  $\overline{(\phi)} = \nabla \cdot$ 

*D* is defined as the rate of deformation tensor

 $D = (\nabla U) + (\nabla U)^{T}$ 

# Appendix Equations

#### • Incompressible two-phase flow

The surface tension force is

$$
\frac{1}{\rho(\phi)}\gamma\kappa(\phi)\nabla H(\phi)
$$

where *H* is the Heaviside function,

 $\lfloor$ ノ<br>〜  $\int 1$  if  $\phi >$ = 0 otherwise.  $H(\phi) = \begin{cases} 1 & \text{if } \phi > 0 \\ 0 & \text{if } \phi > 0 \end{cases}$ 

*F* will be initialized in each computational cell  $\Omega_{ij}$ 

$$
F_{ij} = \frac{1}{\Delta r \Delta z} \int_{\Omega_{ij}} H(\phi(r,z,0)) r dr dz
$$

where  $\Omega_{ii}$  is

$$
\Omega_{ij} = (r, z) | r_i \le r \le r_{i+1} \text{ and } z_j \le z \le z_{j+1}
$$

## Appendix Equations

- Re-Initialization
	- Reinitialize ф

$$
\int_{V} \frac{\partial \phi}{\partial \tau} + \int_{V} w \cdot \nabla \phi = \int_{V} \text{sign } \phi_0
$$

where w is the characteristic velocity pointing outward from the free surface  $w = sign \phi_0 \frac{\nabla \phi}{|\nabla \phi|}$ 

The sign function is

 $sign_{\epsilon}(\phi_0) = 2[H_{\epsilon}(\phi_0) - 1/2]$