

White Paper CSS2013



Neutrinos from STORed Muons

Proposal to the Fermilab PAC

P. Kyberd and D.R. Smith

Brunel University, West London, Uxbridge, Middlesex UB8 3PH, UK

H.A. Tanaka

Department of Physics and Astronomy,

Hennings Building, The University of British Columbia,

6224 Agricultural Road, Vancouver, B.C., V6T 1Z1, Canada

L. Coney and G. Hanson

University of California, Riverside

S. Pascoli

Institute for Particle Physics Phenomenology, Durham University

D. Adey, S.J. Brice, A.D. Bross^a, H. Cease, M. Geelhoed,

T. Kobilarcik, A. Liu^b, N. Mokhov, J. Morfin, D. Neuffer,

S. Parke, M. Popovic, P. Rubinov, T. Sen, and S. Striganov

Fermi National Accelerator Laboratory,

Box 500, Batavia, IL 60510-5011, USA

E. Wildner and L. Sjøby

CERN, CH-1211, Geneva 23, Switzerland

R. Asfandiyarov, A. Blondel, A. Bravar, F. Cadoux, F. Dufour, A. Haesler, Y. Karadzhov,

A. Korzenev, C. Martin, E. Noah, M. Ravonel, M. Rayner, and E. Scantamburlo

University de Geneve, 24, Quai Ernest-Ansermet, 1211 Geneva 4, Suisse

^a Corresponding author: bross@fnal.gov

^b Also at Indiana University Bloomington, 107 S Indiana Ave, Bloomington, IN 47405, USA

R. Bayes and F.J.P. Soler

*School of Physics and Astronomy, Kelvin Building,
University of Glasgow, Glasgow G12 8QQ, Scotland, UK*

P. Snopok^c

Illinois Institute of Technology, Chicago, IL 60616

D. Colling, A. Dobbs, J. Dobson, P. Dornan, M.A. George, A. Kurup,
K. Long, J. Pasternak, E. Santos, J.K. Sedgbeer, M.O. Wascko, and Y. Uchida

*Physics Department, Blackett Laboratory, Imperial College London,
Exhibition Road, London, SW7 2AZ, UK*

S.K. Agarwalla

*Institute of Physics, Sachivalaya Marg,
Sainik School Post, Bhubaneswar 751005, Orissa, India*

A. Cervera, J.J. Gomez-Cadenas, A. Donini, T. Ghosh, P. Hernandez,

A. Izmaylov, A. Laing, O. Mena, M. Sorel, and P. Stamoulis

*Istituto de Fisica Corpuscular (IFIC),
Centro Mixto CSIC-UVEG, Edificio Institutos Investigacin,
Paterna, Apartado 22085, 46071 Valencia, Spain*

L. Stanco

INFN, Sezione di Padova, 35131 Padova, Italy

S.A. Bogacz

Thomas Jefferson National Accelerator Facility

Y. Mori and J.B. Lagrange

Kyoto University

L. Kormos and P. Ratoff

Physics Department, Lancaster University, Lancaster, LA1 4YB, UK

^c Also at Fermi National Accelerator Laboratory, Box 500, Batavia, IL 60510-5011, USA

N. McCauley and C. Touramanis

*Department of Physics, Oliver Lodge Laboratory,
University of Liverpool, Liverpool, L69 7ZE, UK*

J. Evans, S. Soldner-Rembold, and U.K. Yang

*School of Physics and Astronomy, The University of Manchester,
Oxford Road, Manchester, M13 9PL, UK*

J. Kopp

Max-Planck-Institut für Kernphysik, PO Box 103980, 69029 Heidelberg, Germany

C.M. Ankenbrandt^d

Muons Inc., 552 N. Batavia Avenue, Batavia, IL 60510, USA

A. de Gouvêa

Northwestern University

Y. Kuno and A. Sato

Osaka University

V. Blackmore, J. Cobb, C. D. Tunnell^e, and A. Weber

Oxford University, Subdepartment of Particle Physics

K.T. McDonald

Princeton University, Princeton, NJ, 08544, USA

R. Edgecock, W. Murray, S. Ricciardi, and C. Rogers

*STFC Rutherford Appleton Laboratory,
Chilton, Didcot, Oxfordshire, OX11 0QX, UK*

J.A. Hernando Morata

*Universidade de Santiago de Compostela (USC),
Departamento de Física de Partículas,
E-15706 Santiago de Compostela, Spain*

^d Also at Fermilab, P.O. Box 500, Batavia, IL 60510-5011, USA

^e Now at NikHEF, Amsterdam, The Netherlands

C. Booth, P. Hodgson, and P.J. Smith

University of Sheffield, Dept. of Physics and Astronomy, Hicks Bldg., Sheffield S3 7RH, UK

S.R. Mishra

*Department of Physics and Astronomy,
University of South Carolina, Columbia SC 29208, USA*

E. Baussan, M. Dracos, and N. Vassilopoulos

IPHC, Université de Strasbourg, CNRS/IN2P3, F-67037 Strasbourg, France

J. Martin

*Department of Physics, University of Toronto,
60 St. George Street, Toronto, Ontario, M5S 1A7, Canada*

K. Mahn and M.J. Wilking

TRIUMF, 4004 Wesbrook Mall, Vancouver, B.C., V6T 2A3, Canada

R. Nichol

*Department of Physics and Astronomy, University College London,
Gower Street, London, WC1E 6BT, UK*

P. Coloma, P. Huber, J.M. Link, and C. Mariani

*Center for Neutrino Physics, Virginia Polytechnic Institute
and State University. Blacksburg, VA 24061-0435*

J.J. Back, G. Barker, S.B. Boyd, P.F. Harrison, and I.J. Taylor

Department of Physics, University of Warwick, Coventry, CV4 7AL, UK

J.T. Sobczyk

*Institute of Theoretical Physics, University of Wrocław,
pl. M. Borna 9,50-204, Wrocław, Poland*

W. Winter

*Fakultät für Physik und Astronomie, Universität
Würzburg Am Hubland, 97074 Würzburg, Germany*

S. Bhadra and M. Hartz^f

*Department of Physics and Astronomy, York University,
4700 Keele Street, Toronto, Ontario, M3J 1P3, Canada*

(Dated: May 31, 2013)

^f Also at Department of Physics, University of Toronto, 60 St. George Street, Toronto, Ontario, M5S 1A7,
Canada

Contents

1	Executive Summary	3
2	Overview	4
3	Motivation	6
3.1	Sterile neutrinos	6
3.2	Neutrino-nucleus scattering	11
3.3	Technology test-bed	28
4	Facility	30
4.1	Primary proton beam	30
4.2	Target Station	36
4.3	Pion Production	52
4.4	Pion Injection	56
4.5	Decay ring	58
4.6	A future 6D muon ionization cooling experiment	84
5	nuSTORM Conventional Facilities	90
6	Far Detector - SuperBIND	92
6.1	Iron Plates	92
6.2	Magnetization	93
6.3	Detector planes	98
6.4	Photo-detector	100
7	ν Flux at near detector hall	104
7.1	For short-baseline oscillation physics	104
8	Short-Baseline Experiment	105
8.1	Neutrino Flux	105
8.2	Monte Carlo	106

8.3	Data Analysis	108
8.4	Sensitivities	114
8.5	ν_e preliminaries	119
8.6	Neutrino Interaction Study	122
9	Outlook and conclusions	128
9.1	Moving forward	128
9.2	Support request	129
A	Long-Baseline Considerations	131
B	Magnetized Totally Active Detector	133
B.1	Conventional Room Temperature Magnets	134
B.2	Conventional Superconducting Coils	135
B.3	Low Temperature Non-Conventional Superconducting Coils	136
B.4	Superconducting Transmission Line	137
B.5	Conclusions	138

1 Executive Summary

The nuSTORM facility has been designed to deliver beams of $\bar{\nu}_e$ and $\bar{\nu}_\mu$ from the decay of a stored μ^\pm beam with a central momentum of 3.8 GeV/c and a momentum acceptance of 10% [1]. The facility is unique in that it will:

- Allow searches for sterile neutrinos of exquisite sensitivity to be carried out; and
- Serve future long- and short-baseline neutrino-oscillation programs by providing definitive measurements of $\bar{\nu}_e N$ and $\bar{\nu}_\mu N$ scattering cross sections with percent-level precision;
- Constitute the crucial first step in the development of muon accelerators as a powerful new technique for particle physics.

A number of results have been reported that can be interpreted as hints for oscillations involving sterile neutrinos [2–12] (for a recent review see [13]). Taken together, these hints warrant a systematically different and definitive search for sterile neutrinos. A magnetized iron neutrino detector at a distance of $\simeq 2000$ m from the storage ring combined with a near detector placed at a distance of 20 m, identical to it in all respects but fiducial mass, will allow searches for active/sterile neutrino oscillations in both the appearance and disappearance channels. Simulations of the $\nu_e \rightarrow \nu_\mu$ appearance channel show that the presently allowed region can be excluded at the 10σ level while in the ν_e disappearance channel, nuSTORM has the statistical power to exclude the presently allowed parameter space. Furthermore, the definitive studies of $\bar{\nu}_e N$ ($\bar{\nu}_\mu N$) scattering that can be done at nuSTORM will allow backgrounds to be quantified precisely.

The race to discover CP-invariance violation in the lepton sector and to determine the neutrino mass-hierarchy has begun with the recent discovery that $\theta_{13} \neq 0$ [14–18]. The measured value of θ_{13} is large ($\sin^2 2\theta_{13} \sim 0.1$), so measurements of oscillation probabilities with uncertainties at the percent level are required. For future long-baseline experiments to reach their ultimate precision requires that the $\bar{\nu}_e N$ and the $\bar{\nu}_\mu N$ cross sections are known precisely for neutrino energies (E_ν) in the range $0.5 < E_\nu < 3$ GeV. nuSTORM is therefore unique as it makes it possible to measure the $\bar{\nu}_e N$ and the $\bar{\nu}_\mu N$ cross sections with a precision $\simeq 1\%$ over the required neutrino-energy range. At nuSTORM, the flavor composition of the beam and the neutrino-energy spectrum are both precisely known. In addition, the storage-ring instrumentation combined with measurements at a near detector will allow the neutrino flux to be determined to the required precision of 1% or better.

In effect, the unique ν beam available at the nuSTORM facility has the potential to be transformational in our approach to ν interaction physics, offering a “ ν light source” to physicists from a number of disciplines.

Finally, nuSTORM’s unique capabilities offer the opportunity of providing muon beams (simultaneously while running the neutrino program) for future investigations into muon ionization. Muon cooling is the key enabling technology needed for future ultra-high intensity muon accelerator facilities. Its demonstration would be a (the) major step on the path towards realization of a multi-TeV Muon Collider.

2 Overview

The idea of using a muon storage ring to produce a neutrino beam for experiments was first discussed by Koshkarev [19] in 1974. A detailed description of a muon storage ring for neutrino oscillation experiments was first produced by Neuffer [20] in 1980. In his paper, Neuffer studied muon decay rings with E_μ of 8, 4.5 and 1.5 GeV. With his 4.5 GeV ring design, he achieved a figure of merit of $\simeq 6 \times 10^9$ useful neutrinos per 3×10^{13} protons on target. The facility we describe here (nuSTORM) is essentially the same facility proposed in 1980 and would utilize a 3.8 GeV/c muon storage ring with 10% momentum acceptance to study eV-scale oscillation physics, ν_e and ν_μ interaction physics and would provide a technology test bed. In particular the facility can:

- Serve a first-rate neutrino-physics program encompassing:
 - Exquisitely sensitive searches for sterile neutrinos in both appearance and disappearance modes; and
 - Detailed and precise studies of electron- and muon-neutrino-nucleus scattering over the energy appropriate to future long- and short-baseline neutrino oscillation programs; and
- Provide the technology test-bed required to carry-out the R&D critical for the implementation of the next step in a muon-accelerator based particle-physics program.

Unambiguous evidence for the existence of one or more sterile neutrinos would revolutionize the field. nuSTORM is capable of making the measurements required to confirm or refute the evidence for sterile neutrinos using a technique that is both qualitatively and quantitatively new [1]. The nuSTORM facility has been designed to deliver beams of ν_e ($\bar{\nu}_e$) and $\bar{\nu}_\mu$ (ν_μ). A detector located at a distance ~ 2000 m from the end of one of the straight sections will be able to make sensitive searches for the existence of sterile neutrinos. If no appearance ($\bar{\nu}_\mu \rightarrow \bar{\nu}_e$) signal is observed, the LSND allowed region can be ruled out at the $\sim 10\sigma$ level. Instrumenting the nuSTORM neutrino beam with a near detector at a distance of ~ 20 m makes it possible to search for sterile neutrinos in the disappearance $\nu_e \rightarrow \nu_X$ and $\nu_\mu \rightarrow \nu_X$ channels. In the disappearance search, the absence of a signal would permit the presently allowed region to be excluded at the 99% confidence level in our current analysis (see section 8.4.4). For a general discussion of optimization of disappearance searches at short baseline, see [21].

By providing an ideal technology test-bed, the nuSTORM facility will play a pivotal role in the development of accelerator systems, instrumentation techniques, and neutrino detectors. It is capable of providing a high-intensity, high-emittance, low-energy muon beam for studies of ionization cooling and can support the development of the high-resolution, totally-active, magnetized neutrino detectors. The development of the nuSTORM ring, together with the instrumentation required for the sterile-neutrino-search and the νN -scattering programs, will allow the next step in the development of muon accelerators for particle physics to be defined. Just as the Cambridge Electron Accelerator [22], built by Harvard and MIT at the end of the '50s, was the first in a series of electron synchrotrons that culminated in LEP, nuSTORM has the potential to establish a new technique for particle physics that can be developed to deliver the high-energy ν_e ($\bar{\nu}_e$) beams required to elucidate the physics of flavor at the Neutrino Factory and to provide the enabling technologies for a multi-TeV $\mu^+\mu^-$ collider.

nuSTORM itself represents the simplest implementation of the Neutrino Factory concept [23]. In our case, 120 GeV/c protons are used to produce pions off a conventional solid target. The pions are collected

with a magnetic horn and quadrupole magnets and are then transported to, and injected into, a storage ring. The pions that decay in the first straight of the ring can yield a muons that are captured in the ring. The circulating muons then subsequently decay into electrons and neutrinos. We are using a storage ring design that is optimized for 3.8 GeV/c muon momentum. This momentum was selected to maximize the physics reach for both ν oscillation and the cross section physics. See Fig. 1 for a schematic of the facility.

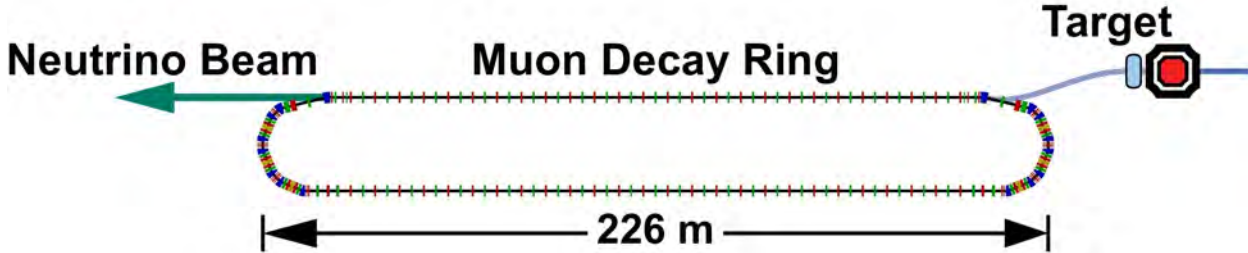


Figure 1: Schematic of the facility

Muon decay yields a neutrino beam of precisely known flavor content and energy. For example for positive muons: $\mu^+ \rightarrow e^+ + \bar{\nu}_\mu + \nu_e$. In addition, if the circulating muon flux in the ring is measured accurately (with beam-current transformers, for example), then the neutrino beam flux is also accurately known. Near and far detectors are placed along the line of one of the straight sections of the racetrack decay ring. The near detector can be placed as close as 20 meters from the end of the straight. A near detector for disappearance measurements will be identical to the far detector, but only about one tenth the fiducial mass. Additional purpose-specific near detectors can also be located in the near hall and will measure neutrino-nucleon cross sections and can provide the first precision measurements of ν_e and $\bar{\nu}_e$ cross sections. A far detector at $\simeq 2000$ m would study neutrino oscillation physics and would be capable of performing searches in both appearance and disappearance channels. The experiment will take advantage of the “golden channel” of oscillation appearance $\nu_e \rightarrow \nu_\mu$, where the resulting final state has a muon of the wrong-sign from interactions of the $\bar{\nu}_\mu$ in the beam. In the case of μ^+ stored in the ring, this would mean the observation of an event with a μ^- . This detector would need to be magnetized for the wrong-sign muon appearance channel, as is the case for the current baseline Neutrino Factory detector [24]. A number of possibilities for the far detector exist. However, a magnetized iron detector similar to that used in MINOS is seen to be the most straight forward and cost effective approach. For the purposes of the nuSTORM oscillation physics, a detector inspired by MINOS, but with thinner plates and much larger excitation current (larger B field) is assumed.

3 Motivation

The case for the nuSTORM facility rests on three themes. First, the neutrino beam, instrumented with a pair of magnetized detectors, near and far, will allow searches for sterile neutrinos of unprecedented sensitivity to be carried out. The signal to background ratio for this combination is of the order ten and is much larger than that in other accelerator-based projects. Second, the uniquely well-known neutrino beam generated in muon decay may be exploited to make detailed studies of neutrino-nucleus scattering over the neutrino-energy range of interest to present and future long and short-baseline neutrino oscillation experiments. In long-baseline experiments, these measurements are required to break the correlation between the cross-section and flux uncertainties and to reduce the overall systematic uncertainty to a level that reinforces the investment in super-beam experiments such as T2HK, LBNE, LBNO and SPL-Frejus. The nuSTORM $\bar{\nu}N$ scattering program is no less important for the next generation of short-baseline experiments for which uncertainties in the magnitude and shape of backgrounds to the sterile-neutrino searches will become critically important. Third, the storage ring itself, and the muon beam it contains, can be used to carry out the R&D program required to implement the next step in the incremental development of muon accelerators for particle physics. The muon accelerator program has the potential to provide elucidation of the physics of flavor at the Neutrino Factory and then to lead to the technological foundation for multi-TeV $\mu^+\mu^-$ collisions at the Muon Collider. The three individually-compelling themes that make up the case for nuSTORM constitute a uniquely robust case for a facility that will be at once immensely productive scientifically and seminal in the creation of a new technique for particle physics.

3.1 Sterile neutrinos

3.1.1 Sterile neutrinos in extensions of the Standard Model

Sterile neutrinos—fermions that are uncharged under the $SU(3) \times SU(2) \times U(1)$ gauge group—are a generic ingredient of many extensions of the Standard Model. Even in models that do not contain sterile neutrinos, they can usually be added easily. For a review of models with sterile neutrinos and the associated phenomenology see [13].

One important class of sterile neutrino theories are models explaining the smallness of neutrino masses by means of a seesaw mechanism. In its simplest form, the seesaw mechanism requires at least two heavy ($\sim 10^{14}$ GeV) sterile neutrinos that would have very small mixings ($\sim 10^{-12}$) with the active neutrinos. However, in slightly non-minimal models, at least some sterile neutrinos can have much smaller masses and much larger mixing angles. Examples for such non-minimal scenarios include the split seesaw scenario [25], seesaw models with additional flavor symmetries (see e.g. [26]), models with a Froggatt-Nielsen mechanism [27, 28], and extended seesaw models that augment the mechanism by introducing more than three singlet fermions, as well as additional symmetries [29–31].

Also Grand Unified Theories (GUTs) can contain Standard Model singlet fermions. In GUTs, fermions are grouped into multiplets of an extended gauge group, for instance $SU(5)$ or $SO(10)$, which has $SU(3) \times SU(2) \times U(1)$ as a subgroup. If the multiplets are larger than needed to accommodate the Standard Model fermions, there will be extra states that will behave like gauge singlets after the GUT symmetry is broken (see for instance [32–35] for GUT models with sterile neutrinos).

Finally, sterile neutrinos arise naturally in “dark sector” models, which contain a group of particles that has nontrivial dynamics of its own, but is only very weakly coupled to the Standard Model particles. If this dark sector is similar to the visible sector—as is the case, for instance, in string-inspired $E_8 \times E_8$ models—it is natural to assume that it also contains neutrinos [36–38], which would appear sterile from a Standard Model point of view.

3.1.2 Experimental hints for light sterile neutrinos

Besides their generic appearance in extended theoretical models, much of the current interest in sterile neutrinos is motivated by experimental results. In fact, several neutrino oscillation experiments have observed deviations from the best available Standard Model predictions and can be interpreted as hints for oscillations involving light sterile neutrinos with masses of order eV.

The most long-standing of these hints is the result from the **LSND** experiment, which studied short-distance $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ oscillations at a baseline of ~ 30 m [2]. A flux of low-energy ($\lesssim 50$ MeV) muon antineutrinos was produced in the decay of stopped pions, $\pi^+ \rightarrow \mu^+ \nu_\mu$, followed by muon decay $\mu^+ \rightarrow e^+ \bar{\nu}_\mu \nu_e$. In the Neutrino Standard Model, neutrinos of this energy are not expected to oscillate over distances as short as the LSND baseline. The detection process for electron antineutrinos in LSND was inverse beta decay, $\bar{\nu}_e p \rightarrow e^+ n$, in a liquid scintillator detector. Backgrounds to the neutrino oscillation search arise from the decay chain $\pi^- \rightarrow \bar{\nu}_\mu + (\mu^- \rightarrow \nu_\mu \bar{\nu}_e e^-)$, if negative pions produced in the target decay before they are captured by a nucleus, and from the reaction $\bar{\nu}_\mu p \rightarrow \mu^+ n$, which is only allowed for the small fraction of muon antineutrinos produced by pion decay *in flight* rather than stopped pion decay. LSND reports an excess of $\bar{\nu}_e$ candidate events above this background with a significance of more than 3σ . When interpreted as $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ oscillations through an intermediate sterile state $\bar{\nu}_s$, this result is best explained by sterile neutrinos with an effective mass squared splitting $\Delta m^2 \gtrsim 0.1$ eV² relative to the active neutrinos, and with an effective sterile sector-induced $\bar{\nu}_\mu$ – $\bar{\nu}_e$ mixing angle $\sin^2 2\theta_{\mu e} \gtrsim 2 \times 10^{-3}$, depending on Δm^2 .

A second possible hint for oscillations involving sterile neutrinos is provided by the **MiniBooNE experiment** [39], which was designed to test the neutrino oscillation interpretation of the LSND result. MiniBooNE uses higher-energy (200 MeV–few GeV) neutrinos from a horn-focused pion beam. By focusing either positive or negative pions, MiniBooNE can switch between a beam dominated by ν_μ and a beam dominated by $\bar{\nu}_\mu$. In both modes, the experiment observed an excess of electron-like events at sub-GeV energies. The excess has a significance above 3σ and can be interpreted in terms of $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ oscillations consistent with the LSND observation [39].

While the $\nu_\mu \rightarrow \nu_e$ and $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ oscillation channels in which LSND and MiniBooNE observe excesses are sensitive to transitions between active neutrino flavors mediated by sterile states, sterile neutrinos can also manifest themselves in the disappearance of active neutrinos into sterile states. In fact, such anomalous disappearance may have been observed in reactor experiments. A larger number of such experiments has been carried out in the past, and while their results were consistent with the flux predictions available at the time [40], they are in conflict with more accurate recent re-evaluations of the reactor antineutrino flux [5, 6]. In particular, the average $\bar{\nu}_e$ event rate is about 6% lower than the current prediction [7, 13], which has a stated uncertainty of 2–3%. The significance of the deficit depends crucially on the systematic uncertainties associated with the theoretical prediction, some of which are difficult to estimate. If the **reactor antineutrino anomaly** is interpreted as $\bar{\nu}_e \rightarrow \bar{\nu}_s$ disappearance via oscillation, the required 2-flavor oscillation

parameters are $\Delta m^2 \gtrsim 0.3 \text{ eV}^2$ and $\sin^2 2\theta_{ee,\text{eff}} \sim 0.1$.

Interestingly, active-to-sterile neutrino oscillations with these parameters can also explain another experimental result, often referred to as the **gallium anomaly**. It is based on measurements by the GALLEX and SAGE solar neutrino experiments which have used ν_e from intense artificial radioactive sources to demonstrate the feasibility of their radiochemical detection method [8–12]. Both experiments observed fewer neutrinos from the source than expected. The statistical significance of the deficit is around 3σ and can be interpreted in terms of short-baseline $\bar{\nu}_e \rightarrow \bar{\nu}_s$ disappearance with $\Delta m^2 \gtrsim 1 \text{ eV}^2$ and $\sin^2 2\theta_{ee,\text{eff}} \sim 0.1$ – 0.8 . [41, 42].

3.1.3 Constraints and global fit

In spite of the interesting hints from four short baseline oscillation experiments, the existence of light sterile neutrinos is far from established. The most important reason is that other short baseline experiments did not observe a signal and place strong constraints on the available sterile neutrino parameter space. The compatibility of the signals from LSND, MiniBooNE, reactor and gallium experiments with null results from a large number of other experiments is assessed in global fits [13, 42–49]. The results from one of these fits [49] are shown in Fig. 2.

We see that there is significant tension in the global data set: The parameter region favored by LSND, MiniBooNE, reactor and gallium experiments is incompatible, at the 99% confidence level, with exclusion limits from other experiments (left panel of figure 2). Similarly, the combination of all $\bar{\nu}_e$ appearance data is in conflict with the $\bar{\nu}_\mu$ and $\bar{\nu}_e$ disappearance data (right panel of figure 2). Quantifying this disagreement with a parameter goodness of fit test [88] yields p-values of order 10^{-4} [49]. (Note that different authors find different levels of tension between appearance and disappearance data [45, 48, 49]. The reason for the differences between global fits lie in the choice of data sets included and in the details of the fits to individual experimental data sets.) It is difficult to resolve this tension even in models with more than one sterile neutrino.

It is important to note that in spite of the tension in the global fit, the different appearance data sets are compatible with each other (Fig. 3, left), as are the disappearance data sets among themselves (Fig. 3, right). This implies in particular that an explanation of the reactor and gallium anomalies in terms of sterile neutrinos is perfectly viable. Also, $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ transitions with parameters suitable for explaining LSND and MiniBooNE are not directly ruled out by other experiments measuring the same oscillation channels. It is only when appearance and disappearance signals are related through the equation

$$\sin^2 2\theta_{\mu e} = 4|U_{e4}|^2|U_{\mu4}|^2 \quad (1)$$

that the tension appears. Here, $\theta_{\mu e}$ is the effective mixing angle governing $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ transition in LSND and MiniBooNE, and U_{e4} , $U_{\mu4}$ are the elements of the leptonic mixing matrix describing mixing between electron neutrinos and sterile neutrinos, and between muon neutrinos and sterile neutrinos, respectively.

Possible solutions to the tension between positive hints and null results are:

1. One or several of the apparent deviations from the standard three neutrino oscillation framework discussed in Section 3.1.2 have explanations not related to sterile neutrinos.
2. One or several of the null results that favor the no-oscillation hypothesis are in error.

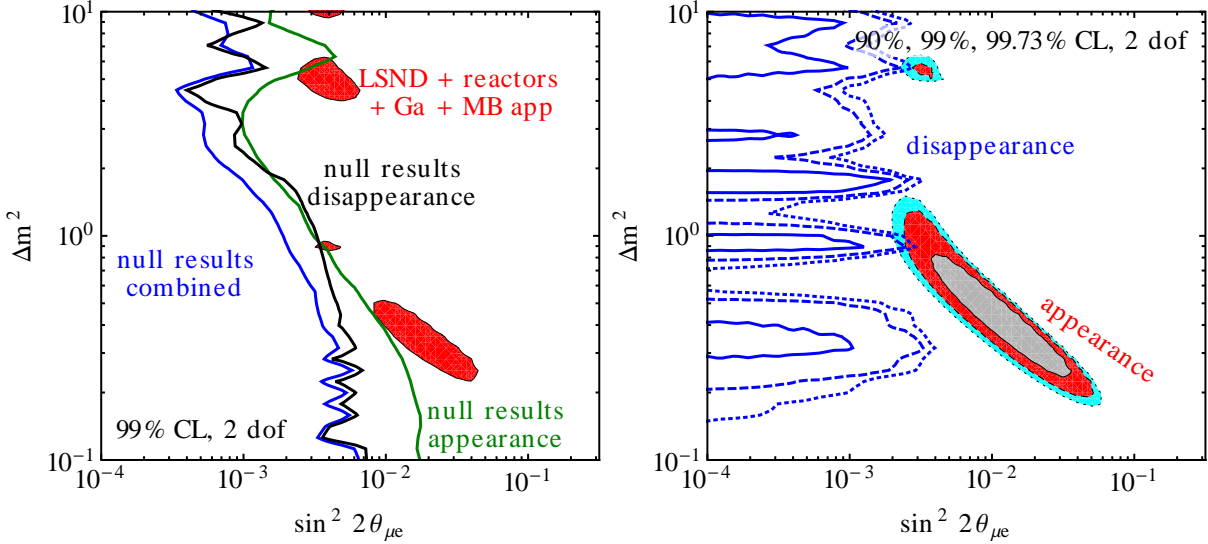


Figure 2: Global constraints on sterile neutrinos in a 3+1 model. In the left panel, we show that $\bar{\nu}_e$ appearance data (colored region: LSND [2], MiniBooNE [39], KARMEN [50], NOMAD [51], E776 [52], ICARUS [53]) is only marginally consistent with disappearance data (blue contours: atmospheric neutrinos [54], solar neutrinos [55–64], MiniBooNE/SciBooNE [65, 66] MINOS [67, 68], reactor experiments [15, 69–79], CDHS [80], KARMEN [81] and LSND [82] ν_e - ^{12}C scattering data and gallium experiments [9, 11, 12, 56]). In the right panel, we compare those experiments which see unexplained signals (LSND, MiniBooNE appearance measurements, reactor experiments, gallium experiments) to those which do not. For the analysis of reactor data, we have used the new reactor flux predictions from [5], but we have checked that the results, especially regarding consistency with LSND and MiniBooNE $\bar{\nu}$ data, are qualitatively unchanged when the old reactor fluxes are used. Fits have been carried out in the GLOBES framework [83, 84] using external modules discussed in [49, 85–87]. Plots taken from ref. [49].

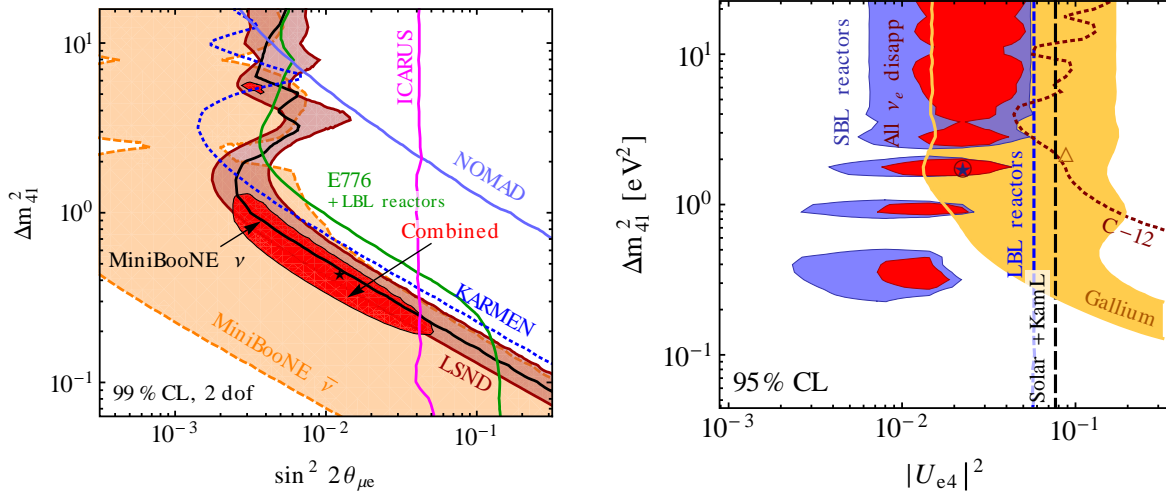


Figure 3: Global constraints on $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ oscillations (left) and on $\bar{\nu}_e$ disappearance (right). These subsets of the globally available data are found to be consistent, and it is only when they are combined, and when, in addition, exclusion limits on $\bar{\nu}_\mu$ disappearance are included, that tension appears. Plots taken from ref. [49].

3. There are sterile neutrinos plus some other kind of new physics at the eV scale. (See for instance [87, 89] for an attempt in this direction.)

3.1.4 Sterile neutrinos in cosmology

Important constraints on sterile neutrino models come from cosmology, which is sensitive to the effective number N_{eff} of thermalized relativistic species in the Universe at the time of Big Bang Nucleosynthesis (BBN) and at the time of recombination. Moreover, cosmological observations constrain the sum of neutrino masses. The most recent Planck data [90] yields $N_{\text{eff}} = 3.30^{+0.54}_{-0.51}$ when combined with polarization data from WMAP [91], high-multipole measurements from ACT [92] and SPT [93, 94] and data on baryon acoustic oscillations (BAO) [95–98]. The sum of neutrino masses is constrained by the same data to be below 0.23 eV. While the exact strength of exclusion depends on which cosmological data sets are analyzed, the general conclusion remains the same: cosmology after Planck is consistent with only the standard three neutrino flavors, but the existence of additional thermalized neutrino species is not ruled out. On the other hand, these extra species should have masses significantly below 1 eV, too low to explain the short-baseline anomalies. However, the Planck limit on the effective relativistic degrees of freedom are weakened if one includes the current best fit data for the Hubble constant.

It is important to keep in mind that cosmological bounds apply only to neutrino species that come into thermal equilibrium in the early Universe, usually through oscillations. Hence, if oscillations between active and sterile neutrinos are suppressed at early times, these limits are avoided (see [48, 99] for recent combined fits of cosmology and short baseline oscillation data). A suppression of active–sterile neutrino oscillations can occur if there is a very large primordial lepton asymmetry (see for instance [100, 101] for recent studies) or in Majoron models [102, 103]. Other scenarios in which eV scale sterile neutrinos can be consistent with cosmology include phenomenological non-standard extensions of Λ CDM cosmology [104], scenarios with

very low reheating temperature [105], certain types of $f(R)$ gravity [106], and models with additional heating mechanisms for the primordial plasma after neutrino decoupling (see for instance [107]).

We conclude that, given the current experimental situation, it is impossible to draw firm conclusions regarding the existence of light sterile neutrinos. There is on the one hand an intriguing accumulation of experimental anomalies that could be interpreted in the context of sterile neutrino models, while on the other hand, it seems difficult to accommodate all these hints simultaneously, given strong constraints from experiments with null results. An experiment searching for short-baseline neutrino oscillations with good sensitivity and well-controlled systematic uncertainties has great potential to clarify the situation by either finding a new type of neutrino oscillation or by deriving a strong and robust constraint on any such oscillation. While the former outcome would constitute a major discovery, the latter one would also certainly receive a lot of attention since it would provide the world’s strongest constraints on a large variety of theoretical models postulating “new physics” in the neutrino sector at the eV scale. A truly definitive experiment for both the muon appearance and muon disappearance channels is required to reach a convincing conclusion on the existence of light, sterile neutrinos.

3.2 Neutrino-nucleus scattering

3.2.1 Introduction

Recent interest in neutrino interactions in the few GeV energy region comes from neutrino oscillation experiments and their need to reduce systematic errors. Cross section measurements have been performed by neutrino oscillation collaborations in the past, with T2K currently carrying on this tradition. Importantly, there is a dedicated cross section experiment (MINERvA) currently underway and others using LAr detectors (MicroBooNE) planned for the near future at Fermilab.

Even with this degree of activity, the precision with which the basic neutrino-*nucleon* cross sections are known is still not better than 20 – 30%. There are two main reasons for this: the poor knowledge of neutrino fluxes and the fact that all the recent cross section measurements have been performed on nuclear targets. It is important to recall that what current neutrino experiments are measuring are events that are generated from a convolution of energy-dependent neutrino flux \otimes energy-dependent cross section \otimes energy-dependent nuclear effects. The experiments have, for example, then measured an effective neutrino-carbon cross section. To extract a neutrino-*nucleon* cross section from these measurements requires separation of nuclear physics effects, which can only be done with limited precision. For many oscillation experiments, using the same nuclear targets for their near and far detectors is a good start. However, even with the same nuclear target near-and-far, that there are different near and far neutrino energy spectra due to beam geometry and oscillations means there is a different convolution of cross section \otimes nuclear effects near-and-far and there is no automatic cancellation between the near-and-far detectors. For a thorough comparison of measured neutrino-nucleon cross sections with theoretical models, these convoluted effects have to be understood. For further details please see [108]. This section will summarize the current status of both theoretical and experimental studies of neutrino nucleus scattering with an emphasis on what nuSTORM, with its superior knowledge of the neutrino flux and its high-intensity source of electron-neutrinos, can contribute.

For neutrino-*nucleon* interactions one can distinguish: Charged Current quasi-elastic (CCQE), Neutral Current elastic (NCEl), Resonance production (RES) and more inelastic reactions involving pion produc-

tion from the Δ through the transition region up to the deep-inelastic (a rather misleading "DIS" term is often used to describe all the interactions which are neither CCQE/NCEI nor RES) domain. Quite different theoretical tools are used to model each of them. The expected distribution of nuSTORM events among the various scattering channels as well as the expected event rates are shown in Fig. 4. For neutrinos the expected distribution is 56% resonant, 32% quasi-elastic and 12 % DIS with event energy peaking at about 2.5 GeV. For anti-neutrinos the breakdown is 52% resonant, 40% quasi-elastic and 8 % DIS.

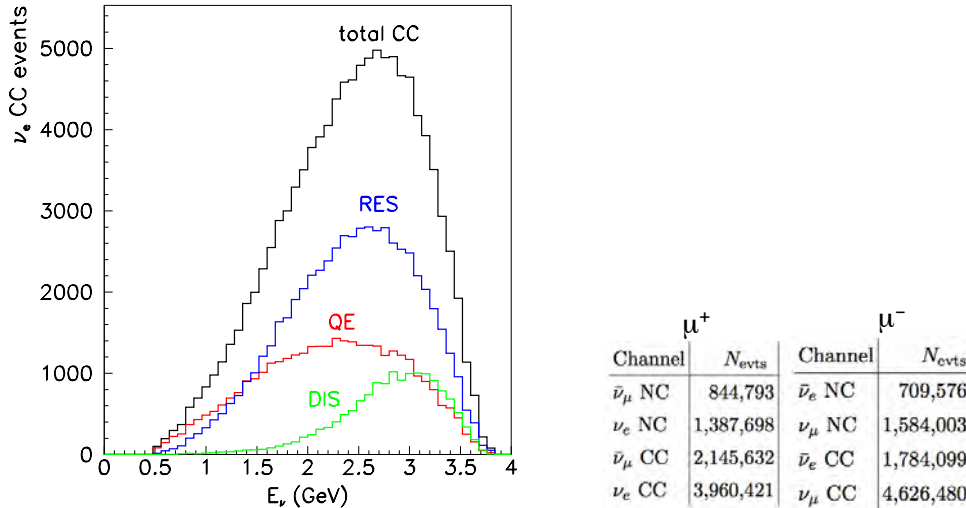


Figure 4: Left: The breakdown of scattering channels for a nuSTORM ν_μ or ν_e beam circulating 3.8 GeV/c muons. Right: The expected event rates for ν and $\bar{\nu}$ for both μ^+ and μ^- circulating beams and a 100 fiducial ton detector located 50 m from the straight. The exposure is 10^{21} POT.

From the experimental point of view it is most natural to speak about events in terms of the visible final state topology; that is, events with no pions in the final state or with only one pion above a given momentum threshold, and so on. In fact, in several recent experimental measurements that investigated quantities defined in this way, the dependence on assumptions of Monte Carlo event generators were minimal. To compare with the experimental data given in this format, one must add contributions from various dynamical mechanisms and also model Final State Interactions (FSI) effects. Several ingredients of the theoretical models are verified simultaneously. It is clear that in order to validate a model one needs many samples of precise neutrino-nucleus scattering measurements on a variety of nuclear targets with various neutrino fluxes.

3.2.2 Charged Current quasi-elastic

The simplest neutrino hadronic reaction is the charge current quasi-elastic (CCQE) interaction: $\nu_\ell + n \rightarrow \ell^- + p$ with two particles: a charged lepton and proton in the produced state and the antineutrino analog state that involves a neutron instead of a proton in the produced state. We need to extend this definition to the neutrino-nucleus interaction occurring on bound nucleons. The ejected proton is not necessarily seen in a detector because quite often its momentum is below the acceptance threshold. However, events with a single reconstructed charged lepton track can result from a variety of initial interactions e.g. from a two body charged current interaction or from real pion production and its subsequent absorption. Similar problems

arise in other type of interactions. It is becoming clear that interpretation of neutrino-nucleus interactions must rely on a careful data/Monte Carlo (MC) comparison done with reliable MC neutrino event generators.

In the case of neutrino nucleus scattering we also use the term CCQE-like reaction to define one in which there are no pions in the final state. It then includes events with real pion production followed by absorption. It also includes interactions on bound-nucleon systems (np-nh or meson-exchange current) which will be discussed shortly.

A theoretical description of the free nucleon target CCQE reaction is based on the conserved vector current (CVC) and the partially conserved axial current (PCAC) hypotheses. The only unknown quantity is the nucleon axial form-factor $G_A(Q^2)$ for which one typically assumes a dipole form $G_A(0)(1 + \frac{Q^2}{M_A^2})^{-2}$ with one free parameter, the axial mass M_A . This dipole form is an assumption which need not hold. Non-dipole form factors are being investigated in [109].

In the past, several measurements of M_A were performed on a deuterium target for which most of nuclear physics complications are minimal and it seemed that the results converged to a value of the order of 1.03 GeV [110]. There is an additional argument in favor of a similar value of M_A coming from the weak pion-production at low Q^2 . A PCAC based evaluation gives an axial mass value of 1.077 ± 0.039 GeV [111]. On the other hand, all of the more recent high statistics measurements of M_A , with the exception of the NOMAD higher-energy experiment, reported larger values, with the MiniBooNE (carbon, $Q^2 > 0$ GeV²) determination of 1.35 ± 0.17 [112] compared to the NOMAD (carbon, $Q^2 > 0$ GeV²) value of 1.07 ± 0.07 [113]). The most recent MINERvA preliminary results for CCQE antineutrino reaction are still subject to large flux normalization uncertainties but they seem to be consistent with $M_A = 0.99$ GeV [114]

3.2.2.1 Theoretical approaches to CCQE

Several approaches have been followed to describe the CCQE-like process. For moderate and intermediate neutrino energies, in the few GeV region, the most relevant ones are: the involvement of one nucleon, or a pair of nucleons or even three nucleon mechanisms and the excitation of Δ or higher resonances.

A review of theoretical model results can be found in [115]. Almost all approaches used at intermediate neutrino energies rely on the impulse approximation (IA) and neutrino-nucleus CCQE interactions and are viewed as a two step process: primary interaction and Final State Interactions (FSI), and then the propagation of resulting hadrons through the nucleus. In addition they consider several nuclear effects such as the Random Phase Approximation (RPA) or Short Range Correlations (SRC). In the neutrino-nucleus cross section measurements, a goal is to learn about neutrino free nucleon target scattering parameters (an obvious exception is coherent pion production). *Effective* parameters, like the sometimes discussed quasi-elastic axial mass M_A^{eff} , are of little use as their values can depend on the neutrino flux, target and perhaps also on the detection technique/acceptance.

The simplest model, commonly used in Monte Carlo event generators, is the relativistic Fermi gas (RFG) model proposed by Smith and Moniz more than 40 years ago [116]. The model combines the bare nucleon physics with a model to account for Fermi motion and nucleon binding within the specific nucleus. The model can be made more realistic in many ways to achieve better agreement with a broad range of electron scattering data. For example, the inclusion of a realistic joint distribution of target nucleon momenta and binding energies based on short range correlation effects leads to the spectral function (SF) approach.

Spectral functions for nuclei, ranging from carbon ($A = 12$) to iron ($A = 56$) have been modeled [117]. Calculations by Benhar *et al.*, [118] and Ankowski *et al.*, [119] show that the SF effects only moderately modify the muon neutrino differential cross sections, leading to reductions of the order of 15% in the total cross sections. Inclusion of nucleon-nucleon long-range correlations leads to RPA effects which improves predictions at lower momentum transfers (and also low Q^2).

3.2.2.2 Multinucleon mechanisms

A plausible solution to the large axial mass puzzle was first pointed out by M. Martini¹ *et al.*, [121, 122], and later corroborated by the IFIC group [123, 124]. In the MiniBooNE measurement of Ref. [112], QE is related to processes in which only a muon is detected in the final state. As was already discussed above, besides genuine QE events, this definition includes multinucleon processes. The MiniBooNE analysis of the data attempts to correct (through a Monte Carlo estimate) for real pion production that escapes detection through absorption in the nucleus leading to multinucleon emission. But, it seems clear that to describe the data of Ref. [112], it is necessary to consider, at least, the sum of the genuine QE (absorption by just one nucleon), and the multinucleon contributions, respectively. The sum of these two contributions contribute to the CCQE-like cross section.

The inclusion of the 2p2h (multinucleon) contributions enables [123, 125] the double differential cross section

$d^2\sigma/dE_\mu d\cos\theta_\mu$ and the integrated flux unfolded cross section measured by MiniBooNE, to be described with values of M_A (nucleon axial mass) around 1.03 ± 0.02 GeV [111, 113]. This is re-assuring from the theoretical point of view and more satisfactory than the situation envisaged by some other works that described the MiniBooNE data in terms of a larger value of M_A of around 1.3–1.4 GeV, as mentioned above.

3.2.2.3 Neutrino energy reconstruction

Neutrino oscillation probabilities depend on the neutrino energy, unknown for broad fluxes and, for CCQE, often estimated from the measured angle and energy of the outgoing charged lepton ℓ only. It is common to define a reconstructed neutrino energy E_{rec} (neglecting binding energy and the difference of proton and neutron masses) as:

$$E_{\text{rec}} = \frac{ME_\ell - m_\ell^2/2}{M - E_\ell + |\vec{p}_\ell| \cos\theta_\ell} \quad (2)$$

which would correspond to the energy of a neutrino that emits a lepton, of energy E_ℓ and three-momentum \vec{p}_ℓ , with a gauge boson W being absorbed by a free nucleon of mass M *at rest* in a CCQE event. The actual (“true”) energy, E , of the neutrino that has produced the event will not be exactly E_{rec} . Actually, for each E_{rec} , there exists a distribution of true neutrino energies that give rise to events whose muon kinematics would lead to the given value of E_{rec} . In the case of genuine QE events, this distribution is sufficiently peaked (the Fermi motion broadens the peak and binding energy shifts it a little) around the true neutrino energy to make the algorithm in Eq. (2) accurate enough to study the neutrino oscillation phenomenon [126].

¹ The papers of Martini *et al.* are based on the older investigation by Marteau *et al.*, [120]. The relevant features of the model were known already at the end of 1990s and at that time the goal was to understand better SuperKamiokande atmospheric neutrino oscillation signal.

However, due to the presence of multinucleon events, there is a long tail in the distribution of true energies associated to each E_{rec} that makes the use of Eq. (2) unreliable. The effects of the inclusion of multinucleon processes on the energy reconstruction have been noticed in [127] and investigated in Ref. [128], within the Lyon 2p2h model and also estimated in Ref. [129], using the simplified model of Ref. [130] for the multinucleon mechanisms. Further discussion of this effect and its implications is given in Section 3.2.6 with Figure 10 giving a good indication of the size of this effect.

3.2.2.4 Monte Carlo event generators

Monte Carlo codes (GENIE, NuWro, Neut, Nuance, etc) describe CCQE events using a simple RFG model, with FSI effects implemented by means of a semi-classical intranuclear cascade. NuWro also offers a possibility to run simulations with a spectral function and an effective momentum dependent nuclear potential. It is also currently the only MC generator with implementation of MEC dynamics. Since the primary interaction and the final state effects are effectively decoupled, FSI do not change the total and outgoing lepton differential cross sections.

3.2.3 The Pion-production Region

In the so-called RES region the channels of interest are mainly hadronic resonances, with the most important being the $\Delta(1232)$. Typical final states are those with a single pion. During the last five years several new pion production measurements have been performed. In all of them, the targets were nuclei (most often carbon) and interpretation of the data in terms of the neutrino-nucleon cross section needed to account for nuclear effects, impossible to do in a model independent manner. On the other hand, there has been a lot of activity in the area of coherent pion production and this subject will be discussed separately.

3.2.3.1 Experimental Results

3.2.3.1.1 NC π^0

Neutral current π^0 production (NC π^0) is a background to the ν_e appearance oscillation signal. One is interested in a π^0 leaving the nucleus and recent experimental data are given in this format with all the FSI effects included. Signal events originate mostly from: NC1 π^0 primary interaction with a π^0 not being affected by FSI and NC1 π^+ primary interaction with the π^+ being transformed into π^0 in a charge exchange FSI reaction. There are four recent measurements of NC π^0 production (K2K [131], MiniBooNE neutrinos, MiniBooNE antineutrinos [132] and SciBooNE [133]) that use three different fluxes: (K2K, Fermilab Booster neutrinos and anti-neutrinos) and three targets: H_2O (K2K), CH_2 (MiniBooNE) and C_8H_8 (SciBooNE). Final results are presented as flux averaged distributions of events as a function of the π^0 momentum and, in the case of MiniBooNE and SciBooNE, also as a function of the π^0 production angle.

3.2.3.1.2 CC π^+

MiniBooNE measured CC $1\pi^+$ production cross sections, where the signal is defined as exactly one π^+ in the final state with no other mesons [134]. A variety of flux integrated differential and doubly differential cross sections, were reported in Q^2 and the final state particles' momenta. The cross section results are much larger than NUANCE MC predictions and the difference is on average 23%. In Fig. 5 on the left GiBUU and NuWro predictions for CC π^+ are compared to the MiniBooNE data.

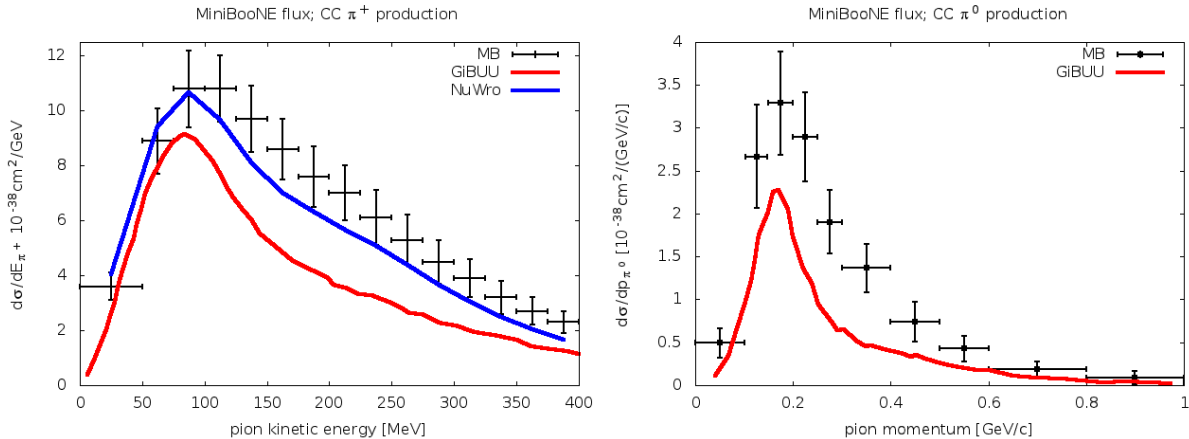


Figure 5: Left: Differential cross section for CC $1\pi^+$ production in the final state (all the FSI effects are included). MiniBooNE measurement [134] is compared to GiBUU [135] and NuWro computations. Right: the same for CC π^0 production, but only GiBUU results are shown.

3.2.3.1.3 CC π^0

MiniBooNE also measured CC $1\pi^0$ production cross sections. As before, the signal is defined as exactly one π^0 in the final state [136]. Various differential distributions are available. There is a dramatic discrepancy between the measured CC $1\pi^0$ production cross section as a function of neutrino energy and NUANCE MC predictions in the region of lower energies. On average the data is larger by $56 \pm 20\%$, but for $E_\nu < 1$ GeV the disagreement is as large as a factor of 2. In Fig. 5 on the right, GiBUU predictions for CC π^+ are compared to the MiniBooNE data.

3.2.3.2 Theoretical Considerations

Due to nuclear effects, a comparison to the new data is possible only for MC event generators, sophisticated computation tools like GiBUU and also a few theoretical groups which are able to evaluate FSI effects.

Most of the interesting work was done within GiBUU. It turned out to be very difficult to reproduce the MiniBooNE CC $1\pi^+$ and CC $1\pi^0$ results: the measured cross section is much larger than theoretical computations. In the case of CC $1\pi^+$ production, the discrepancy is as large as 100%. It was also noted that

the reported shape of the distribution of π^+ kinetic energies is different from theoretical calculations and does not show a strong decrease at $T_{\pi^+} > 120$ MeV located in the region of maximal probability for pion absorption.

The authors of [135] mention three possible reasons for the data/GiBUU predictions discrepancy: (i) the fact that Δ excitation axial form factor was chosen to agree with the ANL data only, neglecting the larger cross section measured in the BNL experiment; (ii) hypothetical 2p-2h-1 π pion production contribution analogous to 2p-2h discussed in Section 3.2.2.2; (iii) flux underestimation in the MiniBooNE experiment. For the last point, the argument gets support from the better data/theory agreement found for the ratio, as discussed below.

In the case of NC π^0 production, a systematic comparison was performed with NuWro MC predictions with an updated FSI model for pions [137]. The overall agreement is satisfactory. Shapes of the distributions of final state π^0 's are affected by an interplay between pion FSI such as absorption and *formation time* effects, understood here as an effect of a finite Δ life-time. It is argued that NC π^0 production data can be very useful for benchmarking neutrino MC event generators.

In addition, it has been known since ANL and BNL pion production measurements that although being a dominant mechanism, Δ excitation alone cannot reproduce the data and that non-resonant background terms must be included in the theoretical models. There were many attempts in the past to develop suitable models but usually they were not very well justified from the theoretical point of view.

3.2.3.3 Coherent pion production

In coherent pion production (COH) the target nucleus remains in the ground state. There are four possible channels: CC and NC reactions using neutrinos or anti-neutrinos. A clear experimental signal for the COH reaction for high energies was observed and the aim of recent measurements was to fill a gap in the knowledge of a region around ~ 1 GeV COH cross sections. At larger neutrino energies a recent measurement was made by MINOS which reported a NC reaction cross section at $\langle E_\nu \rangle = 4.9$ GeV to be consistent with the predictions of the Berger-Sehgal model (see below).

3.2.3.3.1 Experimental Results

In the case of the NC reaction, MiniBooNE [138] and SciBooNE [139] searched for the COH component. SciBooNE [139] evaluated the ratio of the COH NC π^0 production to the total CC cross section as $(1.16 \pm 0.24)\%$.

MiniBooNE evaluated the NC COH component (plus possible hydrogen diffractive contribution about which little is known) in the NC π^0 production as 19.5% (at $\langle E_\nu \rangle \sim 1$ GeV) and then the overall flux averaged overall NC1 π^0 cross section as $(4.76 \pm 0.05 \pm 0.76) \cdot 10^{-40}$ cm²/nucleon. Unfortunately, it is difficult to translate both measurements into the absolutely normalized value of the NC COH cross section because of strong dependence on the NUANCE MC generator used in the data analysis.

In the case of the CC reaction, K2K [140] and SciBooNE [141] reported no evidence for the COH component. For the K2K analysis, the 90% confidence limit upper bound for the COH cross sections on carbon

was estimated to be 0.6% of the inclusive CC cross section. The SciBooNE upper limits (also for the carbon target) are: 0.67% at $\langle E_\nu \rangle \sim 1.1$ GeV, and 1.36% at $\langle E_\nu \rangle \sim 2.2$ GeV. SciBooNE also reported the measurement of the ratio of CC COH π^+ to NC COH π^0 production and estimated it as $0.14_{-0.28}^{+0.30}$. This is a surprisingly low value, which disagrees with results from the theoretical models which, at SciBooNE energies, typically predict values somewhat smaller than 2. For massless charged leptons, isospin symmetry implies the value of 2 for this ratio and the finite mass corrections make the predicted ratio smaller.

3.2.3.3.2 Theoretical developments

Higher neutrino energy ($E_\nu > \sim 2$ GeV) COH production data (including recent NOMAD measurements) were successfully explained with a PCAC based model [142]. Adler's theorem relates $\sigma_{COH}(\nu + X \rightarrow \nu + X + \pi^0)$ at $Q^2 \rightarrow 0$ to $\sigma(\pi^0 + X \rightarrow \pi^0 + X)$. Subsequently, the model for the CC reaction, has been upgraded [143] to include lepton mass effects important for low E_ν studies. The new model predicts the $\sigma_{COH}(\pi^+)/\sigma_{COH}(\pi^0)$ ratio at $E_\nu = 1$ GeV to be 1.45 rather than 2. Another important improvement is to use a better model for $d\sigma(\pi + {}^{12}C \rightarrow \pi + {}^{12}C)/dt$ in the region of pion kinematic energy $100 \text{ MeV} < T_\pi < 900 \text{ MeV}$. As a result, the predicted COH cross section from the model became reduced by a factor of 2-3 [144]. The PCAC based approach is also discussed in [145] and critically re-derived in Ref. [146]. At lower energies the microscopic Δ dominance models for the COH reaction [147–150] are believed to be more reliable.

3.2.3.4 MC generators

Almost all MC events generators rely on the Rein-Sehgal resonance model for pion resonance production [151]. The model is based on the quark resonance model and includes contributions from 18 resonances covering the region $W < 2$ GeV. The model is easily implementable in MC generators and it has only one set of vector and axial form factors. In the original model, the charged lepton is assumed to be massless and prescriptions to cope with this problem were proposed in Refs. [152]. It was also realized that the Rein-Sehgal model can be improved in the Δ region by modifying both vector and axial form factors using either old deuterium or new MiniBooNE pion production data [153, 154].

For coherent pion production, all the MCs use the Rein-Sehgal COH model [142] analysis of MC event generators and theoretical models described in [115] show that in the 1 – 2 GeV energy region, the Rein Sehgal COH model predictions disagree significantly with all the recent theoretical computations and experimental results. None of the microscopic models, which are believed to be more reliable in the 1 GeV region, have been implemented in Monte Carlo codes yet.

3.2.3.5 Duality

Bridging the region between RES and DIS (where interactions occur on quarks, to a good approximation) dynamics is a practical problem which must be resolved in all MC event generators. In MC event generators “DIS” is defined as “anything but QE and RES”. This is usually expressed as a condition on a lower limit for the invariant hadronic mass, such as $W > 1.6$ GeV for example. Notice, however, that such a definition of

“DIS” contains a contribution from the kinematical region $Q^2 < 1 \text{ GeV}^2$ which is beyond the applicability of the genuine DIS formalism. The RES/DIS transition region is not only a matter of an arbitrary choice, but is closely connected with the hypothesis of quark-hadron duality.

Investigation of structure functions introduced in the formalism of the inclusive electron-nucleon scattering led Bloom and Gilman to the observation that the average over resonances is approximately equal to the leading twist contribution measured in the completely different DIS region. One can distinguish two aspects of duality: (i) resonant structure functions oscillate around a DIS scaling curve; (ii) the resonant structure functions for varying values of Q^2 slide along the DIS curve evaluated at fixed Q_{DIS}^2 .

As a practical procedure for addressing this region, Bodek and Yang [155] have introduced and refined a model that is used by many contemporary neutrino event generators, such as NEUGEN and its successor GENIE, to bridge the kinematic region between the Delta and full DIS. The model has been developed for both neutrino- and electron-nucleon inelastic scattering cross sections using leading order parton distribution functions and introducing a new scaling variable they call ξ_w .

At the juncture with the DIS region, the Bodek-Yang model incorporates the GRV98 [156] LO parton distribution functions replacing the variable x with ξ_w . They introduce “K-factors”, different for sea and valence quarks, to multiply the PDFs so that they are correct at the low Q^2 photo-production limit. A possible criticism of the model is the requirement of using the rather dated GRV98 parton distribution functions in the DIS region to make the bridge to the lower W kinematic region seamless.

3.2.4 ν -A Deep-inelastic Scattering

Although deep-inelastic scattering (DIS) is normally considered to be a topic for much higher energy neutrinos, wide-band beams such as the Fermilab NuMI, the planned LBNE and the nuSTORM beams do have real contributions from DIS that are particularly important in feed-down to the background and thus must be carefully considered. In addition, there are x -dependent nuclear effects that should be taken into account when comparing results from detectors with different nuclei and even when comparing results from “identical” near and far detectors when the neutrino spectra entering the near and far detectors are different.

Nonetheless, the DIS fraction of events for nuSTORM are on the order of 10% or less. The contribution of nuSTORM to the study of DIS is expected to be of similar precision. For a full review of neutrino DIS scattering results see [108].

3.2.4.1 nuSTORM Contributions to the Study of Neutrino-Nucleus Scattering

As an example of how nuSTORM will directly contribute to the study of neutrino-nucleus scattering, a comparison of the MiniBooNE and NOMAD results is shown in Fig. 6. Certainly one explanation for the difference between these two measured quasi-elastic cross sections is a mis-estimation of the absolute neutrino flux of one or both of the experiments. The claimed accuracy of the MiniBooNE flux is 8% while the NOMAD flux has a similar claim of 8% accuracy [157]. Therefore, the difference between the MiniBooNE and NOMAD results just from flux normalization spread alone is less than two standard deviations. With the nuSTORM flux resolution of $\leq 1\%$, the actual quasi-elastic cross section off carbon could be measured with an error nearly an order of magnitude smaller than either the MiniBoNE or NOMAD experiments.

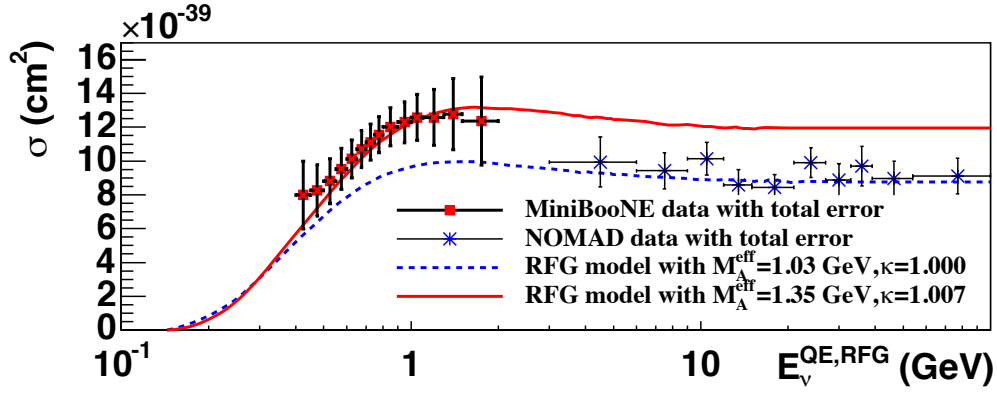


Figure 6: The total charged-current quasi-elastic cross section for ν_μ as measured by the MiniBooNE and NOMAD experiments.

It is important to point out that no other neutrino experiment now being planned can match the power of nuSTORM to answer the many challenges of neutrino-nucleus scattering. All use the conventional pion-decay source neutrino beams and, as such, can not expect to know the actual flux of neutrinos entering their detectors to better than (5-7) % at best compared with 1% or better for the nuSTORM beam.

3.2.5 Differences in the energy-dependent cross sections of ν_μ - and ν_e -nucleus interactions

To determine the mass hierarchy of neutrinos and to search for CP-invariance violation in the neutrino sector, current and upcoming accelerator-based neutrino-oscillation experiments such as T2K [158] and NOvA [159] as well as future proposed experiments such as LBNE and the Neutrino Factory [160] plan to make precision measurements of the neutrino flavor oscillations $\nu_\mu^{(-)} \rightarrow \nu_e^{(-)}$ or $\nu_e^{(-)} \rightarrow \nu_\mu^{(-)}$. An important factor in the ability to fit the difference in observed event rates between the near and far detectors will be an accurate understanding of the cross section of ν_μ - and ν_e -nucleus interactions. Uncertainties on differences in expected event rates due to differences between these cross-sections will contribute to experimental uncertainties in these flavor-oscillation measurements.

There are obvious differences in the cross sections due to the difference in mass of the outgoing lepton. These can be calculated by including the lepton-mass term in the cross-section expression. Fig. 7 [161], shows these expected differences in the cross sections as a function of neutrino energy. Another such calculable difference occurs because of radiative corrections. Radiative corrections from a particle of mass m are proportional to $\log(1/m)$, which implies a significant difference since the muon is ~ 200 times heavier than the electron [162]. This turns into a difference of $\sim 10\%$ in the cross sections. In addition to these differences, there are other more subtle differences due to the coupling of poorly-known or unknown form factors to the lepton tensor that reflect the differences in the outgoing lepton mass. These effects have been investigated in some detail [161] but must be probed experimentally.

Regarding nuclear effects, while there are no differences expected in the final-state interactions, there are expected differences in the initial reaction cross-sections between ν_μ - and ν_e -nucleus interactions. Since the lepton tensor, reflecting the mass of the outgoing lepton, couples to the hadron-response functions, there is a difference in nuclear effects at the interaction vertex due to the μ -to- e mass difference. The expected difference in the ν_μ - and ν_e -nucleus cross-section ratio is around 5% when using a spectral-function model

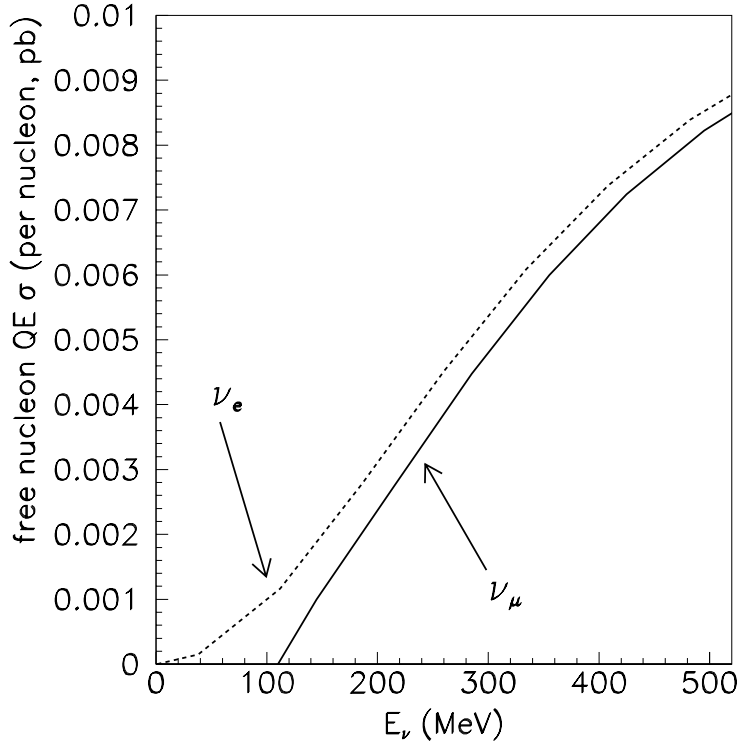


Figure 7: The total charged-current quasi-elastic cross-section for ν_μ and ν_e neutrinos.

[117] for the initial nucleon momentum compared to the relativistic Fermi gas model [116, 163]. There is another 5% difference expected for the multi-nucleon (np - nh) contributions [164]. These differences in cross sections extend up into the resonance region with the low- Q^2 behavior of Δ production, exhibiting 10% differences at values of Q^2 where the cross section has leveled off.

While each of the individual effects outlined above may not be large compared to current neutrino-interaction uncertainties, they are large compared to the assumed precision of oscillation measurements in the future LBL program. Moreover, the sum of these effects could be quite significant and the uncertainty in our knowledge of the size of these effects will contribute directly to uncertainties in the neutrino-oscillation parameters determined from these experiments—and these uncertainties can only be reduced with good quality $\bar{\nu}_e$ scattering data. nuSTORM is the only source of a well-understood and well-controlled $\bar{\nu}_e$ neutrino beam (and $\bar{\nu}_\mu$) with which these cross-section differences can be studied systematically.

3.2.6 Systematics of Long Baseline Oscillation Measurements

The recent measurement of a large value for the previously unknown mixing angle, θ_{13} , has raised the hope that the next generation of long baseline neutrino oscillation experiments could observe CP-violation in the lepton sector. Such a result would have far-reaching consequences in our understanding of the flavor and baryon asymmetry problems and could open a window to studying physics at the GUT scale. CP violation is introduced in the neutrino flavor oscillation mechanism through a CP-violating phase, δ_{CP} , in the PMNS mixing matrix. It can be accessed experimentally through two methods : a non-zero phase will lead to

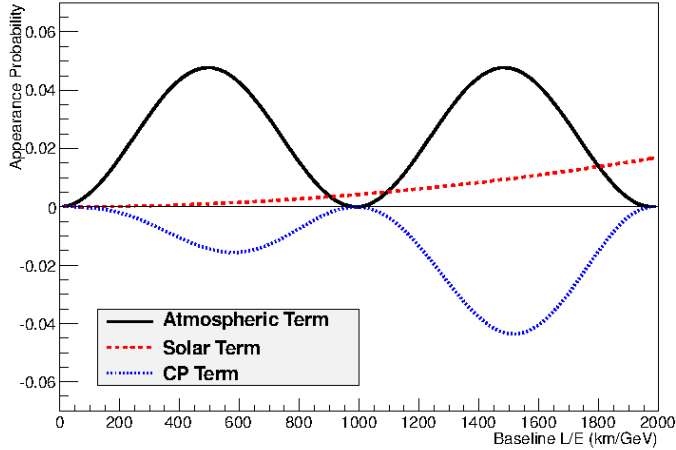


Figure 8: The $\nu_\mu \rightarrow \nu_e$ appearance probability as a function of baseline. The probability contains a term that controls oscillations at the atmospheric mass scale, a term that controls oscillations at the solar mass scale, and an interference term which contains the CP phase.

a difference between the $\nu_\mu \rightarrow \nu_e$ and $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$ appearance probabilities as well as a variation in the relative value of the second oscillation maximum with respect to the first oscillation maximum in $\nu_\mu \rightarrow \nu_e$ appearance measurements. Measurement of this CP-violating phase is challenging, regardless of the method used. Fig. 8 shows the components of the $\nu_\mu \rightarrow \nu_e$ appearance probability as a function of the experiment baseline calculated with oscillation parameters equal to our best-known estimates and assuming maximal CP violation ($\delta_{CP} = \frac{\pi}{2}$). The maximum appearance probability at any baseline is less than 6%, and in the baseline regions being considered by the next generation of experiments ($L/E \approx 400 - 500$ km/GeV), the component of the probability that is sensitive to the CP-phase is subleading. Any experiment that is attempting to measure CP-violation using neutrino oscillations must therefore be capable of measuring a small difference between small number of events, and in this context it is imperative that all systematic errors be well controlled, either by external measurements or by measurements at near detectors.

One of the largest systematic errors come from poor knowledge of the interaction cross sections. Fig. 9 shows the 3σ coverage of δ_{CP} as a function of $\sin^2(2\theta_{13})$ for the proposed experimental setup of T2HK. The recent measurements of $\sin^2(2\theta_{13})$: $[0.0944 \pm 0.007(\text{stat}) \pm 0.003(\text{sys})]$ from Daya Bay[166], $[0.113 \pm 0.013(\text{stat}) \pm 0.014(\text{sys})]$ from RENO[15] and $[0.097 \pm 0.034(\text{stat}) \pm 0.034(\text{sys})]$ [167] from Double CHOOZ locate the next experiments at the extreme right-edge of the plot. If only statistical errors are considered, then T2HK has 3σ sensitivity over almost the entire range of δ_{CP} . However, the coverage range decreases significantly if the ν_μ and ν_e interaction cross-section ratio is assumed to have a systematic uncertainty of 10%, as shown by the "default" line in Fig. 9. One can see that in order to have the largest δ_{CP} coverage, the ratio of the ν_e to the ν_μ cross sections need to be understood at the few percent level. Such a precise constraint cannot be made at a conventional neutrino experiment. As an example, the uncertainty in the ν_μ to ν_e flux ratio at an experiment in a conventional neutrino beam is on the order of 10%. Only a facility with a precisely defined beam, such as nuSTORM, is capable of delivering ν_μ and ν_e cross section measurements with the required precision.

The effect of cross section uncertainties differs depending on the design of the experiment. T2HK runs with an off-axis beam tuned to a peak neutrino energy of 600 MeV. At this energy, the charged current cross

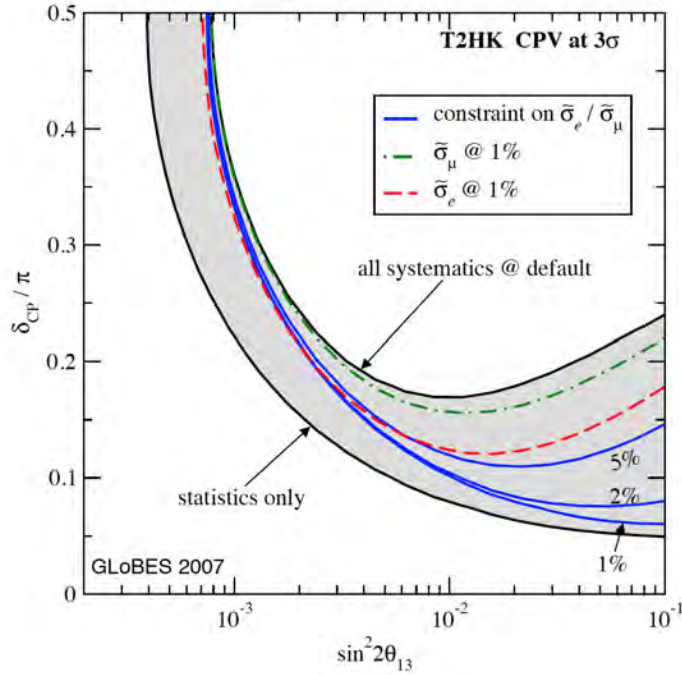


Figure 9: The T2HK 3σ CP phase coverage for a 2 year neutrino, 6 year antineutrino run in the 400 kW JPARC beam using a 500 kt far detector. Details can be found in [165].

sections are dominated by the quasi-elastic scattering process which has significant uncertainties. These uncertainties not only affect coverage, but also the precision of the measurement. Even with the most optimistic of runtime scenarios (2 years of neutrino running followed by 6 years of antineutrino running), the precision to which T2HK could determine δ_{CP} never falls below about 8° [168], limiting the capability of T2HK to distinguish between different flavor models. Other experimental setups, such as LBNE, operate at higher energy and in wide-band beams. Coloma *et al.* show that these wide-band beam experiments are less affected by systematic errors on the σ_e/σ_μ cross section ratio [168], although the study assumes an uncertainty of about 2% on the ν_e to ν_μ cross section ratio in the resonance energy regime. It should be noted that this uncertainty is purely theoretical. No measurements of this ratio exist, but it is expected that the uncertainty on any measurement using current conventional neutrino beams would be dominated by the knowledge of the neutrino flux and would not be much less than 10%.

All of these experimental setups, moreover, suffer from the problem that they must estimate the neutrino energy using the outgoing charged lepton partner from interactions on complex nuclear targets. Imperfect knowledge of the micro-physics of the nuclear environment can generate systematic differences in the mapping between the charged-lepton momentum and the neutrino energy between the model and the data. Fig. 10 (left) shows the effect of assuming a quasi-elastic like neutrino energy reconstruction (which is a reasonably standard procedure) for different types of event classes in the MiniBooNE experiment. The top right panel shows that the procedure reconstructs the neutrino energy in true quasi-elastic events very well, but that for other event classes (such as the 2p2h event class in the middle left panel), the reconstructed energy significantly underestimates the true neutrino energy. Such uncertainties cannot be mitigated by a near detector unless and until the model calculations are sufficiently detailed to allow falsification with final-state particle data. Systematic effects like this, which are unknown or poorly modeled, have been shown to lead to a bias in oscillation parameters which are obtained from fits to the reconstructed neutrino energy spectrum

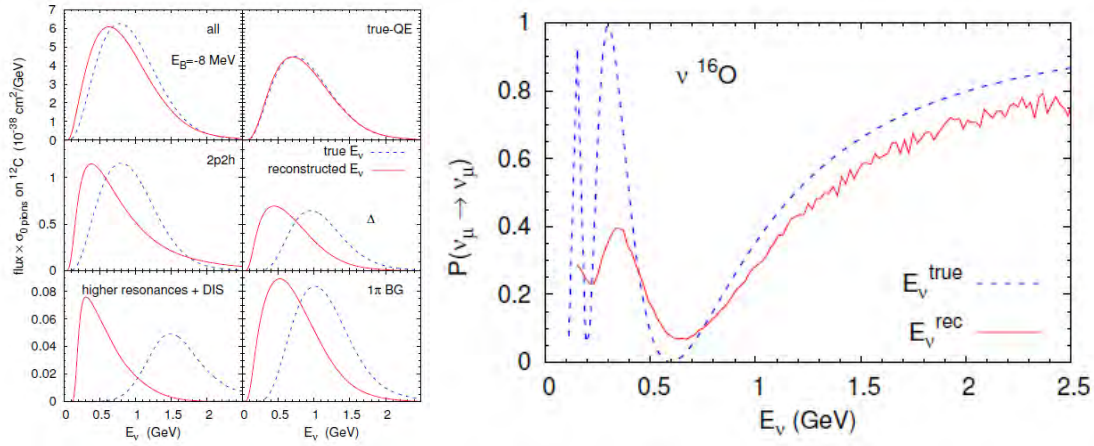


Figure 10: Left: Effect on the reconstructed neutrino energy spectrum of assuming a quasi-elastic topology in MiniBooNE. The neutrino energy spectrum generally underestimates the true spectrum for non-elastic event classes. Right: The muon neutrino disappearance probability for a T2K-like experiment shows a systematic shift in the oscillation dip due to the mis-reconstruction of the neutrino energy spectrum.

[169, 170]. For example, Fig. 10 (right) shows the ν_{μ} disappearance probability for a T2K-like experiment. The position of the first oscillation maximum is shifted slightly from its true position due to the influence of non-quasi-elastic event classes. If these event classes are included in the model, then a correction can be made, but the danger lies in an event class not being included in a model where it exists in the data. Such a situation has the potential to return a biased estimate of the oscillation parameters. Hence, understanding and incorporating these effects into the models is a high-priority task. This can only be done using dedicated experiments with high-resolution detectors, which can provide detailed information about the final-state of neutrino interactions on different target types. These detectors must be paired with a neutrino beam which is precisely known. Currently only the nuSTORM facility design is capable of making these measurements.

3.2.7 Detector Options

The physics program outlined in Section 3.2.1 cannot be performed without the precision beam delivered by the nuSTORM facility. This beam must be coupled with a detector or detectors which are capable of making the measurements required to understand the interaction of neutrinos on nuclei. A consideration of the physics topics suggests that the required detector must have the following capabilities :

- **Different nuclear targets :** Much of the physics which complicates the understanding of neutrino interactions arise from the necessary interaction of the neutrino in a nuclear potential. To understand the effect of nuclear targets, we need to compare the final states of neutrino interactions on light and heavy targets while using the same ν or $\bar{\nu}$ energy distribution. Targets from carbon to iron are now routinely used. New liquid argon experiments will provide data on a heavy noble liquid. One issue that is important, but not currently being addressed, is the requirement for data on light targets such as helium or, preferably, hydrogen or deuterium.
- **Vertex imaging :** Many of the nuclear models predict differing numbers of low energy nucleons being ejected from the nucleus. Currently no experiment can image the vertex with sufficient resolution to collect data on low energy vertex activity to test these models. The only detectors which could do

this are liquid or gas argon TPCs or a bubble-chamber type imaging device.

- **Flavor identification :** The nuSTORM beam delivers an equal mix of ν_μ and $\bar{\nu}_e$ (or $\bar{\nu}_\mu$ and ν_e). A detector must be capable of distinguishing between the final state leptons in charged current interactions. This requires a detector capable of either track/shower discrimination or particle flavor identification.
- **Final state reconstruction :** It is extremely important to understand the topology of the final-state hadronic system as this topology reflects both the hadronic processes in the bare interactions and the secondary interactions of final state particles as they pass through the nucleus. These final state interactions are one of the largest sources of uncertainty in the current round of oscillation experiments. Comparison of the final state on light and heavy targets will help constrain the final state models.
- **Sign selection :** The capability for determining the charge of the final state particles emitted from the interaction is very desirable. The inclusion of a magnet into the detector design is considered for all stand-alone detector designs described below. However, it may not be possible to include this capability fully in the initial measurement phase. This is, however, important for both neutrino oscillation physics, which relies on determining the sign of the outgoing charged lepton, and for neutrino interaction physics which would benefit substantially by separation of final state pions by charge.

It would be difficult to design a single detector that could embody all of these requirements without compromising on performance. We envision the nuSTORM beam to be a facility serving a number of different detectors for different types of studies. nuSTORM could run as a phased research program, initially with existing detectors, and then adding new experiments optimized for different measurements.

The first measurements could involve using existing, possibly refurbished, well-understood detectors. The MINER ν A experiment [171], currently operating in the NuMI beam in the energy range that the nuSTORM beam would deliver, could be moved to the nuSTORM facility. This can be accomplished with relatively minimal expenditure although the photosensors, currently multi-anode PMTs, may need to be replaced with silicon photomultipliers. MINER ν A can provide data on interactions on carbon, lead and iron with reasonable tracking and calorimetry. It has some capacity to image details of the neutrino interaction vertex, but a better detector for this purpose would be one of the liquid argon detectors that are currently being developed, or are envisioned as part of the LBNE research program. One problem with these choices of detectors is that neither MINER ν A, nor any of the planned liquid argon systems, can measure the charge or momentum of muons from charged current interactions. A new muon ranger would have to be provided in the nuSTORM facility. The near-detector companion to SuperBIND for the short-baseline ν oscillation component of nuSTORM could be used as the muon ranger (see section 6). It is currently specified with a mass of 200 T so a more detailed analysis of its use at the muon ranger for the ν interaction component of nuSTORM will have to be done. This would be the only new detector needed for the initial phase of cross-section measurement program.

An alternate possibility could be a completely new, high-resolution, magnetized tracking detector. Two concepts are being studied:

1. The first is the HIRESMNU detector, proposed and fully costed as a near detector for the LBNE experiment [172, 173]. Fig. 11 shows a schematic of the HIRESMNU design. This detector embeds a $4 \times 4 \times 7 \text{ m}^3$ Straw-tube tracker (STT), surrounded by a 4π electromagnetic calorimeter (ECAL)

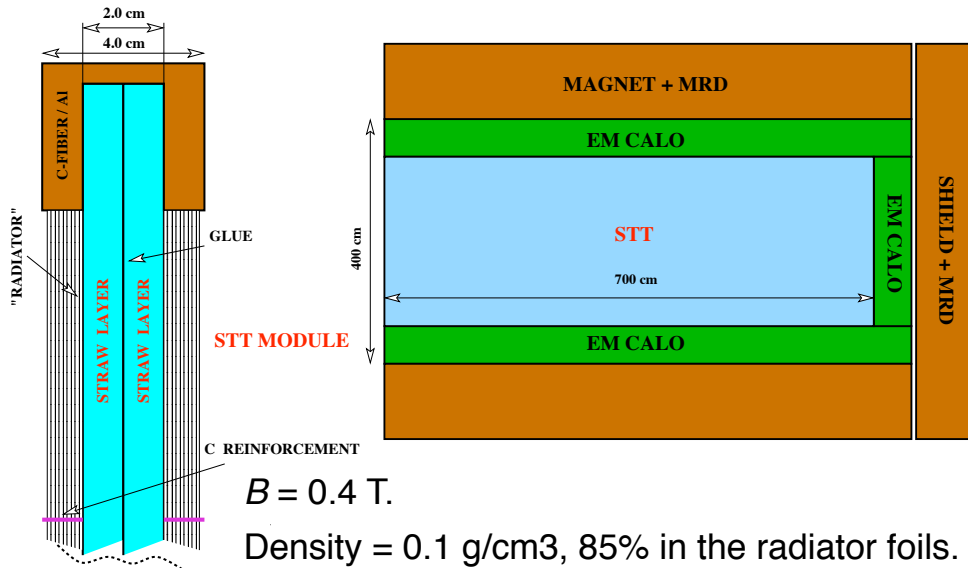


Figure 11: Schematic of the HIRESMNU concept showing the straw tube tracker (STT), the electromagnetic calorimeter (ECAL) and the magnet with the muon range detector (MRD). The STT is based upon ATLAS [174–176] and COMPASS [177, 178] trackers. Also shown is one module of the proposed straw tube tracker (STT). Interleaved with the straw tube layers are plastic foil radiators, which provide 85% of the mass of the STT. At the upstream end of the STT are layers of nuclear-target for cross section measurements.

in a dipole magnet with $B \simeq 0.4 \text{ T}$. Downstream of the magnet, and within the magnet yoke, are detectors for muon identification. The STT will have a low average density similar to liquid hydrogen, about 0.1 gm/cm^3 , which is essential for momentum determination and the identification of electrons, protons, and pions. The foil layers, up- and down-stream of the straw tubes, provide the transition-radiation and constitute most of the 7 ton fiducial mass. The foil layers serve both as the mass on which the neutrinos will interact and as generators of transition radiation (TR), which provides electron identification.

2. A versatile detector option has been proposed as a near detector for LBNO, the Gas Argon Modular Apparatus for Neutrino Detection ($\gamma\nu\text{det}$) [179]. It is based on a pressurized argon time projection chamber (TPC) located in a large 5 m diameter pressure vessel, as shown in Fig. 12. A magnetic field is applied to the full volume of the pressure vessel. A magnet design similar to that of the UA1/NOMAD spectrometer dipole magnet provides a field with characteristics close to those required for this detector. The pressure vessel can accommodate several layers of a scintillator-based calorimeter, such as the SuperBIND plastic scintillator material, between the TPC and the pressure vessel inner surface. One advantage of this design, compared with a more compact pressure vessel enclosing only the TPC, is that there is less redundant/passive material between the TPC and first layers of the scintillator detector and fewer blind spots. The outer layers of the embedded scintillating material can be interleaved with radiators to improve the containment within the pressure vessel of more energetic secondaries from events of interest occurring in the TPC. High energy muons ($> 1 \text{ GeV}$) of both signs from neutrino events originating in the TPC would be measured downstream in the muon ranger/spectrometer described above.

The details and costing of each of these options is currently under study.

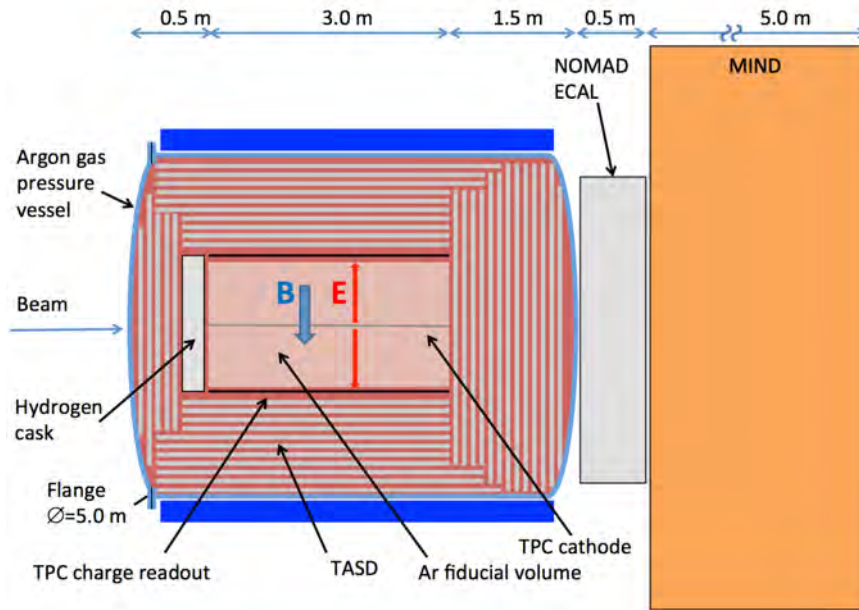


Figure 12: Schematic of the pressurized argon gas-based TPC detector. Both the TPC and scintillator calorimeter layers surrounding it are enclosed in a pressure vessel. A 0.5 T magnetic field is applied to the pressure vessel volume. Downstream of the TPC are also an electromagnetic calorimeter (ECAL) and a magnetized iron neutrino detector (MIND/SuperBIND). The latter acts as a muon spectrometer for neutrino interactions occurring in the TPC and as an independent near detector for the sterile neutrino program.

One limitation that is apparent in these detector options is that they all involve interactions on heavy targets. It is becoming clear, however, that much of the current confusion around neutrino interaction physics arises from the low statistics, sometimes conflicting, data on light targets that are the foundation of many of the models. It is possible that a light-nuclei target could be integrated with either HIRESMNU or the gaseous TPC option in the form of a solid target inside the magnet of HIRESMNU or the pressure vessel of the gaseous TPC detector. However, the constraints of the proposed designs make implementation of such a system difficult and sub-optimal. An alternate possibility in a later phase of nuSTORM would involve repeating, or in many cases performing the first, measurements of interactions on hydrogen or deuterium nuclei. The techniques of the bubble chamber experiments could be revived, complemented by modern readout technology in the form of fast CCD or CMOS imaging systems and fast, accurate image analysis using techniques adapted from the liquid argon TPC program.

It is clear that the measurements envisioned at the nuSTORM facility cannot be accomplished with just one experiment. A careful study of the performance of each of the detector options, in conjunction with a prioritization of the most important measurements by the community, will define a phased research program that will, finally, clear up the many areas of poor knowledge of neutrino interaction cross sections.

3.3 Technology test-bed

3.3.1 Muon beam for ionization cooling studies

Muon ionization cooling improves by a factor ~ 2 the stored-muon flux at the Neutrino Factory and is absolutely crucial for a Muon Collider of any center-of-mass energy in order to achieve the required luminosity. The Muon Ionisation Cooling Experiment (MICE) [180] will study four-dimensional ionization cooling and work is underway to specify the scope of a follow-on six-dimensional (6D) cooling experiment. MICE is a “single-particle” experiment; the four-momenta of single muons are measured before and after the cooling cell and then input and output beam emittances are reconstructed from an ensemble of single-muon events. A 6D cooling experiment could be done in the same fashion, but doing the experiment with a high-intensity pulsed muon beam is preferred. One feature of nuSTORM is that an appropriate low-energy muon beam with these characteristics can be provided in a straightforward fashion, see Section 4.6.

3.3.2 Neutrino cross-section measurements for Super Beams

The neutrino spectrum produced by the nuSTORM 3.8 GeV/c stored muon beam is shown in Fig. 13. The nuSTORM flux at low neutrino energy (< 0.5 GeV) is relatively low. The neutrino energy spectrum that would be produced at a low-energy super-beam such as the SPL-based beam studied in [181] or the recent proposed super beam at the European Spallation Source (ESS) [182] is also shown in Fig. 13. Both the SPL and ESS based super beams propose to use the MEMPHYS water Cherenkov detector [183, 184]. To enhance the event rate in the low neutrino-energy region of importance to such facilities, the possibility of capturing muons with a central momentum below 3.8 GeV/c is being studied.

The “degrader” introduced in Section 4.6 provides an alternative technique by which the required low-energy neutrino beam could be produced. The muons exiting the degrader with $P_\mu > 400$ MeV/c (see Fig. 82) could be used to produce neutrinos with energies of around 300 MeV. A detector placed a few tens of meters behind the degrader would make it possible to measure the $\bar{\nu}_e N$ and $\bar{\nu}_\mu N$ cross sections required for the SPL or ESS based super beams.

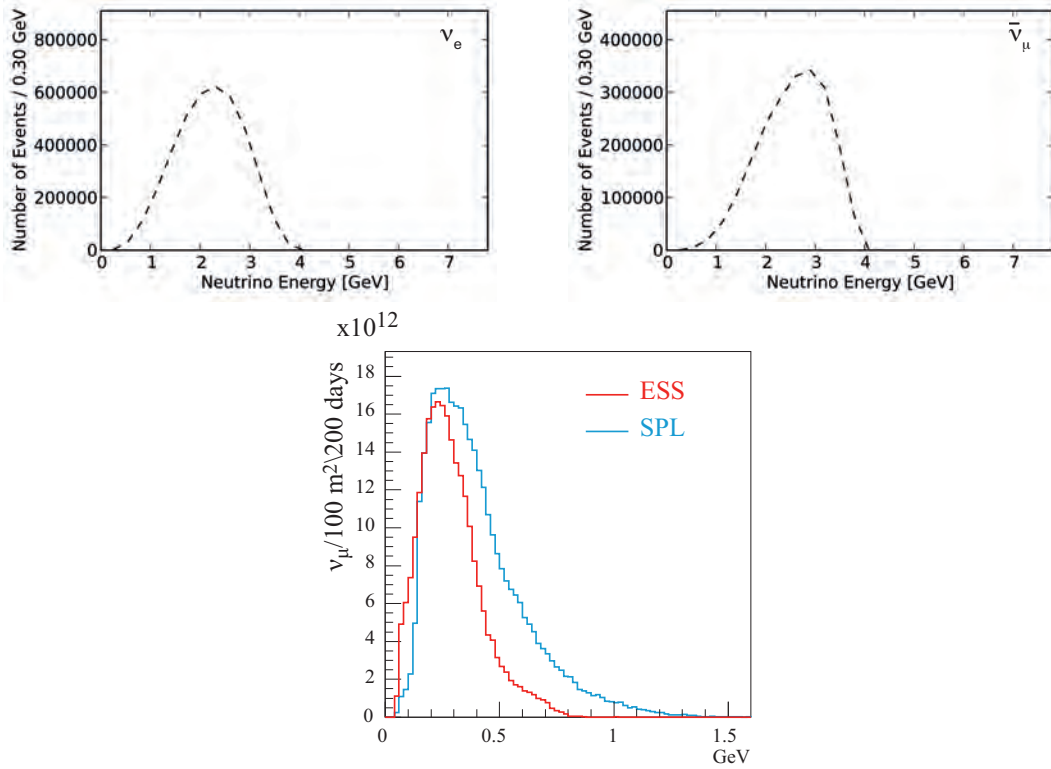


Figure 13: Top row: ν_e (left) and $\bar{\nu}_\mu$ (right) event rates per 100 T in a detector placed ~ 50 m from the end of one of the straight sections (for a stored μ^+ beam) at nuSTORM. Bottom row: neutrino energy spectrum for the SPL (with proton energy of 4.5 GeV) and ESS (with proton energy of 2.5 GeV) based super beams.

4 Facility

The basic concept for the facility was presented in Fig. 1. A high-intensity proton source places beam on a target, producing a large spectrum of secondary pions. Forward pions are focused by a horn into a capture and transport channel. Pion decays within the first straight of the decay ring can yield a muon that is stored in the ring. Muon decay within the straight sections will produce ν beams of known flux and flavor via: $\mu^+ \rightarrow e^+ + \bar{\nu}_\mu + \nu_e$ or $\mu^- \rightarrow e^- + \nu_\mu + \bar{\nu}_e$. For the implementation which is described here, we choose a 3.8 GeV/c storage ring to obtain the desired spectrum of $\simeq 2$ GeV neutrinos (see Fig. 13). This means that we must capture pions at a momentum of approximately 5 GeV/c.

4.1 Primary proton beam

This section describes the reference design for the nuSTORM primary (proton) beamline. This system will extract protons from the Fermilab MI (MI) synchrotron, using a single-turn single-batch extraction method and then transport them to the target in the nuSTORM target hall. The nominal range of operation will be for protons from 60 to 120 GeV/c.

The principal components of the primary beamline include the standard magnets in the MI-40 abort line to capture protons in the synchrotron and redirect them to the nuSTORM beamline. This beamline is a series of dipoles and quadrupole magnets to transport the protons to the target. All of the nuSTORM primary-beam technical systems are being designed to support sustained, robust and precision beam operation.

In 1994, the NuMI Project Definition Report originally designed the extraction line from the MI-40 area. The MI absorber was built with the transport beam pipe installed at an estimated elevation of 714 feet. The nuSTORM facility will extract protons from the MI through this channel and continue through two enclosures towards the nuSTORM target hall [185]. In Fig. 14, this channel is indicated by the shaded-in square offset from the center of the MI Absorber. The nuSTORM primary beam is extracted using single-turn, or “fast” extraction, in which a portion of the protons accelerated in the MI synchrotron ring, will be diverted to the nuSTORM beamline within one revolution after each acceleration cycle. The train of bunches dedicated for the nuSTORM target hall extends one seventh of the MI circumference or for one “Booster Batch.” The remaining bunches are dedicated to additional operational beamlines running concurrently, i.e. NuMI, NoVA, or LBNE [186, 187]. After extraction, the beam is controlled by a series of dipoles (bending) and quadrupole (focusing) magnets.

The nuSTORM primary-beamline is designed to direct the beam towards the nuSTORM target hall and collection channel, with a spot size appropriate for maximizing pion production (see Section 4.3). nuSTORM will implement a point to point focusing design in two sections. This is allowed due to the relatively short distance between THE MI and the nuSTORM target hall (600') and also because a large beam spot is required for the MI absorber line (upstream beamline common to MI abort line and nuSTORM). The first section focuses the proton beam after the MI absorber line. The second and final focus of the beam will be used for controlling the beam spot size on the target.

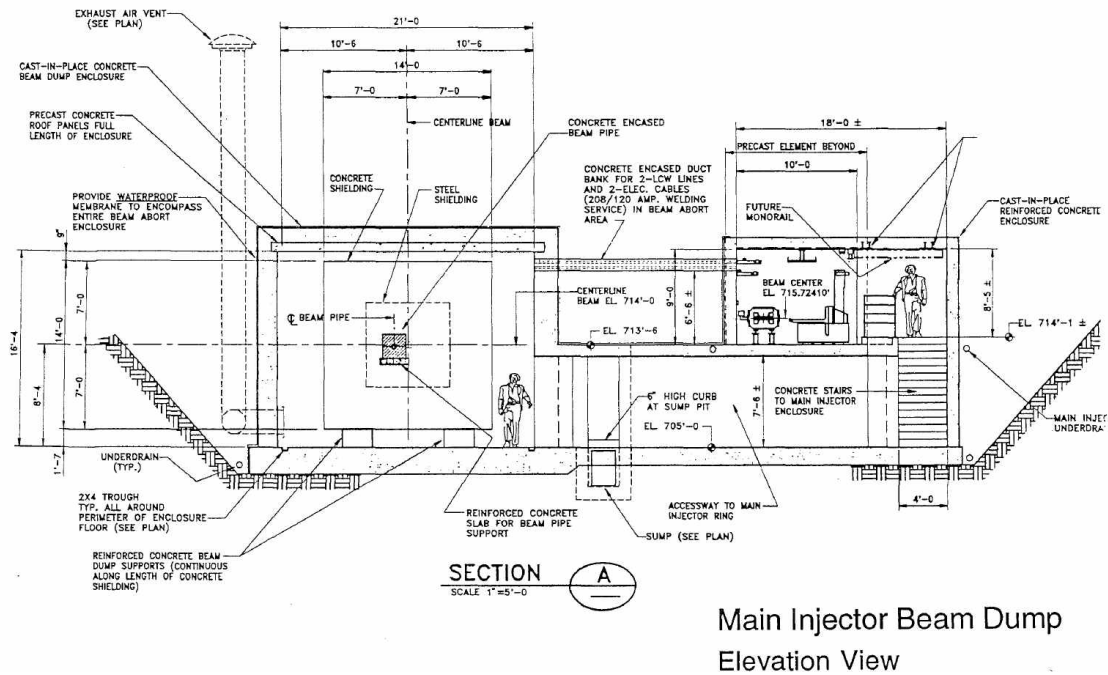


Figure 14: MI absorber room cross section.

4.1.1 Extraction line

In order to achieve this focused beam, the MI absorber line will be modified with respect to placement of existing quadrupole magnets and replacement of their HV cables from the MI quad focusing buss onto separate individual power supplies. All absorber line quadrupoles, Q001 through Q003, will need independent power supplies. Q002 and Q003 will need to be moved upstream of their current locations by 23 and 30 feet respectfully. This relocation will provide adequate space for nuSTORM’s extraction switch magnet and allow for proper optics in the remaining beamline. The two large bending magnets will remain in their current location, and continue to operate on the MI bend buss.

Once MI beam has achieved its flattop energy, three new kicker magnets in the MI-40 area apply a horizontal kick to the beam to the outside of the ring. This beam passes through a set of quadrupoles, Q401 and Q402, to continue the horizontal trajectory at elevation 715 feet, 9 inches. Then a series of three specialized magnets called Lambertsons [188], L001 L002 and L003, vertically extract the beam from the MI. These extraction Lambertsons are unique in that this set bend the beam downward for extraction, while in other Lambertson areas, such as MI-52 and MI-60, they bend the beam upward.

The Lambertsons sit in the path of the beam both when beam circulates and when it is being extracted, so they must accommodate both paths. The circulating beam passes through a field-free region in the magnet, and the extracted beam passes through the region of magnetic field and is bent downward from the circulating MI trajectory by 18.24 milliradians. Fig. 15 shows a cross section of the MI Lambertson. Each Lambertson in the line bends the beam, such that after passing through the string of Lambertsons the extracted beam is sufficiently separated from the MI orbit to pass through the first bending magnet external to the MI, a C-magnet [189]. The C-magnet clears the MI beam tube downstream of the third Lambertson and provides an additional downward bend, 9.34 milliradians, enough so that the extracted beam can pass below the outside of the next quadrupole in the MI lattice. This also accommodates clearance for the first

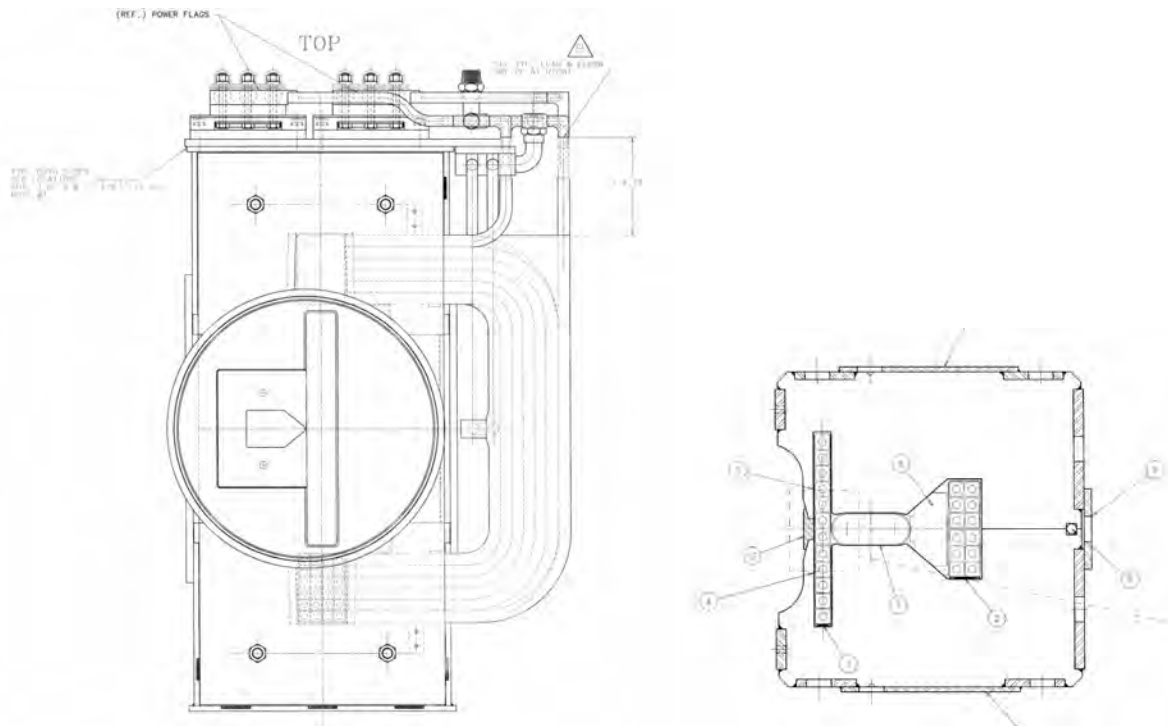


Figure 15: MI Lambertson (left) and C magnet drawings (right).

quadrupole, Q001, in the absorber line. Fig. 15 also shows a cross section of the MI C-magnet.

Once the nuSTORM primary beam is extracted from the MI, it shares the beam line components with the MI aborted beam. With its trajectory, the nuSTORM primary beam will be directed and focused exactly like the MI aborted beam by a series of three quadrupoles, two dipoles and several trim magnets. However, once past the last quadrupole, Q003, the beam will be bent towards the transport beam pipe in the MI absorber using a pulsed EDB (extended dipole bender) dipole named NSHV1 [190]. This horizontal pulsed magnet is rolled by 0.37 radians clockwise to necessitate the horizontal and vertical differences between the MI absorber and the transport beam pipe aperture, as shown in Fig. 14. This results in the beam being bent 4.97 milliradians horizontally away from the MI ring and 1.93 milliradians vertically downward.

Between the MI enclosure and the MI absorber room is a distance of 88 feet. This stretch of beamline is transitioned into an 24 inch wide “bermpipe” commonly used at Fermilab. This vacuum isolated stretch of berm-pipe [191] will contain three beamlines, two of them converging towards the MI Absorber, while the nuSTORM trajectory is towards the Transport Beam Pipe. Fig. 16 shows this berm pipe relative to the MI enclosure and absorber room.

4.1.2 Beam line

From the back end of the MI Absorber Room, the nuSTORM beamline continues into new construction enclosures. The first section of optics is to match the MI Abort line optics to the final focusing optics of the nuSTORM beamline. This is achieved by using only two 3Q120 quadrupole magnets, NS1Q1 and NS1Q2, at the beginning of the first enclosure NS1 [192]. Once the beam has passed the first quadrupoles in the NS1 enclosure, the beam is bent upwards by NS1V1 to correct for the downward trajectory created naturally by

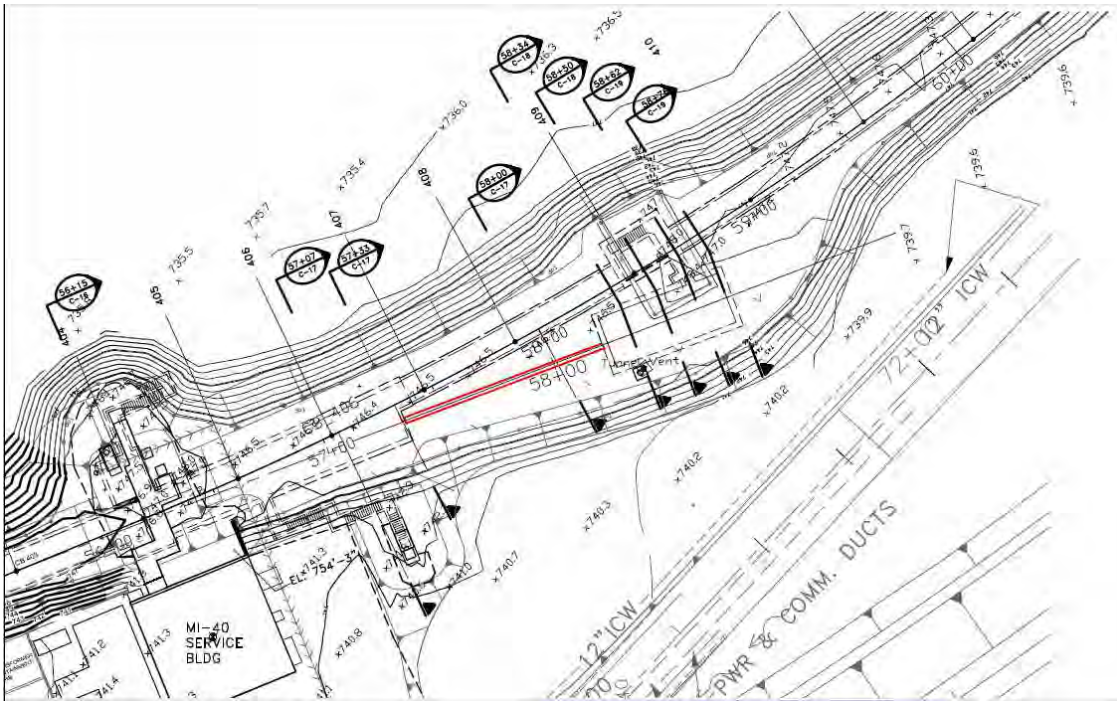


Figure 16: MI absorber berm pipe.

the MI Absorber line and the NSHV1. Here the beam line is at its lowest point 713 feet, 3 inches.

After the beam has had the necessary drift space to be focussed by NS1Q1 and NS1Q2, and be placed on the correct vertical trajectory by NS1V1, the first series of horizontal dipoles, NS1H1, bends the beam 0.0934 radians. This horizontal string of magnets is comprised of four B2 magnets [193] with a 1.54 Tesla field. After this string of dipoles the beam is then transported to the next enclosure, NS2.

In NS2, the beam is bent with another series of four B2 dipoles, NS2H1. This string bends the beam an additional 0.0934 radians, with a bend field of 1.54 T. After the last bend string, a single quadrupole magnet NS2Q1 focuses the beam vertically. This allows the beam to be focused after the bending by the NS2 horizontal magnet string. After the last bend, the beam is focused onto the nuSTORM target via NS2Q1. This quadrupole will be able to focus the beam on target to maximize pion production and efficiency. The beam half widths and component apertures are shown in Fig. 17 and Fig. 18. They include the FODO lattice of the MI through the absorber line and through the nuSTORM primary beamline. The nuSTORM primary beamline starts at station 481 ft. This beamline is also specifically planned so that it has very little impact on current operational surroundings. The nuSTORM beamline optics share three quadrupoles with the MI absorber line, and three dedicated quadrupoles in the primary beamline. The optics and trajectory of this beamline have been designed to handle different momentum protons to be operational with concurrently running experiments utilizing the MI in the future. Fig. 17 is designed for 120 GeV/c protons, however, Fig. 18 shows the beam line is capable of focusing the 60 GeV/c protons for future experiments. Table 1 contains the data for the nuSTORM quadrupoles for 120 GeV/c protons. The nuSTORM beamline contains 18 correctors or 9 pairs of horizontal and vertical trims, before and after every large angle change mentioned above. Four of these correctors are placed just prior to the nuSTORM target hall for the operational ability to change the position and angle of the beam interacting with the target. This set of correctors will be useful for target scans and alignment. These correctors can correct a 0.25 mm transverse mis-alignment offset for

NuStorm Primary Beamline 120 GeV/c

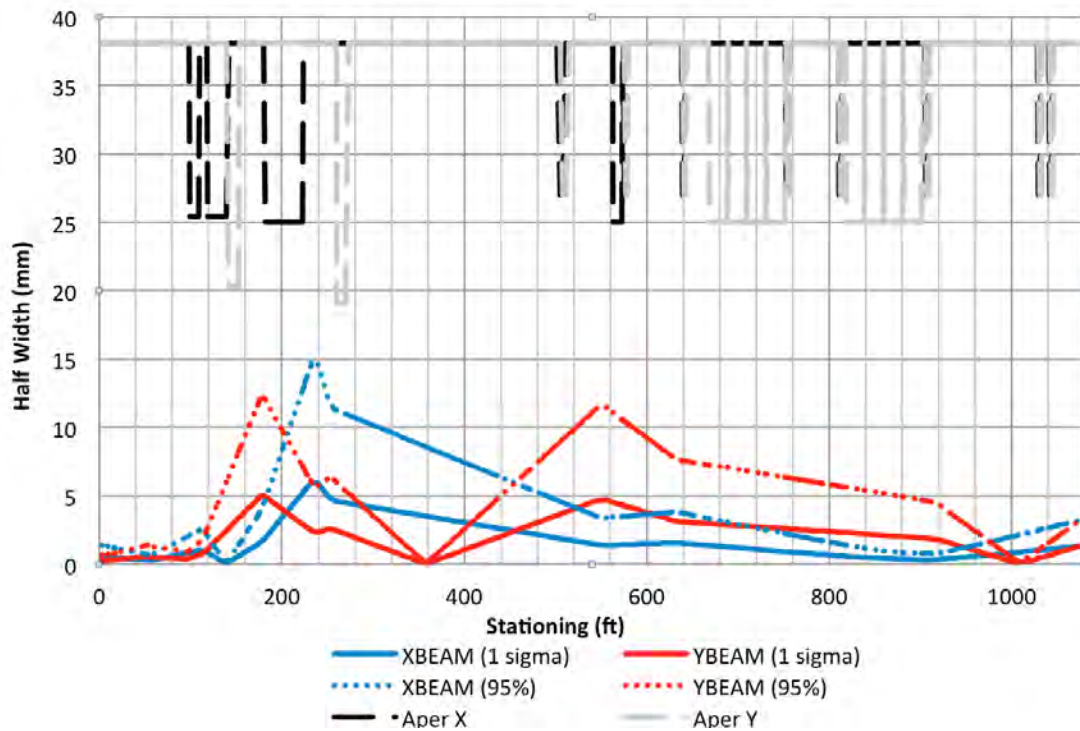


Figure 17: nuSTORM beamline half width sizes and apertures for 120 GeV/c protons.

Table 1: Magnet names types and settings for 120 GeV/c protons.

Dipoles	Type	Current (Amps)	Notes
NSHV1	EDB	796.4	Rolled 0.37 radians
NS1V1	EDB	664.7	Critical Device #1
NS1H1 (4)	B2	3833.1	Critical Device #2
NS2H1 (4)	B2	3833.1	
Quadrupoles	Type	Current (Amps)	Notes
Q001	IQA	1883.2	Vertical Focusing
Q002	IQB	1423.9	Horizontal Focusing
Q003	IQB	853.0	Vertical Focusing
NS1Q1	3Q120	22.3	Vertical Focusing
NS1Q2	3Q120	11.9	Horizontal Focusing
NS2Q1	3Q120	19.5	Vertical Focusing

all the major bending dipoles. For roll tolerances, the maximum acceptable error is 0.5 milliradians [194].

As mentioned above, the nuSTORM primary beamline focusing and bending elements are split between two different enclosures. These enclosures are split by a jacked pipe of 59 feet in length. Running through this jacked pipe, are individual pipes that contain the beam line and other utility supply and return lines. The primary beamline enclosure layout is shown in Fig. 19 along with the proposed target hall, Pion Decay

NuStorm Primary Beamline 60 GeV/c

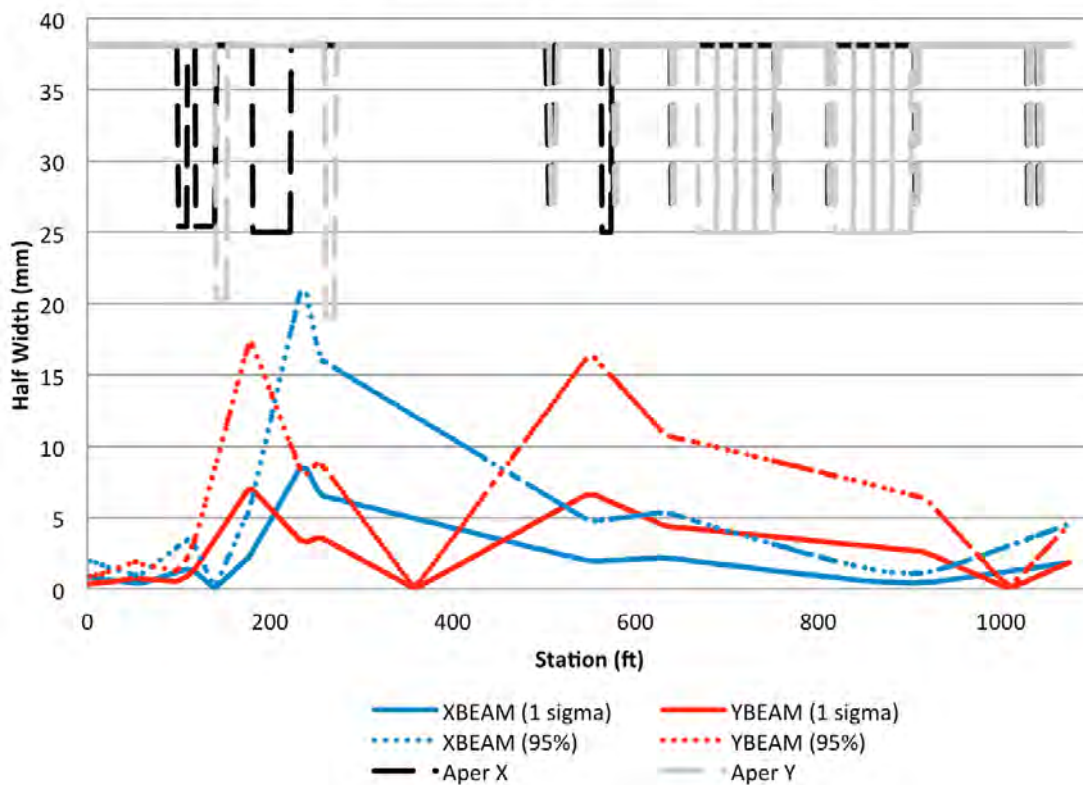


Figure 18: nuSTORM beamline half width sizes and apertures for 60 GeV/c protons.

Channel and Muon Decay Ring. nuSTORM's primary beamline will use two critical devices, as stipulated in the Fermilab Radiological Control Manual [195] (FRCM). The first critical device, NSHV1, is located inside the MI-40 area as described above. This switch magnet must be powered in order to allow beam to the nuSTORM target. The second critical device will be NS1H1, as described above.

nuSTORM's primary beamline will also include instrumentation packages containing Loss Monitors, Toroids, Multiwires, and Beam Position Monitors (BPMs). In this current design the beamline contains three toroids, ten Multiwires, and twelve BPMs. Loss monitors will be placed on magnets with tighter aperture constraints. Each major bending string, NS1V1, NS1H1, and NS2H1 will have loss monitors mounted on the first magnet.

Of the three toroids, the first will be located inside the MI enclosure just prior to the berm pipe. This will be able to report an input for transfer efficiency to the nuSTORM target hall. The second toroid is positioned just after the NS1H1 magnet string in the NS1 enclosure. The last toroid will be positioned in enclosure NS2 just prior to the target hall. This will provide a comparison for transfer efficiency and protons on target measurements.

Of the ten Multiwires, enclosure NS1 has four and enclosure NS2 contains the remaining six. In each Multiwire, the wire spacing is assembled with 1 mm pitch, a common spacing at Fermilab, and each plane will contain forty wires. Each BPM unit contains horizontal and vertical plates to provide horizontal and vertical positions, saving on longitudinal space in the beamline. nuSTORM will adopt the LBNE style

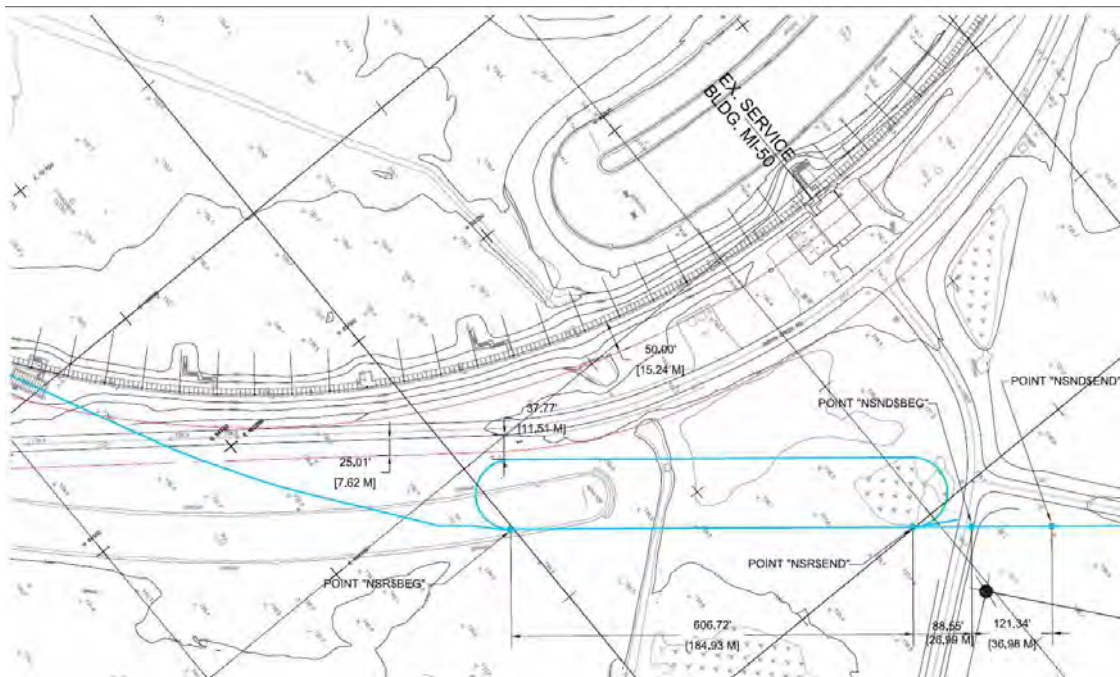


Figure 19: Enclosure layout of nuSTORM primary beamline.

button BPMs. In enclosure NS1, five BPMs will be installed and the NS2 enclosure will have six BPMs.

nuSTORM's two large bending strings of NS1H1 and NS2H1 have the same operating current and bend field. For power supplies to be used by this line, it is cost efficient to use one power supply to power both the first and the second string of B2 magnets. Other magnets such as the correctors, quadrupoles, and the first critical device NSHV1, will need to use independent power supplies .

4.2 Target Station

4.2.1 Target station overview and conceptual layout

The nuSTORM target station conceptual layout addresses the requirement of providing a reliable pion production facility while providing a platform for component maintenance and replacement. Due to the severe service environment encountered in target halls, it is expected that the beamline elements will require replacement on the order of every few years.

The general operation of the target station utilizes a primary proton beam extracted from the MI and transported to interact with a target to produce pions (along with other short-lived hadrons) which are subsequently focused toward a set of capture quadrupoles by a single magnetic focusing horn. The design parameters of beam spot size, target material and interaction length, and focusing horn current and geometry are considerations for providing reliable and sufficient pion production to support the experimental requirements. The following parameters for the proton beam on target are specified for the baseline in Table 2. Several considerations must be adequately understood and addressed to ensure safe and reliable operation of the target station. The target station is one area where nuSTORM can draw heavily on the successful operation and experience gained in NuMI target hall operations. The nuSTORM target station

Table 2: Proton beam parameters

Energy	120 GeV
Protons per pulse	8×10^{12}
Pulse width	1.6 μ s
Beam σ	1.1 mm
Cycle time	1.33 sec.

baseline conceptual layout will employ a very similar design approach to that used in the NuMI target hall complex. The following key elements address the primary requirements for safe and reliable target station operation:

- Provide adequate shielding to safely accommodate a maximum beam power of 400kW.
- Utilize economical shielding and target pile design methodology to minimize cost impact.
- Provide for the installation and operation of the following active beamline components:
 1. Production target
 2. Focusing horn, electrical stripline bus, and pulsed power supply
 3. Pair of capture quadrupole magnets and related power supplies and utilities
 4. Water-cooled collimators for quadrupole secondary beam spray protection
- Provide target pile shield with air cooling while considering humidity control to minimize component corrosion and provide the ability for safe and effective tritium management.
- Provide a target, horn, and capture quadrupole-positioning module support platform including shielding, hardware support provisions, remote hot handling capability with rigid, stable alignment capability.
- Provide for hot handling operations such as failed component replacement and cool-down storage for highly radioactivated components.
- Provide the infrastructure layout for constructing and operating the facility including radioactive water cooling (RAW) systems, component power supplies, air handling systems, adequate floor space for placement of shielding blocks during maintenance periods, and a component handling interface including remote pick functionality, cameras to facilitate hot handling, and a suitable overhead crane for material handling.

Many of the above elements will be addressed by using NuMI-style components and general target station layout as the design costs and operational characteristics are well understood for NuMI. In addition, manpower is a significant cost driver for new projects and utilizing or slightly modifying existing design concepts minimizes cost impact.

The general target chase (i.e., beam space) shielding requirements will be met by utilizing a shield pile layout nearly identical to that of NuMI for 400kW operation. The nuSTORM target station shielding specifies 4 feet of steel surrounded by 3 feet of concrete, with vertical shielding requirements for sky-shine requiring 9 feet of steel with 6 in of borated polyethylene for prompt neutron shielding. Fig. 20 shows a cross-section of the target pile just downstream of the horn position. Several key elements appear in Fig. 20, including the Duratek steel (now Energy Solutions) shielding block stack around the chase perimeter. These shielding blocks measure 26x52x52 in. with a corresponding weight of 10 tons each. The current nuSTORM conceptual layout requires approximately 140 Duratek blocks. As a cost benchmark, NuMI purchased a quantity

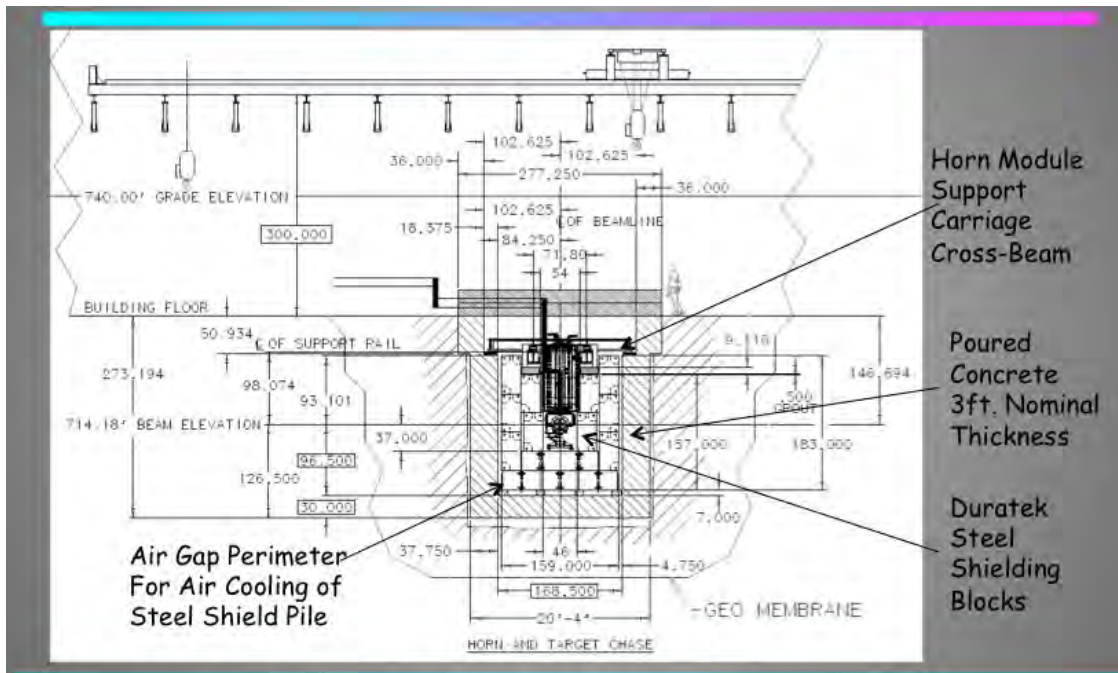


Figure 20: nuSTORM target pile and beamline chase cross-section downstream of horn looking in beam-upstream direction.

of 500 Duratek blocks at a price of \$226 per block (1.13 cents per pound). This underscores the benefit of using Duratek blocks, as they represent a significant source of very inexpensive steel.

Fig. 20 also depicts the horn-positioning module supported by a rigid I-beam carriage structure that is supported on an isothermal surface for accurate alignment during beam operation. Fig. 21 of this shielding configuration, as seen during NuMI construction, highlights additional detail. It is envisioned that this component mounting scheme and shield pile arrangement will be used for the target, horn, and capture quadrupoles.

Hot component handling and failed component replacement is addressed in the inherent design of the NuMI-style module that provides for remote handling capability. Component replacement is addressed by the use of a NuMI-style workcell that has a rail landing area identical to the beamline chase and allows for remote placement of the module into the workcell, after which a remotely operated door is closed and shielding hatch covers placed over the top-center of the module space to allow personnel access to the module top for remote disconnects and component servicing. Fig. 22 provides a sense of scale of the NuMI workcell during construction with the target module inside for trial hot handling practice. The above noted elements are incorporated into the target station conceptual layout as an input to the civil facility construction. Fig. 23 gives a plan view of the current version of the target station layout. Note that the layout incorporates a drop hatch and rail cart for rigging material into the complex for construction and removing failed components in a shielded transportation cask for long-term storage. A morgue is included in the layout for temporary storage of radioactive elements and failed component cool-down. The active functional area includes the target shield pile and beamline chase and an area that will be likely separated by a masonry wall to house power supplies, RAW water skids and a chase air handling system.

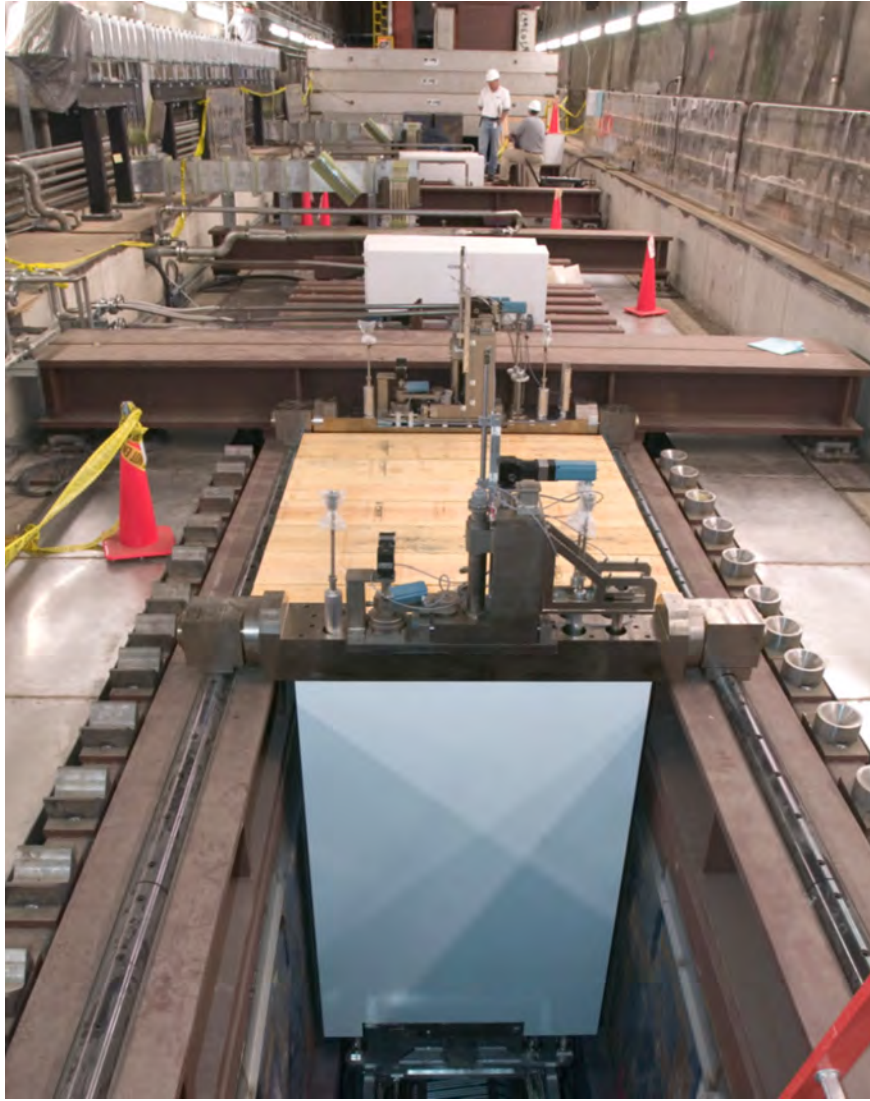


Figure 21: NuMI target pile chase, target module, and carriage I-beam support structure depicting target module installed in Duratek-lined beamline chase (view is upstream of target module looking downstream).

4.2.2 Pion Production Target

The nuSTORM baseline target is very similar to the NuMI low energy target used in the MINOS and MINER ν A run from CY2005 thru CY2012. This style of target has undergone significant analysis and optimization during that time period. When properly constructed and qualified by sufficient QA steps during construction, the target has been successfully operated for 6×10^{20} protons on target (NuMI target NT-02) at beam powers near 400kW and 4.4×10^{13} protons per pulse. Target replacement is, therefore, not expected for the 10^{21} POT exposure for nuSTORM.

Since the energy deposition is proportional to atomic number, Z , this style of low- Z target has been specified and successfully used in several neutrino experiments when coupled with a large depth of field focusing device, such as the magnetic focusing horn, to achieve high pion yields at a range of energies dependent upon the relative placement of target to horn. For the NuMI low energy beamline with 4.4×10^{13} protons on target, the energy deposition per pulse was calculated at 5.1 kJ per pulse. For the 400kW



Figure 22: NuMI Workcell for hot handling operations and failed component replacement. Image shows NuMI target module in the workcell for a hot handling procedure dry run during NuMI construction

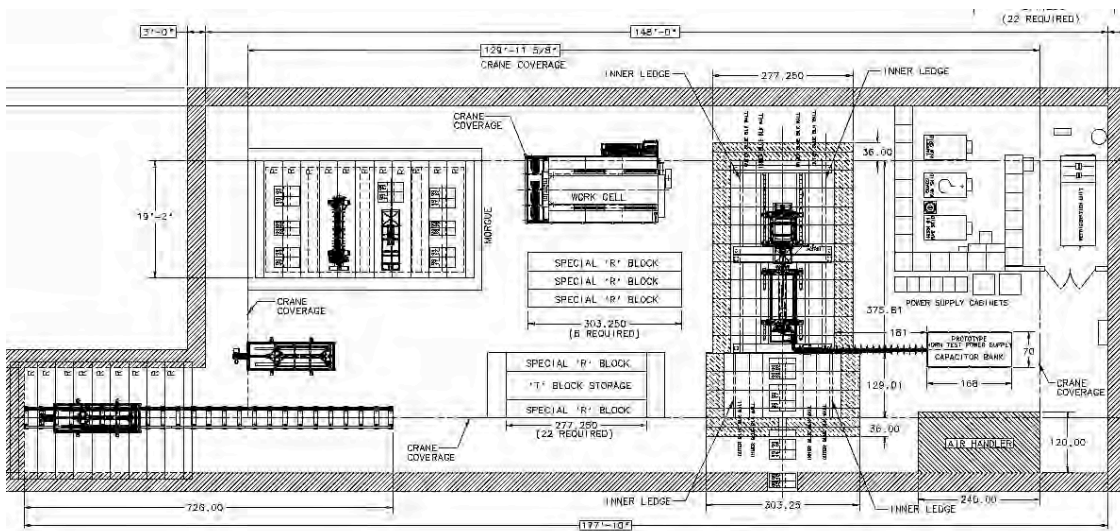


Figure 23: nuSTORM target station main level plan view.

case cycle time of 1.87 seconds, the average power into the graphite is approximately 2.7kW. Scaling to nuSTORM with 0.8×10^{13} protons per pulse and a cycle time of 1.33 seconds, one expects a total average power of 770W. Note that these targets have successfully operated at much higher power levels.

Graphite possesses favorable material properties for pulsed-beam operation to minimize dynamic stress waves and thermal stress gradients including high thermal conductivity, relatively high specific heat capacity, relatively low thermal expansion and Young's Modulus of elasticity, possesses reasonable strength when considering the above properties, and is able to survive at high temperatures in the absence of an oxidizing

(i.e., oxygen) environment. Scaling from the NuMI experience to the nuSTORM expected power levels and the integrated yearly proton on target value, the graphite should not experience significant material irradiation damage for the specified beam parameters for several years of operation.

Physically, the nuSTORM current baseline design will consist of a 2-interaction length POCO graphite grade ZXF-5Q fin-style target. The target construction consists of 47 graphite target segments each 2 cm in length, 15mm in vertical height, and 6.4mm in width. The nominal target overall length is 95 cm, with the fins being brazed to a cooling pipe on the top and bottom surfaces of the graphite fin. Cooling of the target fins from beam interaction is accomplished via conduction of heat through the graphite fin to the cooling pipe water. The target core assembly is encapsulated in a thin-wall (0.4mm) aluminum tube to minimize pion absorption and capped at each end by a 0.25mm thick beryllium window. This allows the target canister to be evacuated and back-filled with helium to minimize graphite oxidation and provides a conduction path for cooling the outer aluminum tube at higher beam powers (note that for the NuMI low energy configuration the target inserts 60cm into the horn and not much external airflow is available for convection cooling on the outer surface of the aluminum tube). In addition, the thin-wall aluminum tube provides containment to mitigate the spread of radioactive contamination from target material degradation due to large amounts of beam exposure.

Colleagues from IHEP in Protvino, Moscow Region fabricated all NuMI low energy targets for the MINOS/MINER ν A running that ended in CY2012. Towards the last $1\frac{1}{2}$ years of that run period, enhancements to the targets were made at Fermilab, including a prototype core fabrication of a complete ZXF-5Q graphite fin target brazed to a titanium cooling pipe. Analysis has shown this combination to be more robust than the prior targets which used a Russian proprietary grade of high-chromium steel cooling pipe. It is likely that some amount of engineering effort will be required to repackage and slightly redesign the low energy target for nuSTORM use, but given our experience and knowledge base, this effort is viewed as low risk and not requiring large amounts of manpower for redesign.

Efforts are ongoing to investigate the use of a medium-Z target material (e.g., Inconel 718) to enhance pion yield (see Section 4.2.2.1), but this effort will need to provide a thorough analysis of target material energy deposition and thermal-mechanical response as well as understanding the additional heat load input to the horn inner conductor from a higher-z target material.

Fig. 24 delineates the basic design of the nuSTORM target, which in the baseline configuration is very similar to the NuMI low energy targets. As previously noted, the NuMI target is designed in conjunction with the horn inner conductor shape to optimize neutrino production in the 1 to 3 GeV region. This low energy range is achieved by inserting the target 60cm into the field free bore-region of the horn. The target is mounted on a target carrier frame that allows for target z-motion of 2.5m along the beamline. This entire carrier frame is mounted to the positioning module and allows for different target to horn spacing or simply provides the means to insert the target into the horn for normal low energy running. Fig. 25 demonstrates the target to horn relationship.

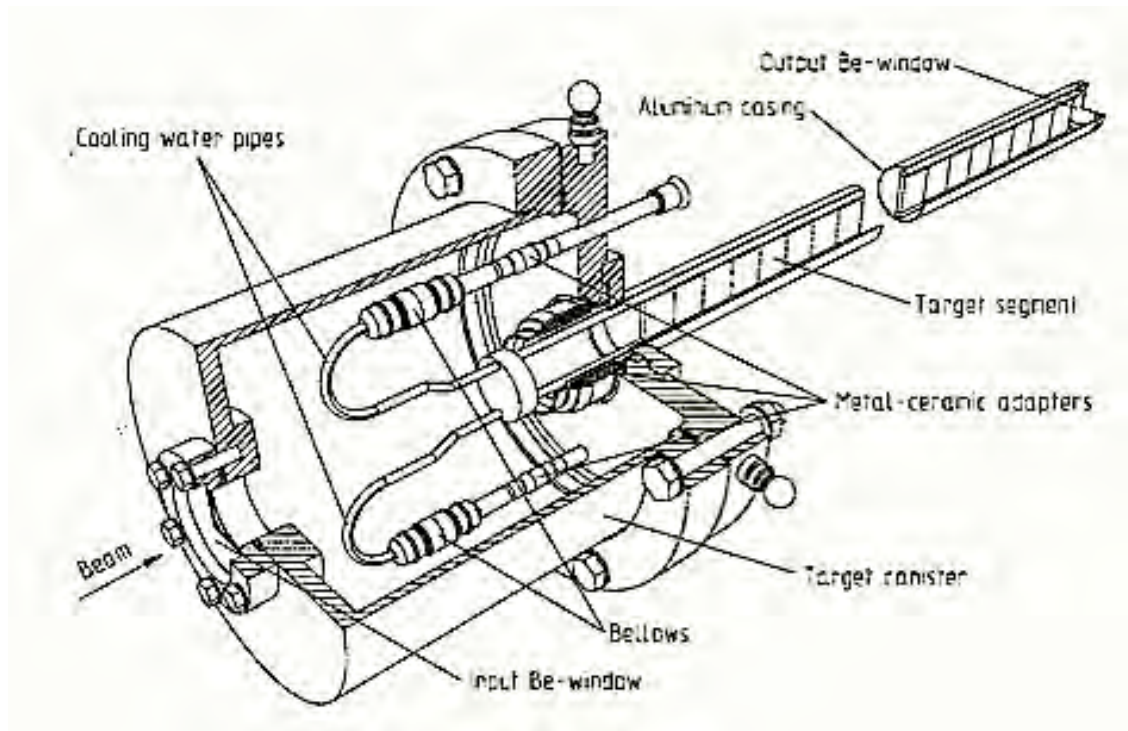


Figure 24: NuMI-style low energy graphite fin target.

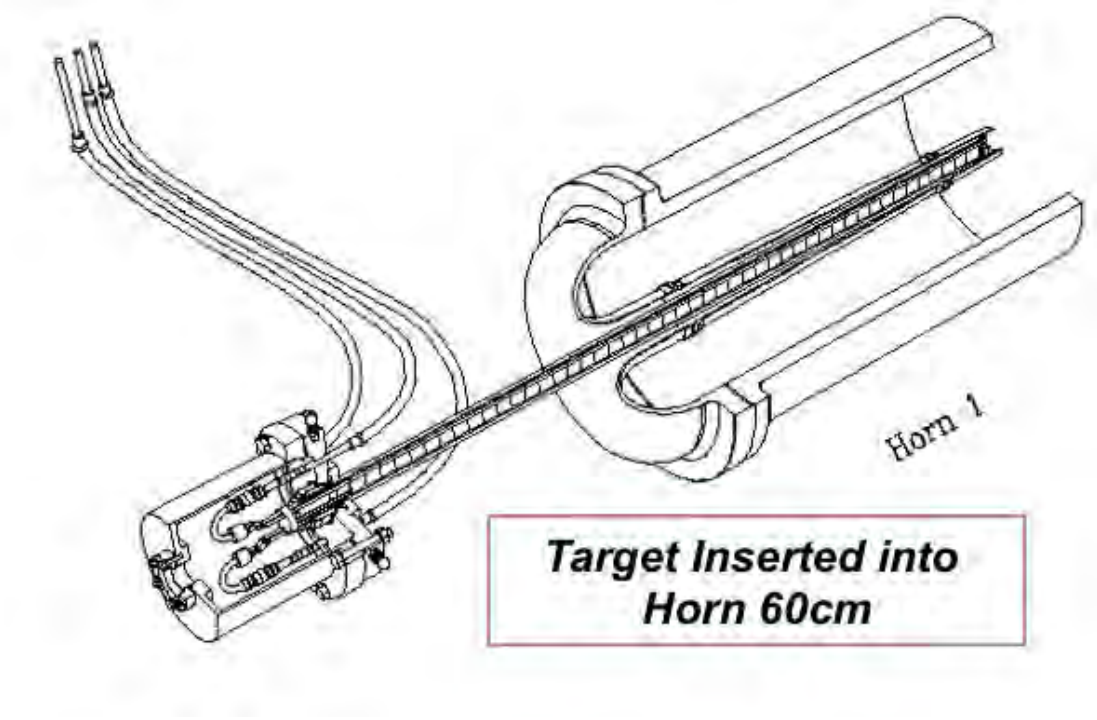


Figure 25: NuMI-style graphite fin target in low energy position (inserted into horn 60 cm).

Table 3: MARS simulation parameters.

Parameter	Value	Unit
Material	Inconel 718	
Diameter	0.7	cm
Length	25	cm
Beam Energy	120	GeV
Beam $\sigma_{x,y}$	1.1	mm
Protons/pulse	8×10^{12}	
Pulse Length	1.6	μsec
Rep Rate	0.752	Hz

4.2.2.1 INCONEL target option

Although the baseline nuSTORM production target material is graphite, as can be seen in Section 4.3, the use of Inconel gives up to a 40% increase in pion yield. We have, therefore, considered a cylindrical Inconel 718 target with a 7 mm diameter and 25cm length. We have performed an energy deposition study with MARS and have determined the resulting thermal load. Based upon this thermal loading, the resulting temperature profiles for a variety of cooling methods were evaluated, with forced Helium cooling being the leading candidate for further analysis. Basic structural analyses were also carried out, showing that further work on the structural design is necessary due to plastic deformation. Further analysis will be necessary to look into target geometry optimization, more realistic temperature estimates via CFD, dynamic stress effects, and resonant effects on the structural analyses.

4.2.2.1.1 MARS 15 Model and Results

MARS15(2013) was used to calculate the energy deposition into the target from the incoming proton beam. The simulation parameters used are listed in Table 3. Based on these inputs, the energy deposition was compiled and converted to a format suitable for input into ANSYS. The total heat loading on the target is about 4.8kW. A graphical, axisymmetric plot of energy deposition along the target is shown below in Fig. 26. The beam travels from left to right starting at the (0,0) point. It should also be noted that MARS15 predicts high DPA rates in the radial center of the target, with a peak of about 40DPA/yr. assuming continuous beam. Material degradation from radiation damage must be considered in the final design and target lifetime calculations. A plot of DPA/yr is shown in Fig. 27.

4.2.2.1.2 ANSYS Simulations

ANSYS 14 was used to calculate the thermal and structural effects from the energy deposition. Temperature dependent material properties for Inconel 718 were used for all analyses, containing information up to 1200C. A simple axisymmetric model was used for initial scoping to minimize simulation time. PLANE77 (thermal) and PLANE183 (structural) elements were used with a size of 0.4mm to accurately capture the

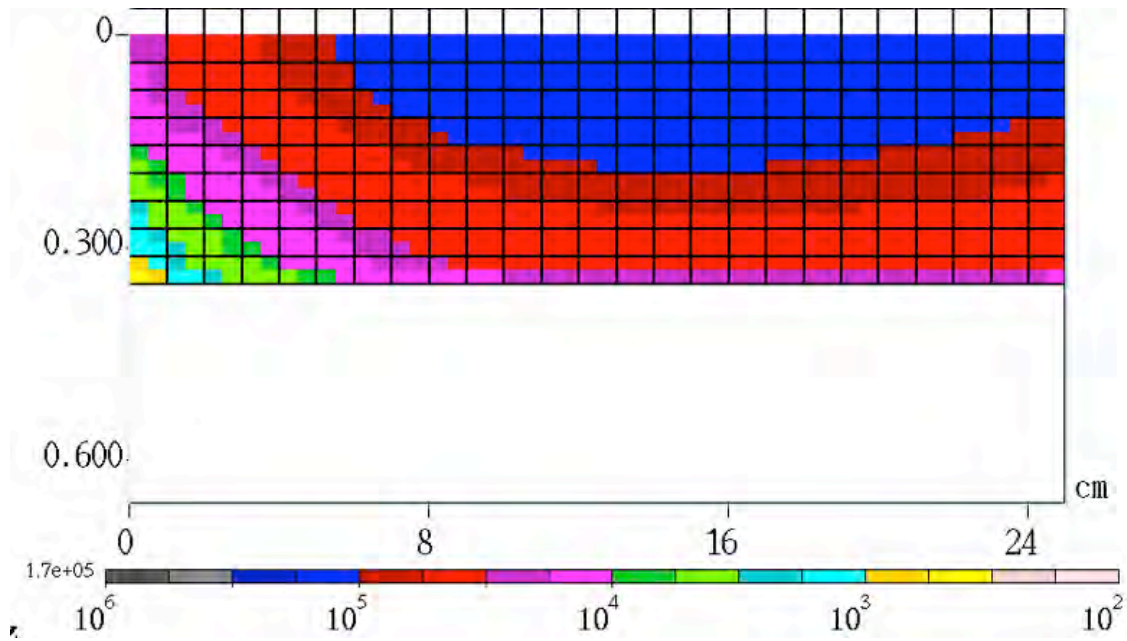


Figure 26: Energy deposition [mW/g] into Inconel target.

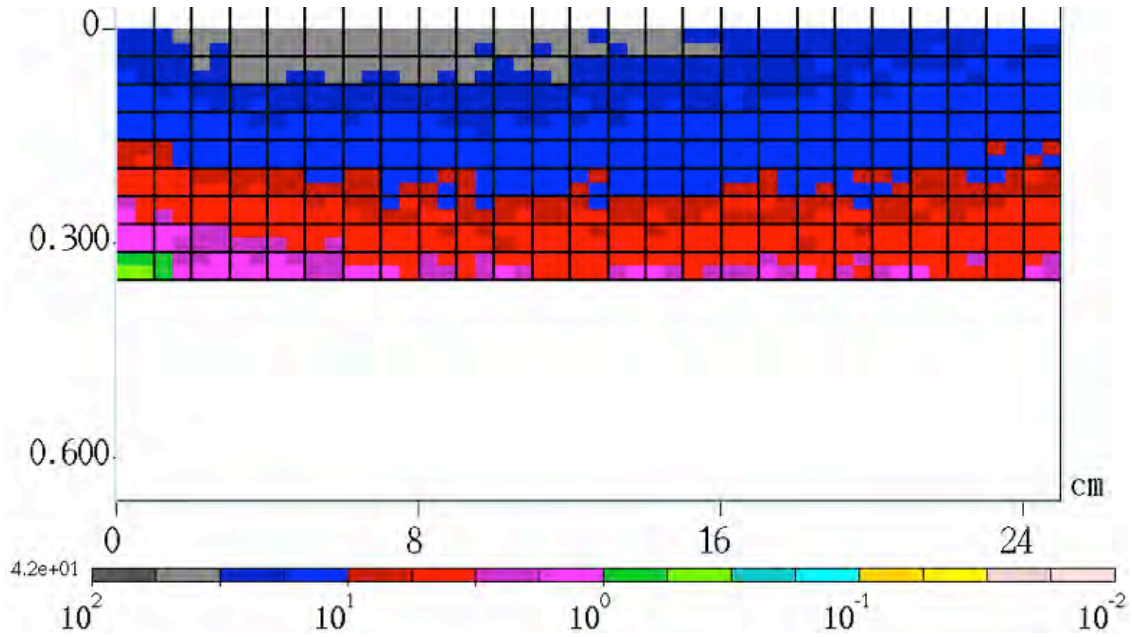


Figure 27: DPA/yr in Inconel target.

maximum temperatures (≈ 3 elements per beam sigma) and resulting stress effects.

Thermal analysis - Steady state

A convection boundary condition was placed on the outer surfaces of the target and was varied according to different cooling methods as shown in Table 4 with a reference temperature of 22°C . It should be noted that this model does not include heating of the fluid from flow along the surface. The fluid is also assumed to be in full contact with the outer wall of the target. A full CFD model will be necessary for accurate predictions of all temperatures. Pressurized Helium and Air both appear to be possible candidates for further study,

Table 4: Steady state target temperatures with varying convection coefficients.

Method	Convection Coefficient	Peak Steady-State Temperature	Peak Fluid Interface Temperature
	[W/(m ² -K)]	°C	°C
Forced Helium (1 bar, mach 0.3)	1500	1065	950
Forced Air (10 bar, mach 0.3)	3500	580	420
Forced Helium (10 bar, mach 0.3)	10000	370	160
Water (5 m/s)	25000	310	80
Water (10 m/s)	45000	285	55

Table 5: Steady state + transient target temperatures with varying convection coefficients.

Method	Convection Coefficient	Peak Steady-State Temp.	Peak Temp. After Pulse	Peak Fluid Interface Temp.
	[W/(m ² -K)]	°C	°C	°C
Forced Air (10 bar)	1500	-	-	-
Forced Helium (1 bar)	3500	580	1010	585
Forced Helium (10 bar)	10000	370	820	350
Forced Water (5 m/s)	25000	310	770	270
Forced Water (10 m/s)	45000	285	750	245

and water cooling will need further analysis to determine the fluid interface temperature during the dynamic effect of a beam pulse. Optimizations of target geometry would also be helpful to reduce peak steady state temperatures.

Thermal analysis - Steady state + transient effects

To understand the peak temperatures at both the radial center of the target and the cooling fluid interface immediately following a pulse, a transient thermal analysis was run. This run uses a steady state heat generation profile until the steady state temperature is reached (5-15s), then the heat generation from a pulse is applied for 1.6μs.. A typical plot of temperature vs. time is shown in Fig. 28. Using the same bound-

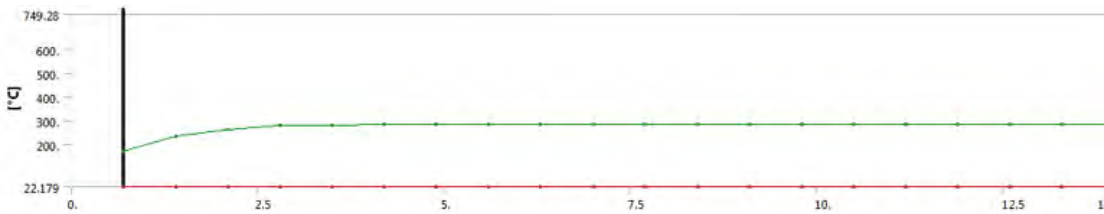


Figure 28: Typical temperature vs time profile for transient case.

ary conditions and convection coefficients as in the previous analysis, peak steady state temperature, peak temperature in the target, and peak temperature at the fluid interface were found and are shown in Table 5. Temperatures listed are obtained immediately after the pulse is applied. Water cooling can be ruled out

since the interface temperature is above the boiling point of water and could lead to accelerated corrosion and pitting. Pressurized Helium appears to be the leading candidate for cooling based on this analysis.

Structural analysis - Steady state + transient effects

A structural model was constructed in the same manner as the previous transient thermal analysis to determine the stress state of the target both in the steady state condition and after a beam pulse. Refer to Fig. 28 for a plot of temperature over time. Instead of modeling multiple pulses of the beam and observing the ratcheting effect, this method saves some simulation time while giving accurate results. Only two cooling cases were analyzed: the compressed air and helium cases. A large temperature gradient develops across a very short radial dimension which induces a large stress in the material. A typical plot of maximum principal stress is shown in Fig. 29 where blue colors are compressive and red colors are tensile. The peak

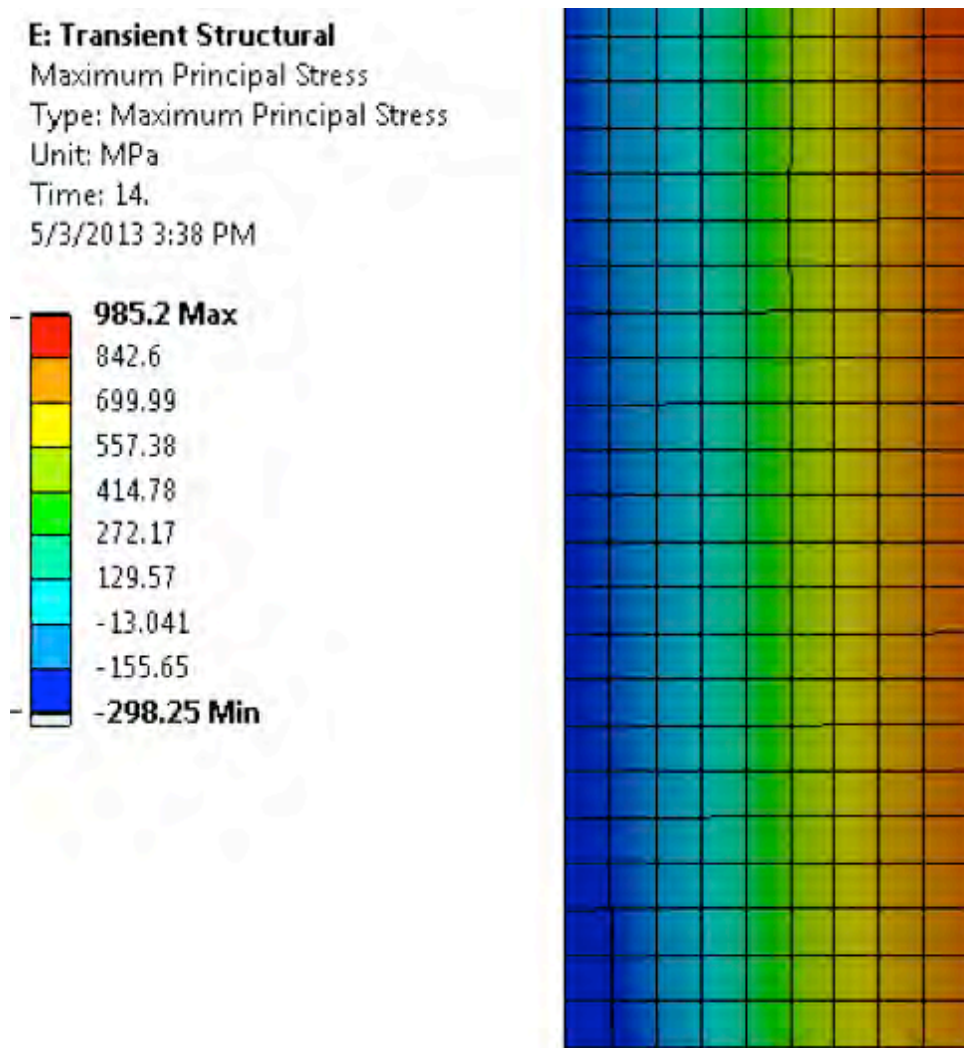


Figure 29: Typical maximum principal stress plot.

steady-state Von-Mises stress for both cooling cases is listed in Table 6. Fig. 30 shows the temperature dependent tensile yield and ultimate strengths for Inconel 718. Steady state stresses are relatively low for this material and temperature. Next the transient effects were evaluated with a beam pulse after the steady state temperature was obtained. Table 7 shows the peak tensile and compressive temperatures and stresses.

Table 6: Steady state VM stress for various cooling methods.

Convection Coefficient W/(m ² -K)	Peak VM Stress Steady State Mpa (ksi)
3500	300 (44)
10000	380 (55)

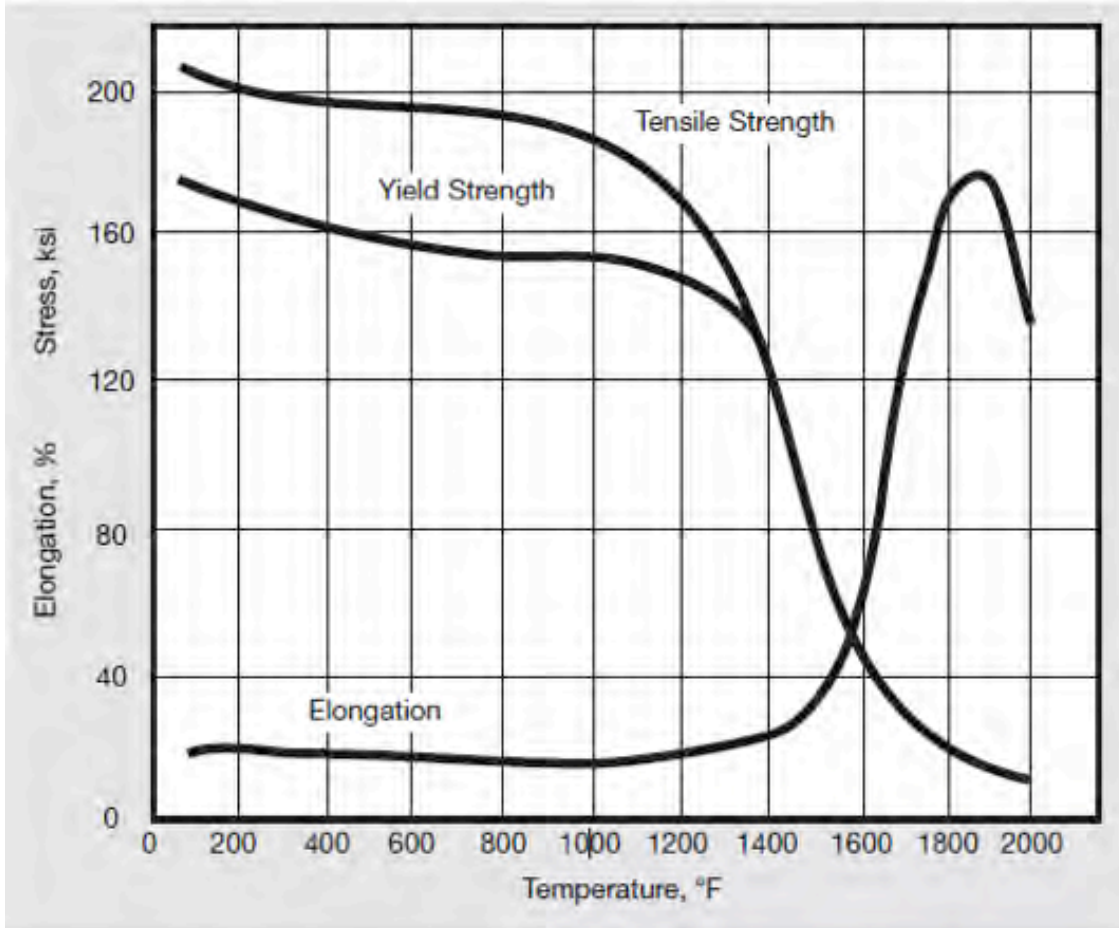


Figure 30: Tensile yield, ultimate strength, and elongation as a function of temperature.

While it is possible that there will be no yielding on the outer surface of the target, yielding will most likely occur in the radial center of the target where the compressive stress is concentrated. Segmenting the target may help reduce the stress and should be further analyzed.

Table 7: Peak temperatures and stresses after pulse.

Convection Coefficient W/(m ² -K)	Peak VM Stress Steady State [Mpa (ksi)]
3500	300 (44)
10000	380 (55)

4.2.2.1.3 Next steps in the analysis for Inconel

Further analysis of the Inconel target is needed in at least four areas to get a better understanding of the beam response and interaction with the target geometry:

- Fluid flow and heating (CFD)
- Dynamic stress effects
- Resonant effects
- Target segmentation

CFD analysis is needed to determine a more accurate temperature profile of the target. ANSYS thermal calculations do not include fluid heating and this can only be evaluated with a CFD model. Dynamic stress waves have been shown to increase stress in a target by up to $2\times$ depending on the geometry because of the interference between stress waves. This effect needs to be studied with a longer run after the beam pulse with short time-steps. Resonant modes of the target will also come into play and have an effect on the dynamic stress. A modal analysis needs to be conducted to determine the resonant modes of the target and any supporting structures. The effect of target segmentation needs to be looked at, including all of the previously described areas for further analysis. It has also been suggested to investigate the additional heat loading onto the horn because of the larger shower coming from the target. This can be done with a fairly simple MARS model. While a completely solid target will undergo plastic deformation during a beam pulse, optimization of the geometry may allow the target stresses to be reduced to an acceptable range. Geometry optimization would also allow lower steady state temperatures and stresses. Further analysis is needed to define an optimized target geometry.

4.2.3 Focusing Horn

The primary objective of the focusing horn is to collect the pion phase space from the target interaction with the primary beam and focus the pions such that they are stably captured by the quadrupole magnets just downstream of the horn. This leads to several requirements of the horn for reliable and effective operation:

1. The horn should have the ability to operate at sufficiently high currents to maximize the pion focus to the capture quadrupoles.
2. The inner conductor of the horn should be sufficiently thin to minimize absorption of off-axis pions produced in the target that enter the field region of the horn.
3. The horn should have sufficient structural integrity to survive a reasonable number of high current pulses with adequate safety factor to allow reliable operation for several years of service.
4. The horn should employ radiation hard structural and insulating materials.
5. The horn should employ suitable corrosion resistant materials to mitigate erosion of the thin-wall inner conductor from the water-cooling spray.
6. The horn should be designed with a fabrication tolerance that assure uniform field region.
7. The horn should have adequate cooling plus overhead for the expected 100kW beam power and the 200kA (or higher) current pulse.

The horn provides large depth of field focusing compatible with a low-Z target in order to maximize the pion capture rate. This is achieved by using a target with a small cross-sectional component, allowing pions to

exit the target material without further interaction. Pions with a nearly on-axis trajectory travel through the field free region of the inner bore of the horn inner conductor, while pions with an off-axis trajectory travel through the thin-wall inner conductor of the horn into the field region and are subject to a focusing force vector which is proportional to the vector cross-product of instantaneous velocity and the magnetic field vector. The selection of the horn inner conductor thickness is a balance between minimizing pion absorption, providing adequate thickness to allow for precision machining and fabrication, and providing adequate margin of safety relative to the operating stress that results from the thermal components of secondary particle beam heating, joule heating from current pulse resistive heating, and the magnetic forces from the interaction of current density and magnetic field. Fig. 31 outlines the basic structure of the focusing horn. nuSTORM expects to utilize the successful operational experience of NuMI and the baseline configuration

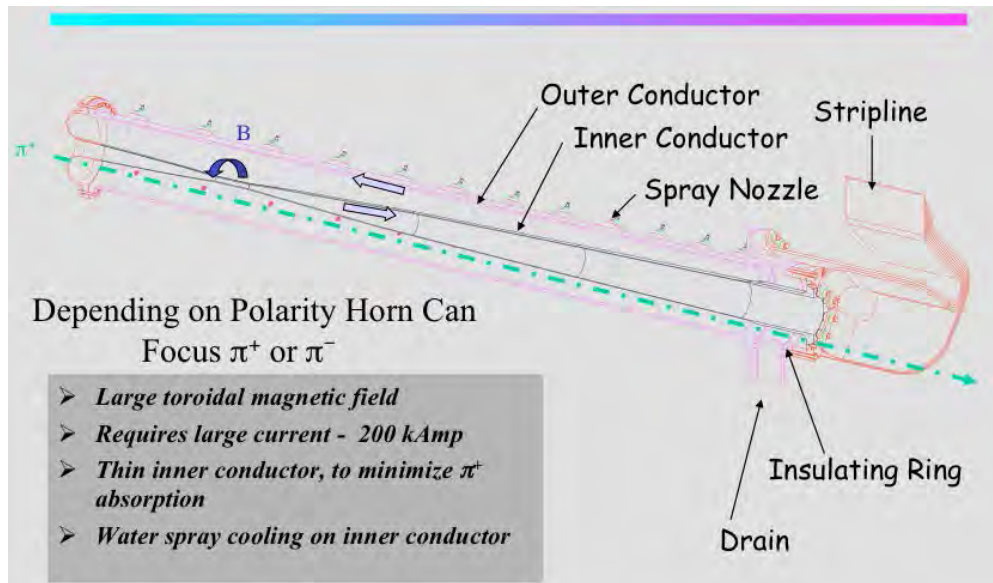


Figure 31: NuMI Horn 1 basic elements.

consists of a NuMI style horn 1. The NuMI horns have operated successfully for more than 3×10^6 pulses of operation with average beam powers as high as 375kW and maximum proton intensity of 4.4×10^{13} protons per pulse. In addition, significant analysis and understanding of horn operational characteristics and reliability exists at Fermilab. Such analyses are well documented for the 400kW NuMI/MINOS beamline operation, the upcoming 700kW NOvA era running, and the 700kW baseline LBNE configuration. In particular, a recent analysis for LBNE indicates that it may be possible to operate with adequate safety margin at horn currents of 230kA for the 700kW LBNE beam. It is believed that this scenario is likely for nuSTORM, but would require some further analysis to understand the entire load history to accurately calculate the fatigue life safety factor. Note that the fatigue life value is highly dependent upon the coupled loading of beam thermal energy, current pulse resistive heating, and magnetic loading stress value and sign (compressive vs. tensile stress), as the magnitude of alternating stress has significant effect on fatigue life.

An additional consideration for using a NuMI-style horn is that Fermilab has the infrastructure for, and experience in, fabricating all NuMI horns to date. A few examples of the benefits to such expertise in addressing the challenge of fabricating these critical devices include the in-house CNC welding and straightening of the inner conductor structure to very high tolerances ($\pm 0.25\text{mm}$), a ready design with little modification for nuSTORM use (i.e., minimizes the cost of manpower for a new design or substantial redesign), and the

infrastructure to pulse test and field map a finished horn before beamline installation. Fig. 32 shows a NuMI horn 1 ready spare. The design package of a new-style horn, module, and supporting hardware represents



Figure 32: NuMI Horn 1 ready spare.

significant manpower effort and cost. It is envisioned that nuSTORM can utilize most elements of the NuMI design. The fabrication costs and operating envelope are well understood. Minor design effort does exist in that the horn hangers and module for NuMI are designed for a beamline pitch of 58 milliradians. The nuSTORM beamline pitch is level. Such modifications to the NuMI horn and module design are viewed as relatively minor when compared to more substantial redesign efforts and are expected to pose negligible risk to design reliability. Fig. 33 depicts the NuMI horn 1 package during the installation into the NuMI beamline. Similar hardware is specified for the target, the first 2 capture quadrupoles immediately downstream of the horn, and beam spray protection collimators for those quadrupole magnets.



Figure 33: NuMI Horn 1 and positioning module installation in beamline chase.

4.2.4 Quad capture magnets

Unlike a conventional neutrino beam where pions exiting the horn are launched into a decay pipe, in nuSTORM we have a pion capture and transport channel that brings the pions to the decay ring. The initial part of this section (just downstream of the horn) consists of two quadrupoles. They are in the target chase and see a very large radiation dose and, therefore, must be radiation hard. There are two options we have considered: MgO insulated magnets and HTS magnets following the BNL magnets designed for the Facility for Rare Isotope Beams (FRIB) [196]. The current baseline design for the capture quad section of the pion capture channel (see Section 4.3.1) uses magnets with a 40 cm bore. However, recent studies indicate that a 20 cm bore can be used with little loss in flux. This would allow nuSTORM to use the same magnets that have been designed for FRIB and would represent a substantial cost savings. These magnets

have a unique design and technology that uses Second Generation (2G) High Temperature Superconductor (HTS). These magnets can survive very intense heat and radiation loads (up to 10 MGy/year) and can operate at an elevated temperature of 40 K, instead of $\simeq 4$ K as needed in the conventional low temperature superconductors. This elevated temperature has a major impact regarding the heat load on the cryogenic system. In addition, a large temperature margin allows for robust operation by tolerating a large local increase in temperature. These HTS quadrupoles are the baseline design for the fragment separator region of FRIB which follows the production target ($\simeq 400$ kW beam power).

The BNL magnet group [197] has looked into the feasibility of a HTS Quad with a 40 cm bore for nuSTORM. Fig. 34 shows the preliminary magnetic design and field contour for this magnet.

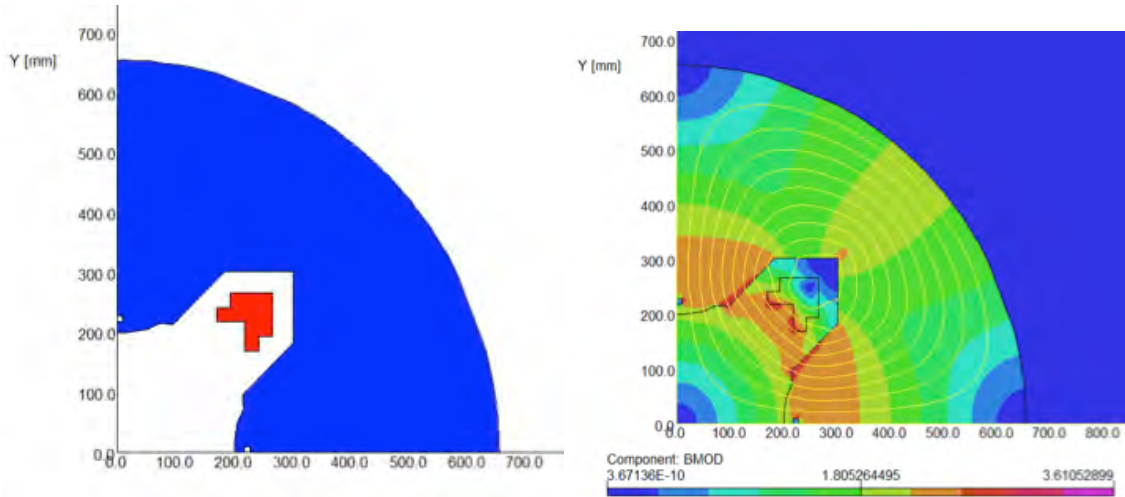


Figure 34: A preliminary magnetic design of the HTS quadrupole for nuSTORM (model on left and field contours on right). In the model, blue represents the warm steel and the red represents the HTS conductor.

4.3 Pion Production

It is known that the maximum pion yield can be achieved with a target radius ~ 3 times the proton beam RMS size. The optimal target length depends on the target material and the secondary pion momentum. The results of our optimization study are presented in Table 8. We see that approximately $0.11 \pi^+$ /POT can be collected into $\pm 10\%$ momentum acceptance off medium to heavy targets with very small proton beam size (0.15 mm). The difference between the yield from heavy and light targets becomes about $2 \times$ smaller for a more realistic beam size with a 1 mm RMS. These numbers are for pions within the 2 mm-radian acceptance of the decay ring.

We have considered two options for pion capture, a lithium lens and a horn. The existing Fermilab lithium lens has a working gradient of 2.6 Tesla/cm at 15 Hz. The optimal distance between the target and lens center is about 25 cm. Pions produced into 2 mm-radian acceptance have a wide radial distribution, however. The current lens with its 1 cm radius would only capture 40% of the pions within the desired $\pm 10\%$ momentum acceptance. With a 2 cm lens radius, the pion capture efficiency increases to 60%. Further improvement could be achieved by increasing the lens gradient, but increasing the gradient reduces the focal length. Maximal efficiency would reach 80% with a 4 Tesla/m gradient and a 2 cm lens radius. These parameters

are beyond the state-of-art for an operating lens, however, and the target's downstream end would need to be very close to the lens. Therefore for nuSTORM, we have abandoned consideration of a Li Lens.

The existing NuMI horn was considered as the other capture option. Different target materials, horn currents, beam RMS sizes (target size) were studied. Results for a 60 GeV/c proton beam are presented in Table 9. We see that approximately 0.06 π^+ /POT can be captured into a $\pm 10\%$ momentum acceptance for 1 mm (σ_b^{rms}) proton beam. Yield can be increased by using a heavy target and very small beam transverse size.

Approximately twice as many pions can be collected with 120 GeV/c protons and a NuMI-style horn. Table 10 presents the pion yield dependence on target material for this configuration. Using a conventional graphite target and NuMI horn at 230 kA, 0.094 π^+ /POT are captured after the horn into the 2 mm-radian acceptance. The phase-space distribution of pions downstream of the target and downstream of the horn are shown in Fig. 35 and Fig. 36, respectively. The ellipse shown in each figure represents the acceptance of the muon decay ring.

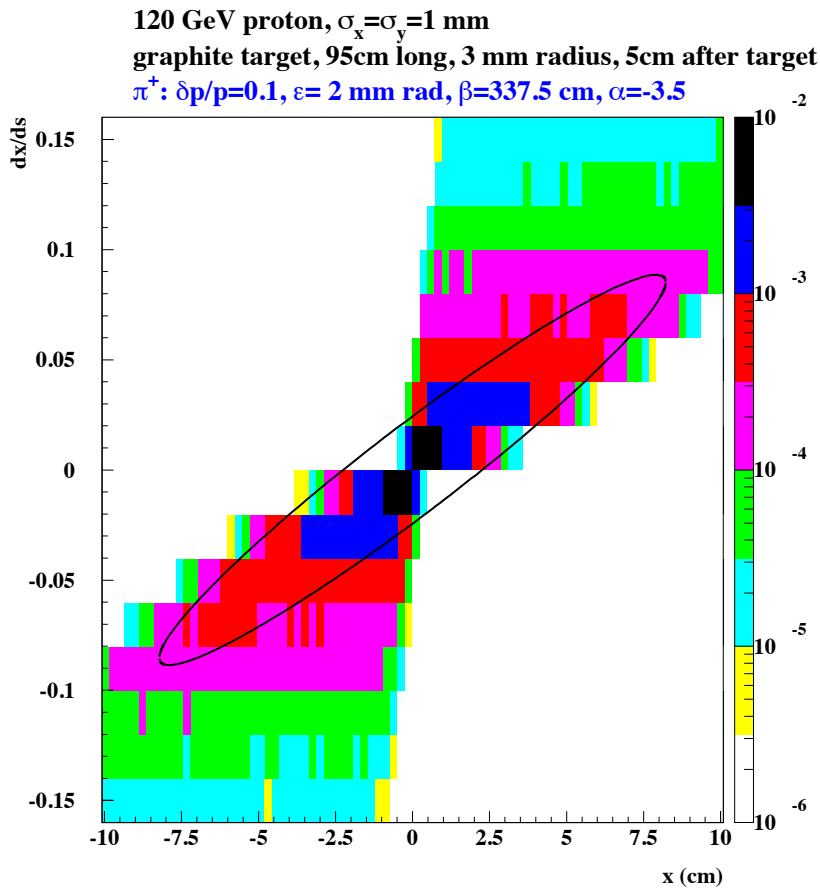


Figure 35: Phase-space distribution of pions 5 cm downstream of target

Table 8: π^+ yield/POT at 60 GeV into 2 mm radian acceptance.

material	momentum (GeV/c)	$\pm 15\%$	$\pm 10\%$	$\pm 5\%$	target length (cm)	density (g/cm ³)	σ_b (mm)
Carbon	3	0.085	0.056	0.028	27.3	3.52	0.15
Carbon	5	0.099	0.067	0.033	32.2	3.52	0.15
Inconel	3	0.131	0.087	0.044	19.2	8.43	0.15
Inconel	5	0.136	0.091	0.045	27.0	8.43	0.15
Tantalum	3	0.164	0.109	0.054	15.3	16.6	0.15
Tantalum	5	0.161	0.107	0.053	21.3	16.6	0.15
Gold	3	0.177	0.118	0.059	18.0	19.32	0.15
Gold	5	0.171	0.112	0.056	20.0	19.32	0.15
Gold	5	0.143	0.094	0.047	20.0	19.32	1.
Graphite	5	0.085	0.057	0.028	95.0	1.789	0.15
Graphite	5	0.096	0.064	0.032	95.0	1.789	1.

Table 9: π^+ yield/POT at 60 GeV into 2 mm radian acceptance after NuMI horn. 5 ± 0.5 GeV/c

material	Current (kA)	horn length (cm)	σ_b^{rms} (mm)	α	β (cm)	yield
Gold	300	200	0.15	0.	522.5	0.081
Gold	300	300	0.15	0.	427.5	0.077
Gold	300	200	1.	0.	542.5	0.063
Gold	300	300	1.	0.5	812.5	0.059
Graphite	300	200	.15	0.5	257.5	0.049
Graphite	300	300	.15	0.5	202.5	0.049
Graphite	300	200	1.	0.5	282.5	0.056
Graphite	300	300	1.	0.	217.5	0.056
Graphite	185	200	1.	-1	682.5	0.056
Graphite	185	300	1.	-0.5	987.5	0.054
Graphite	230	200	1.	0.5	512.5	0.057
Graphite	230	300	1.	0.5	687.5	0.056
BeO	230	200	1.	0.	602.5	0.065
BeO	230	300	1.	0.5	782.5	0.066
NuMI tgt	185	200	1.1	-1.5	852.5	0.056
NuMI tgt	185	300	1.1	-0.5	1097.5	0.054

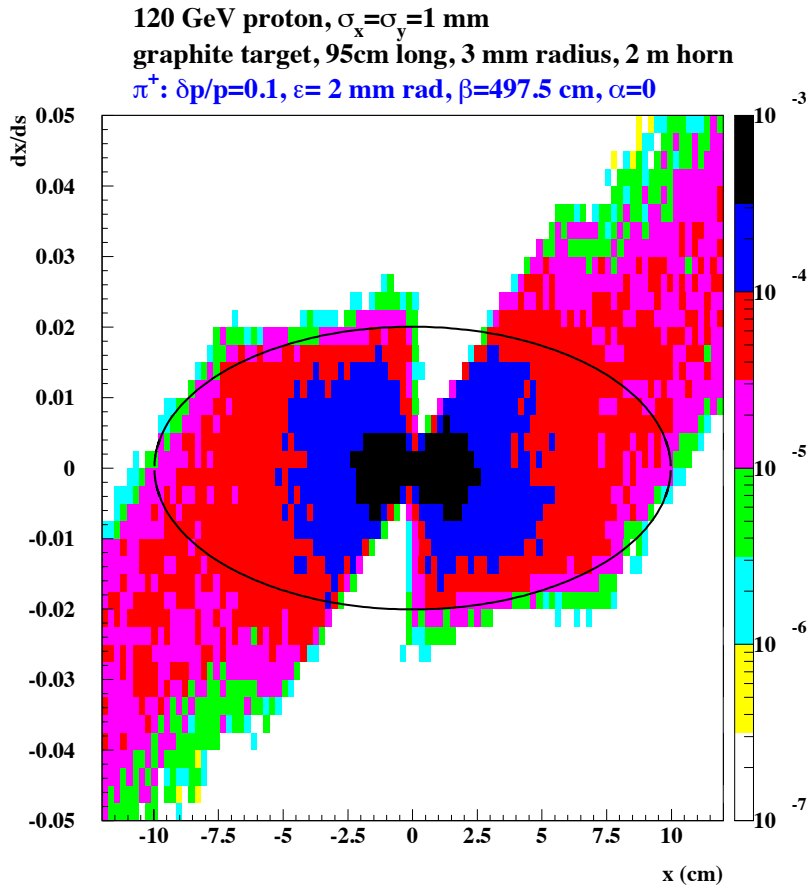


Figure 36: Phase-space distribution of pions downstream of the horn

Table 10: π^+ yield/POT after NuMI horn at 230 kA. 120 GeV/c proton beam with 1 mm RMS. 5 ± 0.5 GeV/c

material	target length(cm)	horn length (cm)	α	β (cm)	yield (2 mm rad)	yield ($r \leq 20$ cm)
Graphite	95	200	0.	497.5	0.094	0.156
Graphite	95	300	0.5	612.5	0.092	0.139
BeO	66	200	0.	547.5	0.115	0.174
BeO	66	300	0.5	742.5	0.115	0.154
Inconel	38	200	-0.5	742.5	0.122	0.179
Inconel	38	300	0.5	897.5	0.126	0.157

4.3.1 Capture and Transport

As described in the previous section, the pion distribution at the downstream end of the horn was simulated and generated by MARS. A shell script code converts the MARS output to G4beamline[198] conventions, for the simulation's input beam. Another script converts OptiM[199] lattice output to G4beamline lattice input. Assuming a phase space acceptance of 2 mm-rad for pions, it is convenient to fit the transverse distribution to a 2D Gaussian with a covariance matrix obtaining Courant-Snyder(CS or Twiss) parameters

[200]. These parameters are used for the matching condition for designing the transport line.

From the downstream end of the horn, we continue the pion transport line with several quadrupoles. Although conventional from the magnetic field point of view, these first two to four quads still need special and careful treatment in their design in order to maximize their lifetime in this high-radiation environment. As described in Section 4.2.4, the FRIB quads show promise regarding suitability for nuSTORM.

The injection scenario for the decay ring, that will be discussed in section 4.4, needs a large dispersion value at the injection point. This dispersion D_x and its derivative D'_x both need to be matched to 0 at the horn, although this is not necessarily the case in the whole transport line. Considering this constraint, along with the requirement for spacing between target station and decay ring, two bending dipoles are used in the transport line, which bend the pions to the ring injection point. Two long drift spaces are reserved before the first dipole for collimators to reduce downstream radiation. The field strength, which is roughly 4.9 T in the first dipole, requires it to be superconducting. The long distance between the two dipoles separates the pions from the high energy residual protons, which go into a separate transport line and then into a MI-style proton absorber.

4.3.2 Proton Absorber

The current design uses the same proton absorber size that the MI uses, which is 4.3 meters both in width and height, and 10.7 meters in length. Because the first dipole also bends the protons at the same time as the π^+ or π^- , another long dipole is needed in order to bend protons back to their initial direction. No other magnets are needed for the proton absorber beam line. The layout drawing is shown in Fig. 37. The absorber, located at ~ 32 meters after the second dipole in Fig. 37 collects 43.5% of the total energy from the residual protons remaining after the target.

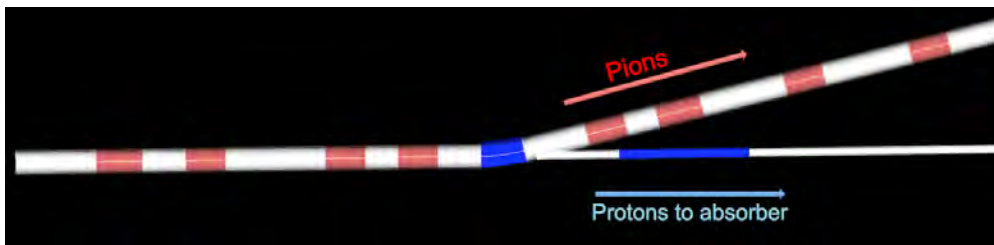


Figure 37: Separation of proton absorber beamline and pion transport line. Red: quadrupole, Blue: dipole, White: drift.

4.4 Pion Injection

The straight-section FODO cells were designed to have betatron functions β_x, β_y (the Twiss parameters) optimized for beam acceptance and neutrino beam production. Larger betatron functions increase the beam size, following $\sigma \sim \sqrt{\beta \epsilon_{rms}}$ and cause aperture losses. On the other hand, smaller betatron functions increase the divergence of the muon beam and also the divergence of the resulting neutrino beams, following $\delta\theta \sim \sqrt{\epsilon_{rms}/\beta}$. In addition, the muon beam emittance is increased by the angular divergence from pion decay following $\delta\epsilon \sim \beta_t \theta_{decay}^2 / 2$.

Balancing these criteria, we have chosen FODO cells with $\beta_{\max} \sim 30.2$ m, and $\beta_{\min} \sim 23.3$ m for the 3.8 GeV/c muons, which for the 5.0 GeV/c pions, implies ~ 38.5 m and ~ 31.6 m pion's β_{\max} and β_{\min} , respectively.

Fig. 38 shows results of a set of simulations used in determining this lattice design, showing the relative increase in angular divergence obtained by reducing the FODO betatron functions.

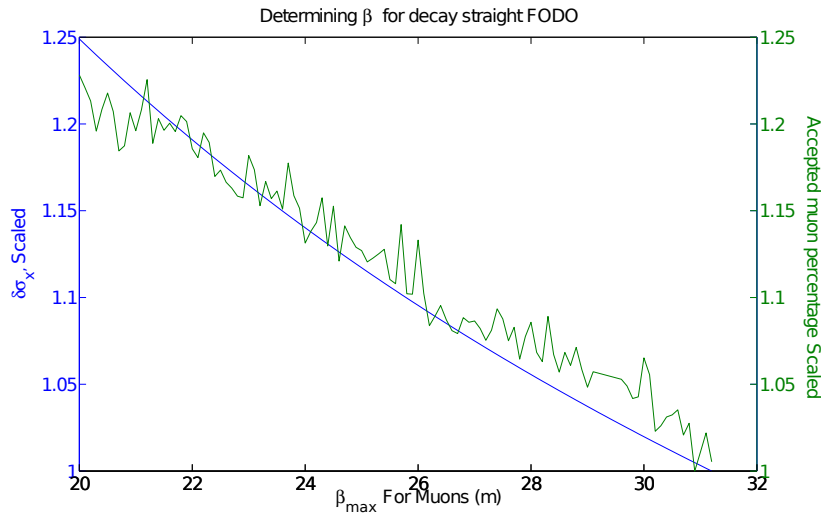


Figure 38: Determining the Twiss for decay straight FODO cells

As discussed in section 4.3.1, a large dispersion D_x is required at the injection point, in order to achieve beam separation. A carefully designed “beam combination section”, or “BCS”, can readily reach this goal. The schematic drawing of the injection scenario is shown in Fig. 39. The pure sector dipole for muons in the

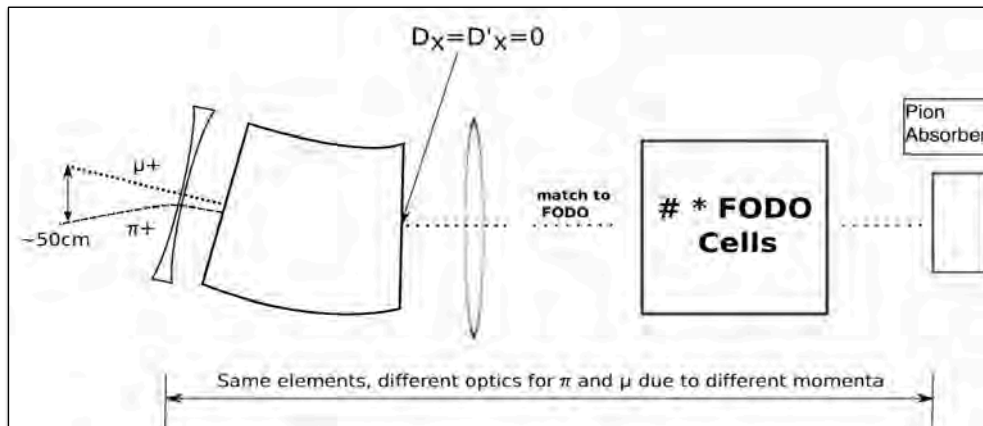


Figure 39: The schematic drawing of the injection scenario

BCS has an exit angle for pions that is non-perpendicular to the edge, and the pure defocusing quadrupole in the BCS for muons is a combined-function dipole for the pions, with both entrance and exit angles non-perpendicular to the edges. The corresponding optics from OptiM are shown in Fig. 40. The BCS will be followed by a short matching section to the decay FODO cells (see Fig. 41). At the other end of the

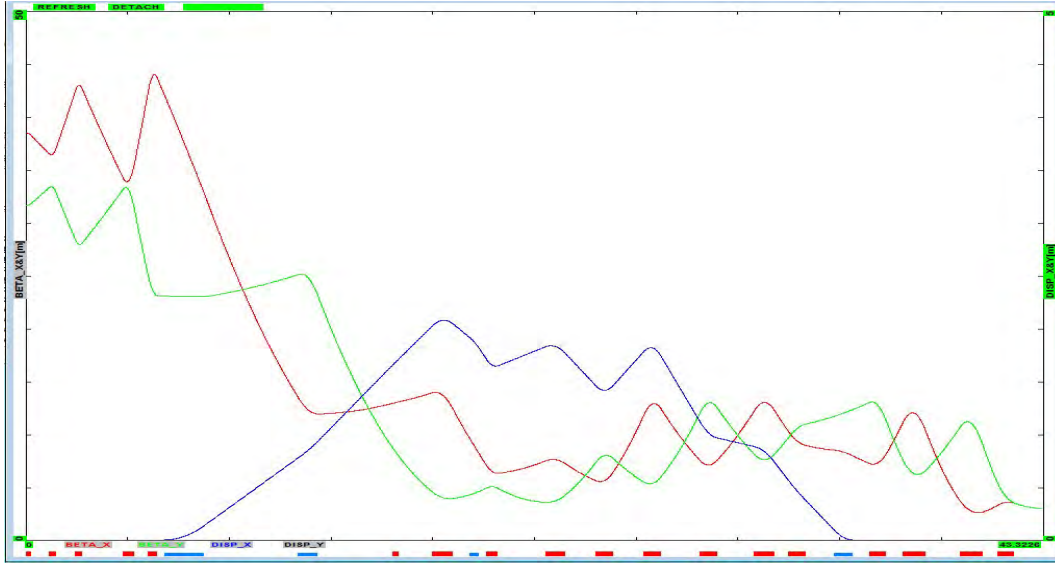


Figure 40: The optics of π transport and injection. The optics shown start in the decay straight and end at the downstream end of the horn (left to right).larger

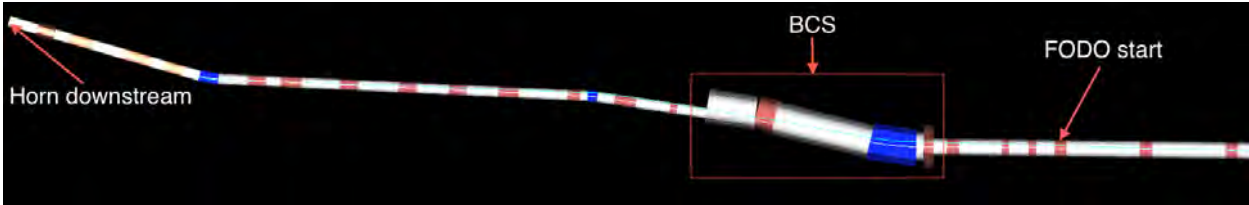


Figure 41: The G4beamline drawing from horn downstream to the FODO cells. Red: quadrupole, Blue: dipole, White: drift.

decay straight, another BCS will be used to extract the pions which have not decayed. This BCS, which also extracts muons within the pion momentum range, will be discussed in Section 4.6.

The performance of the injection scenario can be gauged by determining the number of muons at the end of the decay straight using G4beamline. We were able to obtain 0.012 muons per POT (see Fig. 42). These muons have a wide momentum range (beyond that which the ring can accept, $3.8 \text{ GeV}/c \pm 10\%$) and thus will only be partly accepted by the ring. The green region in Fig. 42 shows the $3.8 \pm 10\% \text{ GeV}/c$ acceptance of the ring, and the red region shows the high momentum muons which will be extracted by the BCS. This will be discussed in Section 4.6. The muons also occupy a very large phase-space, which is also shown in Fig. 42.

4.5 Decay ring

We have investigated both a FODO racetrack and a FFAG racetrack for the muon decay. The FODO ring that is described in detail below uses both normal and superconducting magnets. A FODO lattice using only normal-conducting magnets ($B \lesssim 1.8\text{T}$) is also being studied. The racetrack FFAG (RFFAG) is described in Section 4.5.2. Table 11 gives a comparison between the FODO and the RFFAG with regard to the ratio of the total number of useful muons stored per POT, assuming that capture off the target and injection into the ring are the same for both. Acceptance for all the decay ring options we are considering will be studied and

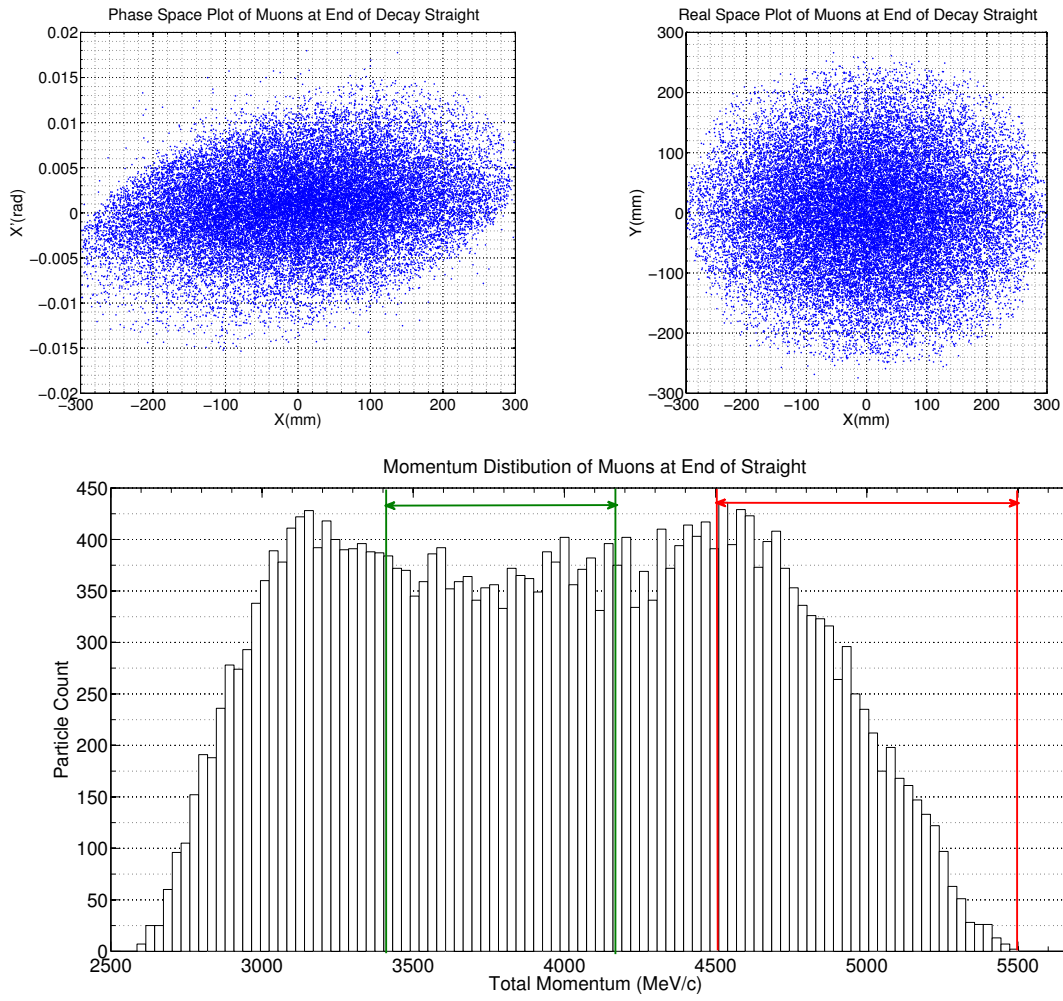


Figure 42: The muon real space distribution (upper right), phase space distribution (upper left) and the muon momentum distribution (lower) at the end of decay straight.

compared in order to obtain a cost/performance optimum but, for now, the FODO lattice is the nuSTORM baseline.

Table 11: Relative μ yield for FODO vs. RFFAG rings

Parameter	FODO	RFFAG
$L_{straight}$ (m)	185	240
Circumference (m)	480	606
Dynamic aperture A_{dyn}	0.6	0.95
Momentum acceptance	$\pm 10\%$	$\pm 16\%$
π /POT within momentum acceptance	0.094	0.171
Fraction of π decaying in straight (F_s)	0.52	0.57
Ratio of $L_{straight}$ to ring circumference (Ω)	.39	.40
Relative factor ($A_{dyn} \times \pi$ /POT $\times F_s \times \Omega$)	0.011	0.037

4.5.1 FODO ring Lattice Design

A FODO ring with such a large phase space and momentum acceptance has not been previously developed [201]. Here we propose a compact racetrack ring design (480 m in circumference) based on large aperture, separate function magnets (dipoles and quadrupoles). The ring is configured with FODO cells combined with DBA (Double Bend Achromat) optics. The ring layout, including pion injection/extraction points, is illustrated in Fig. 43 and the current ring design parameters are given in Table 12. The design



Figure 43: Racetrack ring layout. Pions are injected into the ring at the Beam Combination Section (BCS). Similarly, extraction of pions and muons at the end of the production straight is done using a mirror image of the BCS.

Table 12: Decay ring specifications

Parameter	Specification	Unit
Central momentum P_μ	3.8	GeV/c
Momentum acceptance	$\pm 10\%$	
Circumference	480	m
Straight length	185	m
Arc length	50	m
Arc cell	DBA	
Ring Tunes (ν_x, ν_y)	9.72, 7.87	
Number of dipoles	16	
Number of quadrupoles	128	
Number of sextupoles	12	

goal for the ring was to maximize both the transverse and momentum acceptance (around the 3.8 GeV/c central momentum), while maintaining acceptable physical apertures of the magnets. These requirements would drive the lattice design towards strongly focusing (large transverse acceptance) and low chromaticity (large momentum acceptance) optics in the arcs. Furthermore, one side of the arc needs to accommodate pion injection/extraction sections. The stochastic injection, as described in Section 4.4, drives the dispersion value to about 3 m, which puts a serious limitation on the transverse acceptance. The large dispersion at the injection point must be suppressed in the arc. To accommodate this, we have used Double-Bend Achromat (DBA) optics in the arcs, which controls the beam size.

To maintain the compactness of the arc, while accommodating adequate drift space between magnets, we limit the overall arc length to about 50 m, keeping the dipole fields at $\simeq 4$ Tesla. We use DBA optics, which maintains reasonably small values of the beta functions and dispersion. We limit the maximum field

at the quadrupole magnet pole tip to be less than 5 Tesla. The overall arc optics are illustrated in Fig. 44. The decay straight requires much larger values of the beta functions ($\simeq 27$ m average) in order to assure

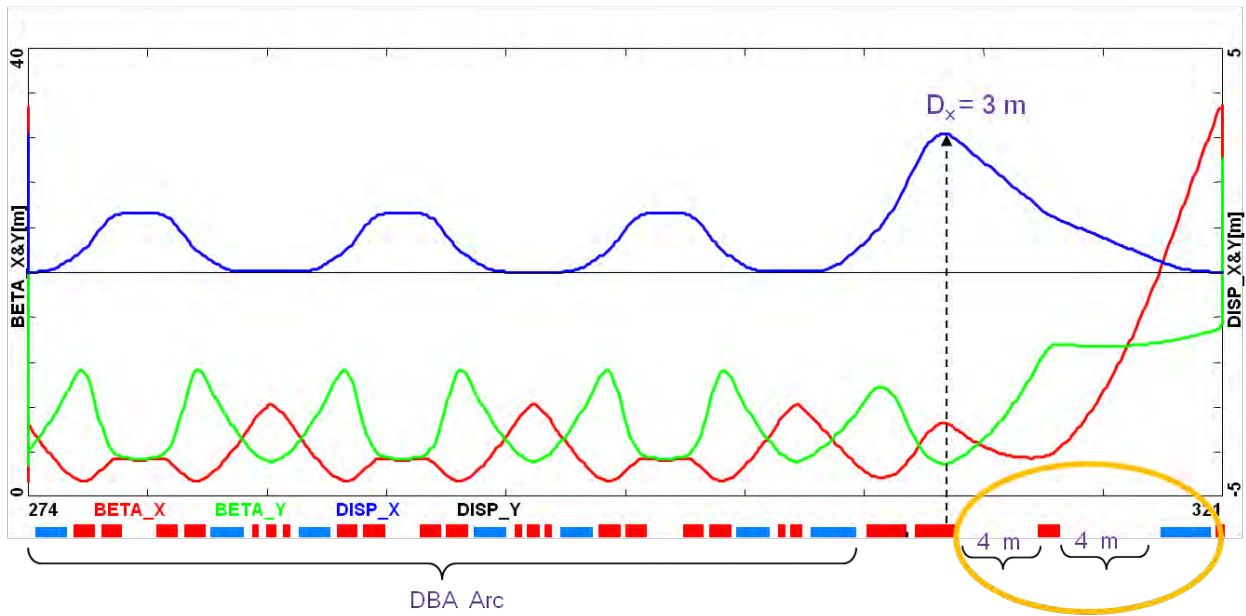


Figure 44: The arc optics illustration

small beam divergence ($\simeq 7$ mrad). The resulting muon beam divergence is a factor of 4 smaller than the characteristic decay cone of $1/\gamma$ (0.029 at 3.8 GeV). The decay straight is configured with a much weaker focusing FODO lattice ($\simeq 15$ deg. phase advance per cell). It uses normal conducting, 30 cm radius aperture quads with a modest gradient of 2 Tesla/m (0.6 Tesla at the pole tip).

The opposite straight, which is not used for neutrino production, can be designed with much smaller beta functions. This straight also uses normal conducting quads, but with a gradient of 11 Tesla/m (1.6 Tesla at the pole tip).

Finally, the racetrack ring optics are illustrated in Fig. 45. It features a low-beta straight matched to a 180 deg. arc and is then followed by a high-beta decay straight connected to the other arc with a compact telescope insert. The complete ring optics and the single turn beam loss histogram are shown in Fig. 46.

It is very likely that the large beam loss where the beam enters the decay ring arc is caused by beta chromaticity, or “beta beat” raised by momentum difference. It is observed in simulations that, with sextupole and octupole correction, the orbit response of off-momentum particles can be well corrected (See Fig. 47 and Fig. 48). Using particle tracking in G4beamline, we are able to achieve approximately 60% beam survival rate, for a Gaussian distributed muon beam, after 100 turns in the ring (without higher-order correctors). This number can be increased when further detailed corrections of tune chromaticity and beta chromaticity are developed.

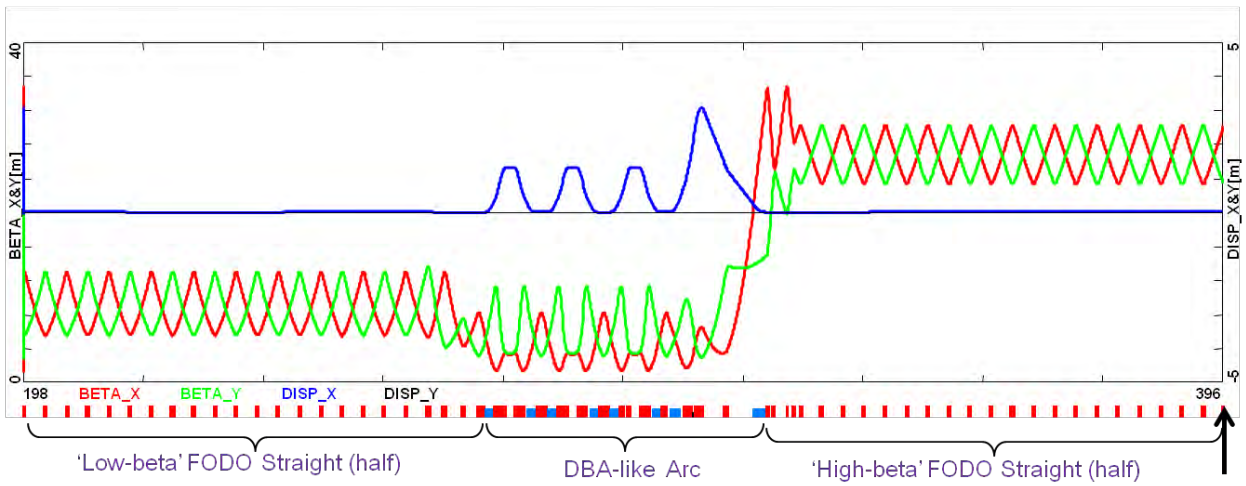


Figure 45: Ring optics.

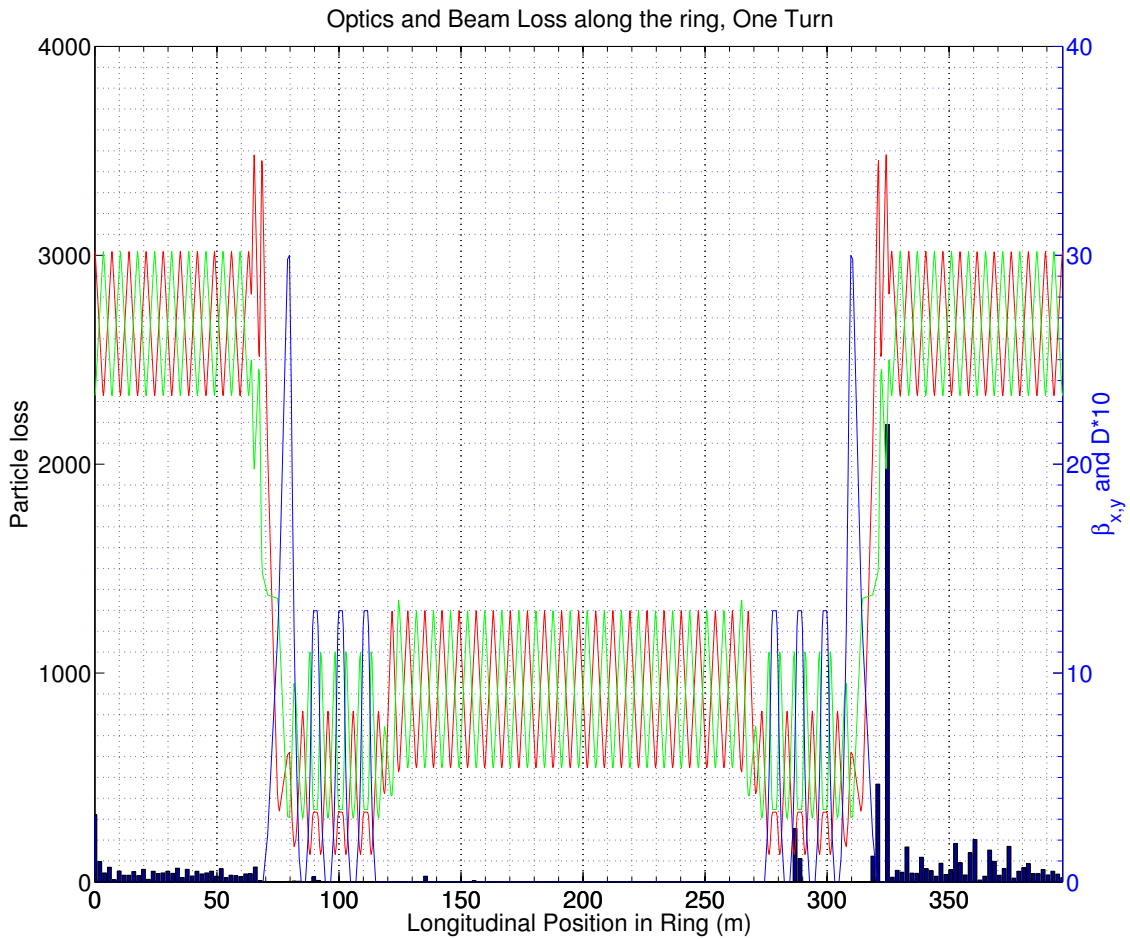


Figure 46: The complete ring optics and single-turn beam loss histogram.

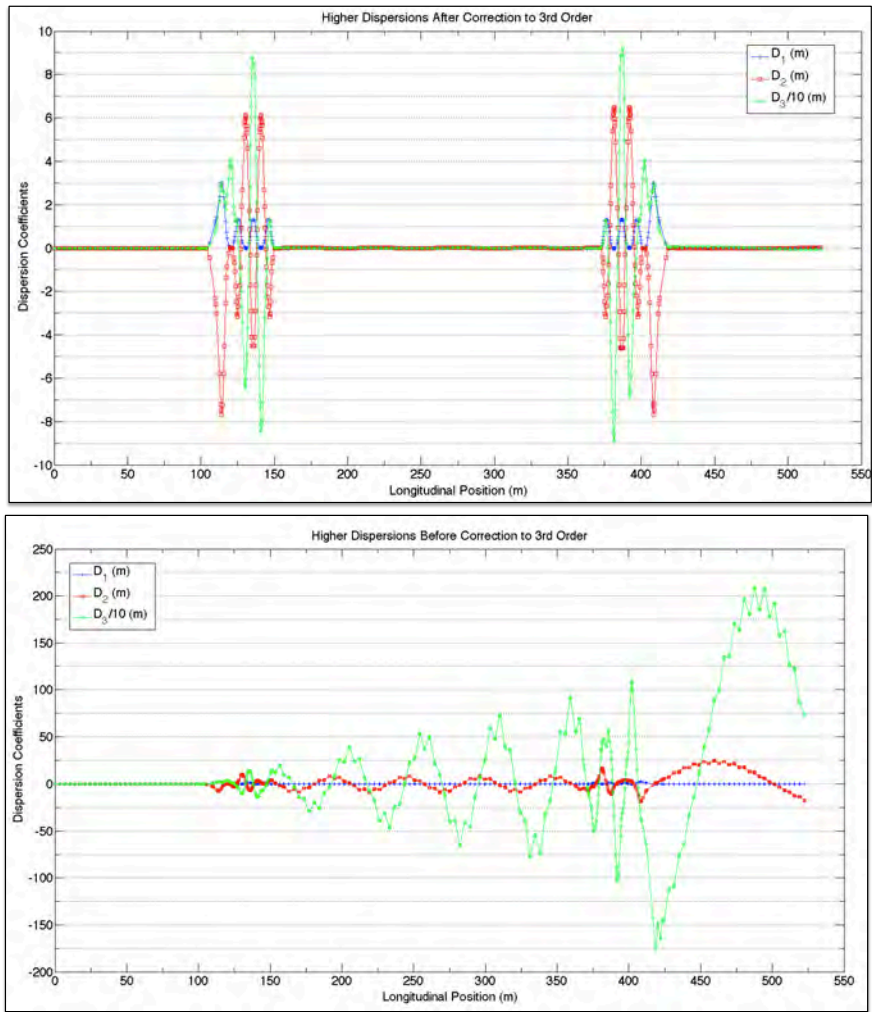


Figure 47: The higher order dispersions (up to 3rd order) before(lower) and after(upper) correction

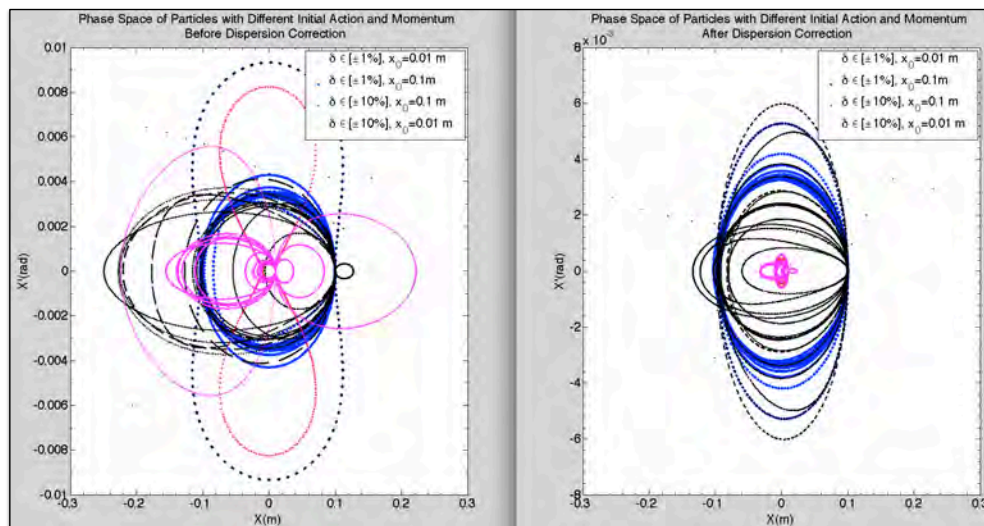


Figure 48: The 100-turn tracking for off-momentum particles before(left) and after(right) correction.

4.5.2 Advanced scaling FFAG

The racetrack FFAG ring is composed of two cell types: a) a straight scaling FFAG cell and b) a circular scaling FFAG cell. There are 40 straight FFAG cells in each long straight section (80 for the whole ring) and 16 circular FFAG cells in each of the arc sections.

4.5.2.1 Straight scaling FFAG cell parameters

In the straight scaling FFAG cell, the vertical magnetic field B_{sz} in the median plane follows:

$$B_{sz} = B_{0sz} e^{m(x-x_0)} \mathcal{F},$$

with x the horizontal Cartesian coordinate, m the normalized field gradient, \mathcal{F} an arbitrary function and $B_{0sz} = B_{sz}(x_0)$. The parameters of the straight scaling FFAG cell are summarized in Table 13. The cell is

Table 13: Parameters of the straight scaling FFAG cell.

Cell type	DFD triplet	
Number of cells in the ring	80	
Cell length	6 m	
x_0	36 m	
m-value	2.65 m^{-1}	
Packing factor	0.1	
Collimators ($x_{min}, x_{max}, z_{max}$)	(35.5 m, 36.5 m, 0.3 m)	
Periodic cell dispersion	0.38 m	
Horizontal phase advance	13.1 deg.	
Vertical phase advance	16.7 deg.	
D ₁ magnet parameters		
	Magnet center	0.2 m
	Magnet length	0.15 m
	Fringe field fall off	Linear (Length: 0.04 m)
	$B_0(x_0 = 36 \text{ m})$	1.28067 T
F magnet parameters		
	Magnet center	3 m
	Magnet length	0.3 m
	Fringe field fall off	Linear (Length: 0.04 m)
	$B_0(x_0 = 36 \text{ m})$	-1.15037 T
D ₂ magnet parameters		
	Magnet center	5.8 m
	Magnet length	0.15 m
	Fringe field fall off	Linear (Length: 0.04 m)
	$B_0(x_0 = 36 \text{ m})$	1.28067 T

shown in Fig. 49. The red line represents the $\simeq 3.8 \text{ GeV}/c$ muon reference trajectory, and its corresponding magnetic field is shown in Fig. 50. Periodic β functions are shown in Fig. 51.

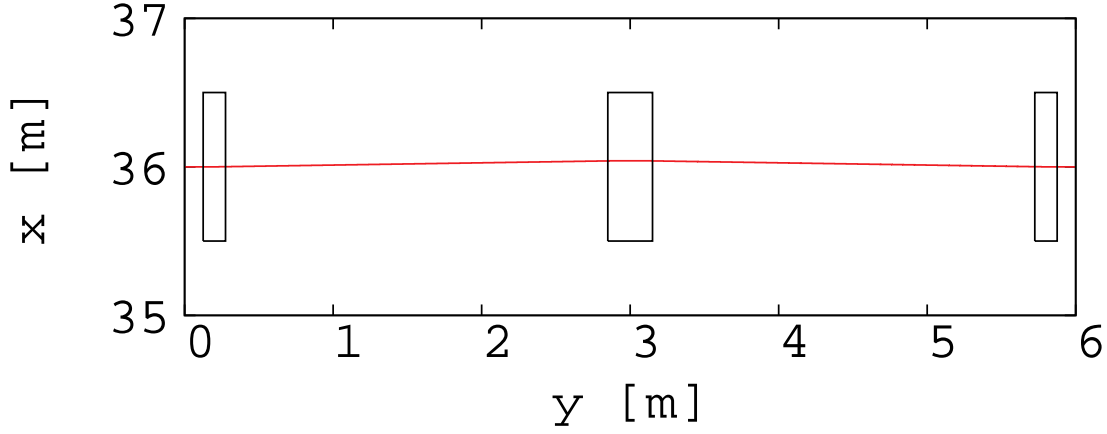


Figure 49: Top view of the straight scaling FFAG cell. The 3.8 GeV/c muon reference trajectory is shown in red. Effective field boundaries with collimators are shown in black.

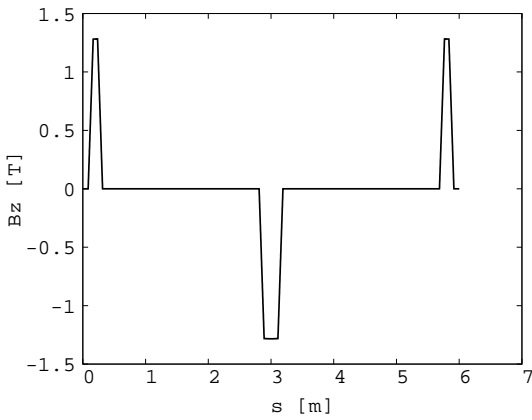


Figure 50: Vertical magnetic field for 3.8 GeV/c muon reference trajectory in the straight scaling FFAG cell.

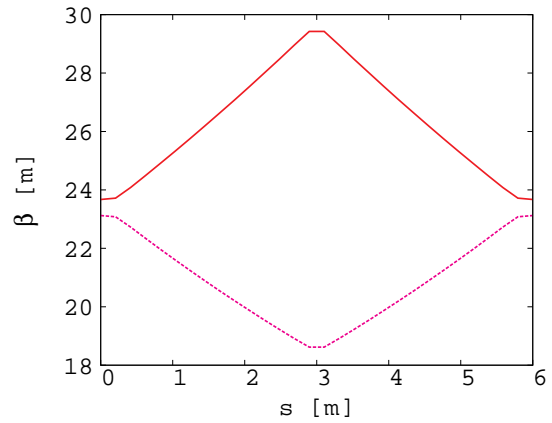


Figure 51: Horizontal (plain red) and vertical (dotted purple) periodic β functions of the straight scaling FFAG cell.

4.5.2.2 Circular scaling FFAG cell parameters

In the circular scaling FFAG cell, the vertical magnetic field B_{cz} in the median plane follows

$$B_{cz} = B_{0cz} \left(\frac{r}{r_0} \right)^k \mathcal{F},$$

with r the radius in polar coordinates, k the geometrical field index, \mathcal{F} an arbitrary function and $B_{0cz} = B_{cz}(r_0)$. The parameters of the circular scaling FFAG cell are summarized in Table 14. The cell is shown

Table 14: Parameters of the circular scaling FFAG cell.

Cell type	FDF triplet	
Number of cells in the ring	32	
Cell opening angle	11.25 deg	
r_0	36 m	
k-value	10.85	
Packing factor	0.96	
Collimators ($r_{min}, r_{max}, z_{max}$)	(35 m, 37 m, 0.3 m)	
Periodic cell dispersion	1.39 m (at 3.8 GeV/c)	
Horizontal phase advance	67.5 deg.	
Vertical phase advance	11.25 deg.	
F ₁ magnet parameters		
	Magnet center	1.85 deg
	Magnet length	3.4 deg
	Fringe field fall off	Linear (Length: 0.1 deg)
	$B_0(r_0 = 36\text{ m})$	-1.55684 T
D magnet parameters		
	Magnet center	5.625 deg
	Magnet length	4.0 deg
	Fringe field fall off	Linear (Length: 0.1 deg)
	$B_0(r_0 = 36\text{ m})$	1.91025 T
F ₂ magnet parameters		
	Magnet center	9.4 deg
	Magnet length	3.4 deg
	Fringe field fall off	Linear (Length: 0.1 deg)
	$B_0(r_0 = 36\text{ m})$	-1.55684 T

in Fig. 52. The red line represents the 3.8 GeV/c muon reference trajectory, and its corresponding magnetic field is shown in Fig. 53. Periodic β functions are shown in Fig. 54.

4.5.2.3 Single particle tracking

Stepwise tracking using Runge Kutta integration in a field model with linear fringe fields has been performed where interpolation of the magnetic field away from the mid-plane has been done to first order. Only single particle tracking has been done so far. We used μ^+ with a central momentum, p_0 , of 3.8 GeV/c, a minimum momentum, p_{min} , of 3.14 GeV/c and a maximum momentum, p_{max} , of 4.41 GeV/c. $\Delta p/p_0$ is thus $\pm 16\%$. The tracking step size was 1 mm. The exit boundary of a cell is the entrance boundary of the next cell.

The ring tune point is (8.91,4.72) at the central momentum, p_0 . Stability of the ring tune has been studied over the momentum range. The tune shift is presented in Fig. 55. The tune point stays within a 0.1 shift in both planes over this momentum range.

Closed orbits of p_0 , p_{min} , and p_{max} particles are shown in Fig. 56. The magnetic field for the p_{max} closed orbit is presented in Fig. 57. Dispersion at p_0 is shown in Fig. 58. β functions for p_0 , p_{min} , and p_{max} are plotted in Fig. 59.

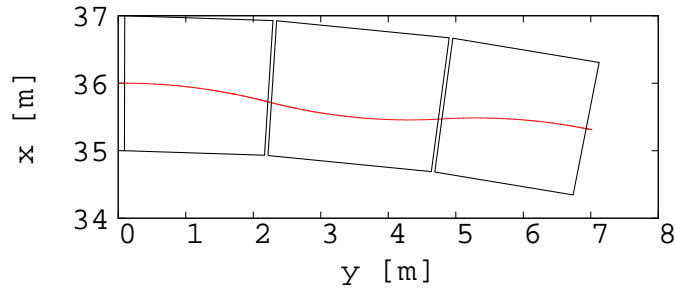


Figure 52: Top view of the circular scaling FFAG cell. The 3.8 GeV/c muon reference trajectory is shown in red. Effective field boundaries with collimators are shown in black.

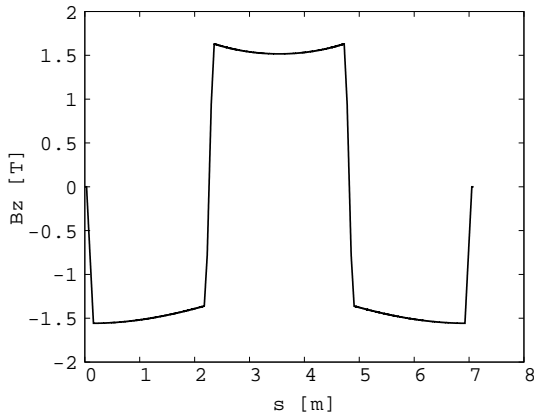


Figure 53: Vertical magnetic field for the 3.8 GeV/c muon reference trajectory in the circular scaling FFAG cell.

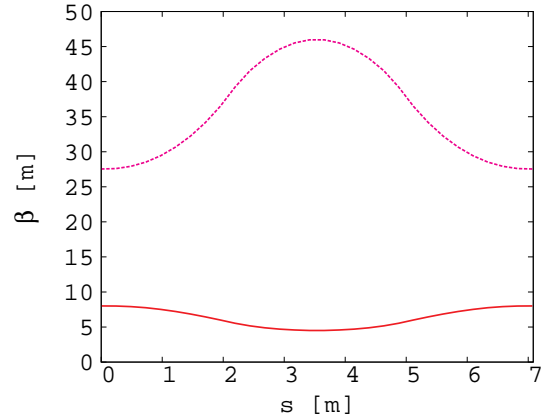


Figure 54: Horizontal (plain red) and vertical (dotted purple) periodic β functions of the circular scaling FFAG cell.

An acceptance study at fixed energy has also been done. The maximum amplitudes with stable motion at p_0 over 30 turns are shown for horizontal and vertical motion in Fig. 60 (left) and in Fig. 61 (right), respectively. The same procedure has been done for p_{min} (see Fig. 62) and p_{max} (see Fig. 64). The results are comparable. The unnormalized maximum emittance is more than 1 mm-radian.

4.5.2.4 Multi-particle tracking

Multi-particle beam tracking in 6-D phase space has been carried out for the beam with $\Delta p/p_0 = \pm 16\%$. Fig. 66 and 67 show the results of the beam tracking simulation in the horizontal and vertical directions, respectively. A normalized emittance of 14 mm-radian in the transverse direction is assumed. In these figures, the blue dots show the initial particle distribution and the red ones are after 60 turns. No beam loss is observed in 60 turns.

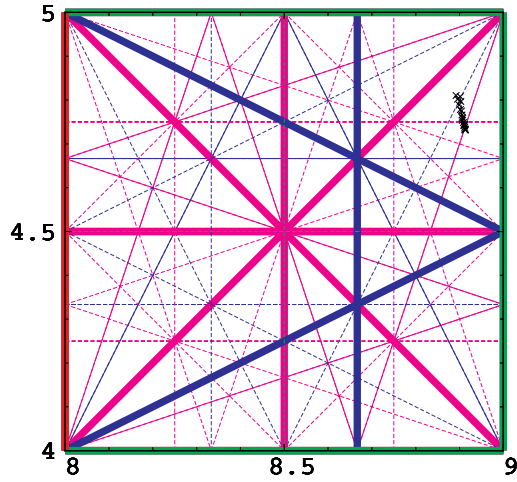


Figure 55: Tune diagram for muons from p_{min} to p_{max} ($\pm 16\%$ in momentum around 3.8 GeV/c). Integer (red), half-integer (green), third integer (blue) and fourth integer (purple) normal resonances are plotted. Structural resonances are in bold.

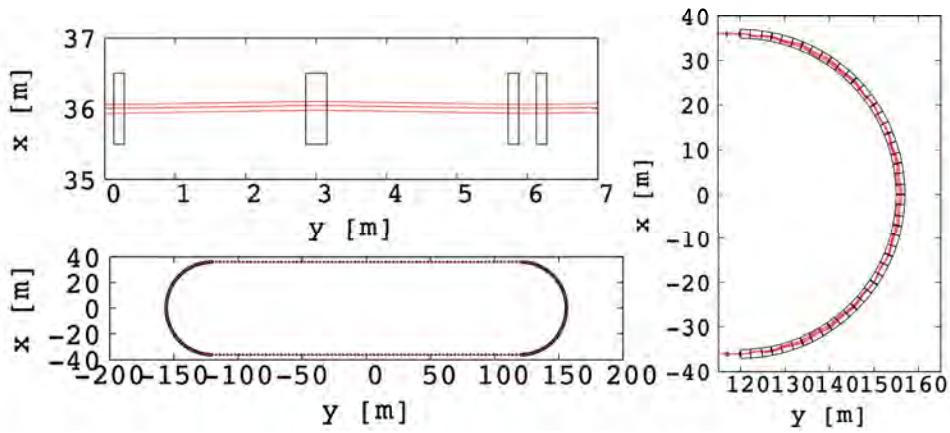


Figure 56: Top view of the racetrack FFAG lattice (bottom left scheme). The top left shows a zoom of the straight section and on the right we show a zoom of the arc section. p_0 , p_{min} , and p_{max} muon closed orbits are shown in red. Effective field boundaries with collimators are shown in black.

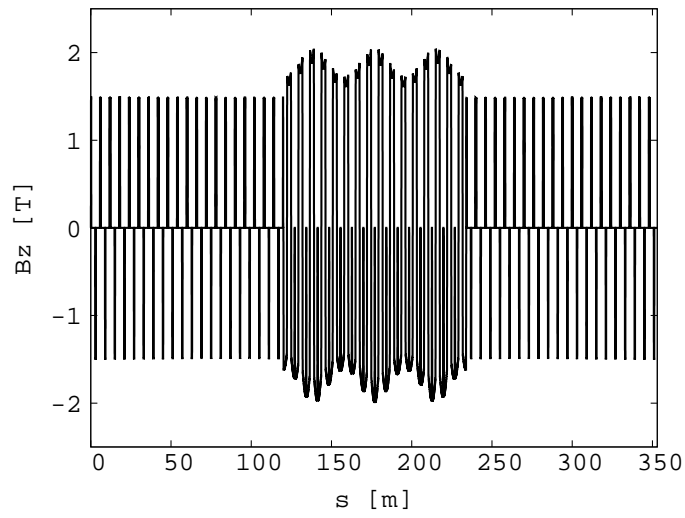


Figure 57: Vertical magnetic field for p_{max} muon closed orbit in the racetrack FFAG ring.

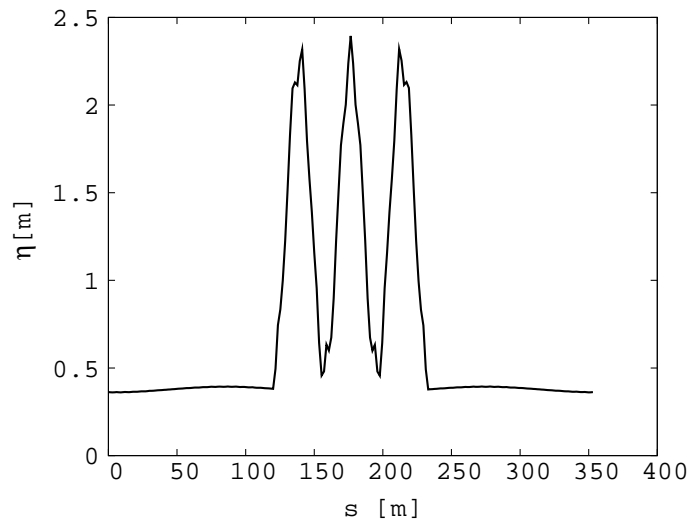


Figure 58: Dispersion function for p_0 in half of the ring. The plot is centered on the arc part.

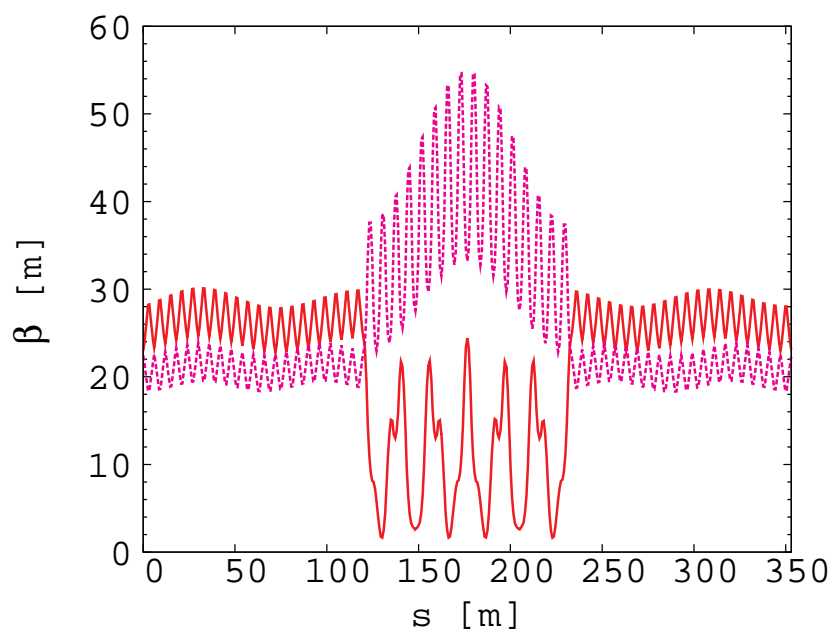


Figure 59: Horizontal (plain red) and vertical (dotted purple) periodic β functions of half of the ring for p_0 . The plot is centered on the arc part.

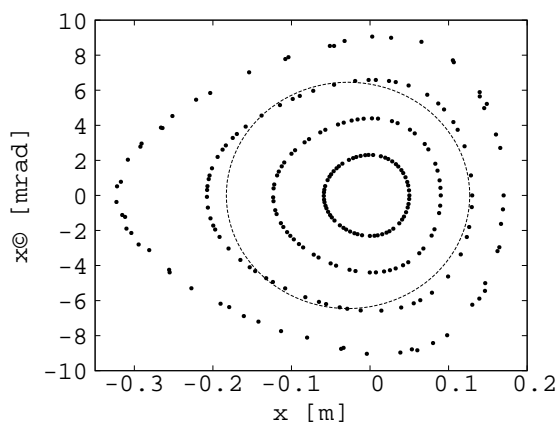


Figure 60: Stable motions in the horizontal Poincaré map for different initial amplitudes (5 cm, 9 cm, 13 cm and 17 cm) over 30 turns for p_0 . The ellipse shows a 1 mm-radian unnormalized emittance.

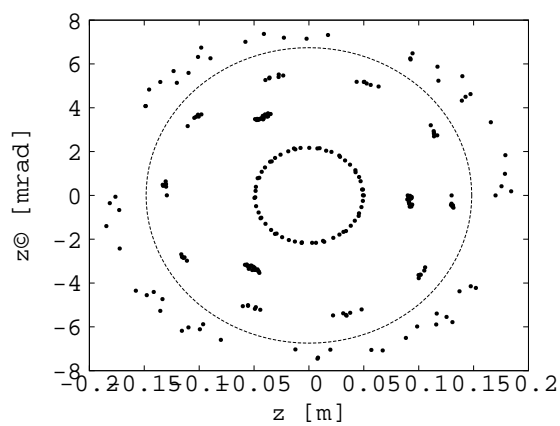


Figure 61: Stable motions in the vertical Poincaré map for different initial amplitudes (5 cm, 9 cm, 13 cm and 17 cm) over 30 turns for p_0 . The ellipse shows a 1 mm-radian unnormalized emittance.

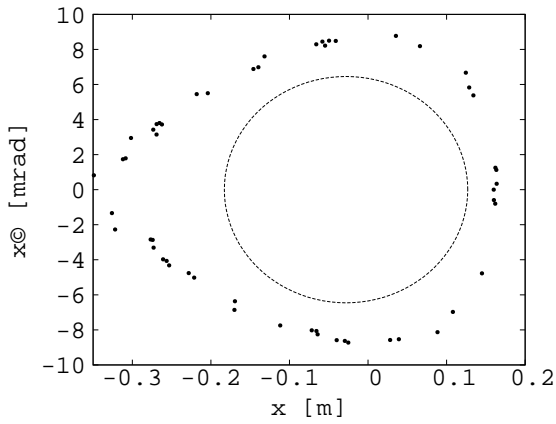


Figure 62: Horizontal Poincare map for maximum initial amplitude (16 cm) with stable motion over 30 turns for p_{min} . The ellipse shows a 1 mm-radian unnormalized emittance.

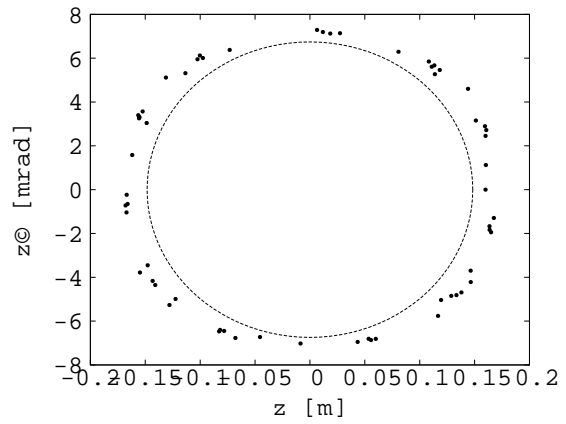


Figure 63: Vertical Poincare map for maximum initial amplitude (16 cm) with stable motion over 30 turns for p_{min} . The ellipse shows a 1 mm-radian unnormalized emittance.

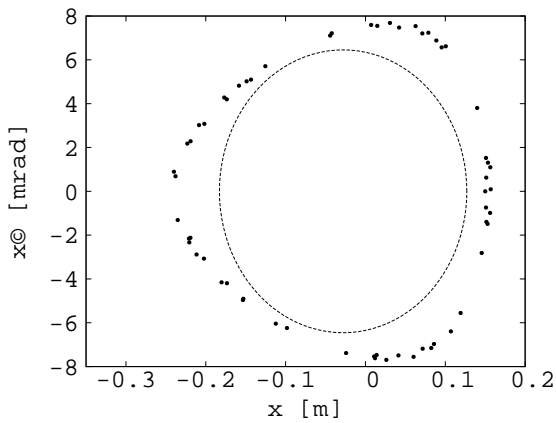


Figure 64: Horizontal Poincare map for maximum initial amplitude (15 cm) with a stable motion over 30 turns for p_{max} . The ellipse shows a 1 mm-radian unnormalized emittance.

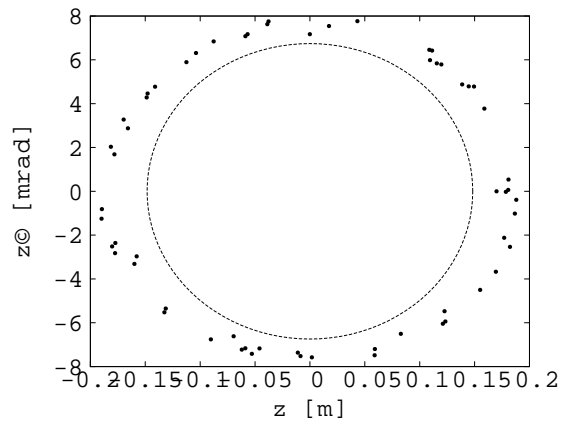


Figure 65: Vertical Poincare map for maximum initial amplitude (17 cm) with a stable motion over 30 turns for p_{max} . The ellipse shows a 1 mm-radian unnormalized emittance.

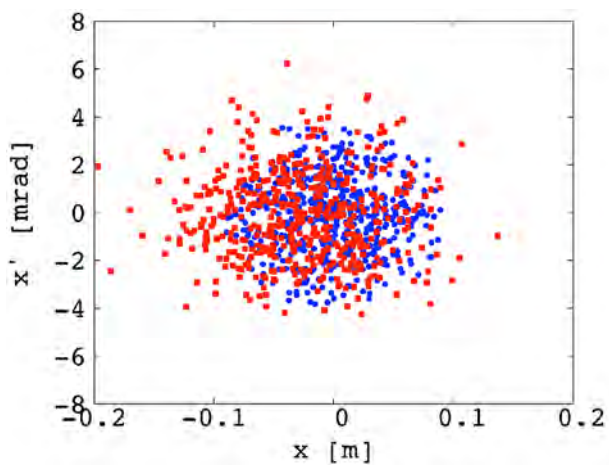


Figure 66: Beam tracking results in the horizontal phase space for a beam with $\Delta p/p_0 = \pm 16\%$. The blue shows the initial particle distribution and the red the final distribution after 60 turns.

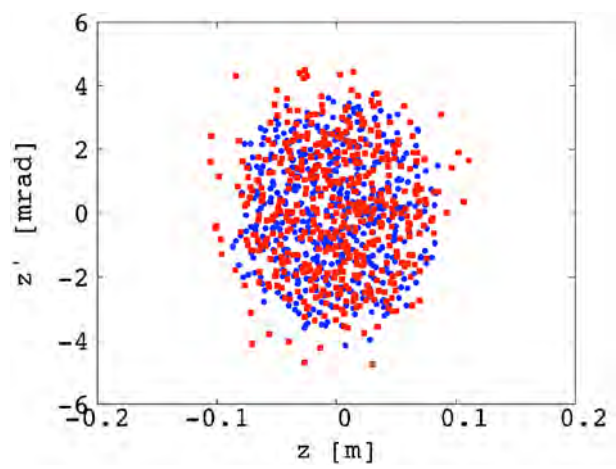


Figure 67: Beam tracking results in the vertical phase space for a beam with $\Delta p/p_0 = \pm 16\%$. The blue shows the initial particle distribution and the red the final distribution after 60 turns.

4.5.2.5 Compact arc design for the racetrack FFAG ring

In order to reduce the construction and operational cost of the racetrack FFAG decay ring, a compact arc has been designed. It assumes the use of super-ferric combined-function magnets with magnetic field strengths up to 3 T. The arc consists of four regular FDF triplet cells in the centre and two matching FDF triplet cells on each side of the regular cells, four matching cells in total for the arc. The purpose of the matching section is to match the dispersion function between the production section, assuming straight FFAG cells with small, but non-zero dispersion of 0.38 m, and the centre of the arc. It must also accommodate straight sections which allow for the stochastic injection of 5 GeV/c pions. The parameters of the regular scaling FFAG arc cell are summarized in Table 15. In the circular matching scaling FFAG cell,

Table 15: Parameters of the circular regular scaling FFAG arc cell.

Cell type	FDF triplet	
Number of cells in the ring	8	
Cell opening angle	30 deg	
r_0	16 m	
k-value	6.25	
Packing factor	0.92	
Collimators ($r_{min}, r_{max}, z_{max}$)	(15 m, 17 m, 0.4 m)	
Periodic cell dispersion	2.21 m (at 3.8 GeV/c)	
Horizontal phase advance	90 deg.	
Vertical phase advance	13.92 deg.	
F ₁ magnet parameters		
	Magnet center	5.8 deg
	Magnet length	10 deg
	Fringe field fall off	Linear (Length: 0.7 deg)
	$B_0(r_0 = 16\text{ m})$	-1.70382 T
D magnet parameters		
	Magnet center	15 deg
	Magnet length	7.6 deg
	Fringe field fall off	Linear (Length: 0.7 deg)
	$B_0(r_0 = 16\text{ m})$	2.13119 T
F ₂ magnet parameters		
	Magnet center	24.2 deg
	Magnet length	10 deg
	Fringe field fall off	Linear (Length: 0.7 deg)
	$B_0(r_0 = 16\text{ m})$	-1.70382 T

the vertical magnetic field in the median plane follows the circular scaling law, as in the circular cell. The parameters of the matching scaling FFAG cell are summarized in Table 16. The arc layout of the ring is shown in Fig. 68. The central orbit, p_0 (3.8 GeV/c) and the orbits for p_{min} (-16%) and p_{max} (+16%) are also shown in Fig. 68. The magnetic field for the p_{max} closed orbit is shown in Fig. 69. The dispersion at

Table 16: Parameters of the matching scaling FFAG cell.

Cell type	FDF triplet	
Number of cells in the ring	8	
Cell opening angle	15 deg	
r_0	36.15 m	
k-value	26.98	
Packing factor	0.58	
Collimators ($r_{min}, r_{max}, z_{max}$)	(35.3 m, 37 m, 0.4 m)	
Periodic cell dispersion	1.29 m (at 3.8 GeV/c)	
Horizontal phase advance	90 deg.	
Vertical phase advance	16.95 deg.	
F ₁ magnet parameters		
	Magnet center	4.2 deg
	Magnet length	2.8 deg
	Fringe field fall off	Linear (Length: 0.7 deg)
	$B_0(r_0 = 36.15 \text{ m})$	-2.18805 T
D magnet parameters		
	Magnet center	7.5 deg
	Magnet length	3.0 deg
	Fringe field fall off	Linear (Length: 0.7 deg)
	$B_0(r_0 = 36.15 \text{ m})$	2.74622 T
F ₂ magnet parameters		
	Magnet center	10.8 deg
	Magnet length	2.8 deg
	Fringe field fall off	Linear (Length: 0.7 deg)
	$B_0(r_0 = 36.15 \text{ m})$	-2.18805 T

p_0 is shown in Fig. 70 and the beta-functions at p_0 in Fig. 71.

Future studies on the racetrack FFAG decay ring will include a ring reconfiguration to adjust the ratio of the production straight and the arc length, detailed optimization of the working point and tracking studies. In addition, the detailed geometry of the pion injection together with the design of the super-ferric magnets must also be addressed.

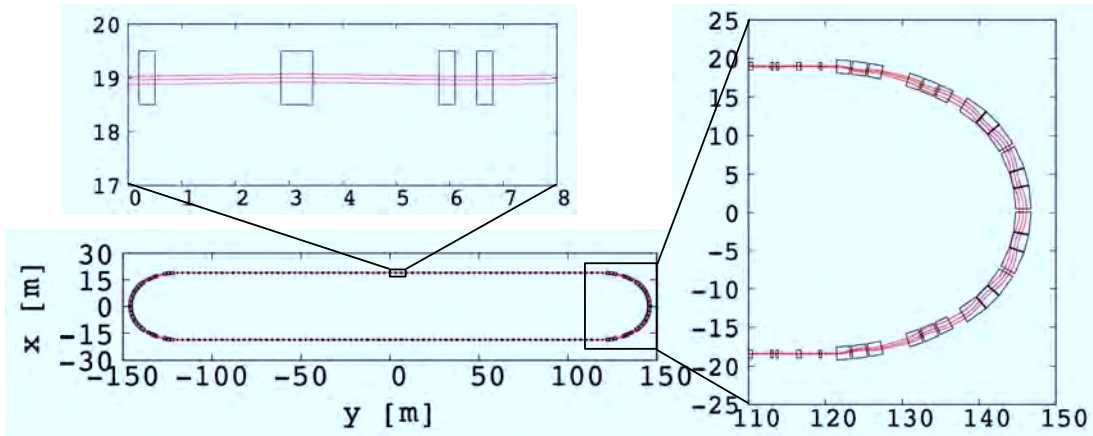


Figure 68: Top view of the racetrack FFAG lattice (bottom left figure). The top left figure shows a detail of the straight section and the right figure a detail of the arc. Muon closed orbits for p_0 , p_{min} , and p_{max} are shown in red. Effective field boundaries with collimators are shown in black.

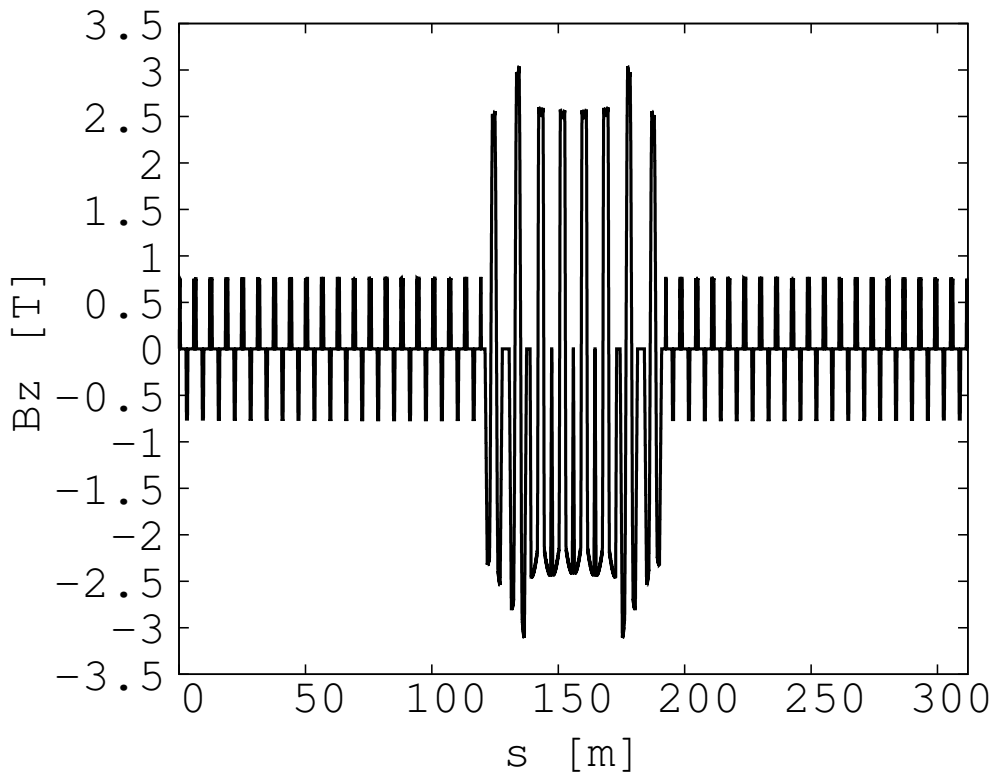


Figure 69: Vertical magnetic field for the muon closed orbit at p_{max} in the racetrack FFAG ring.

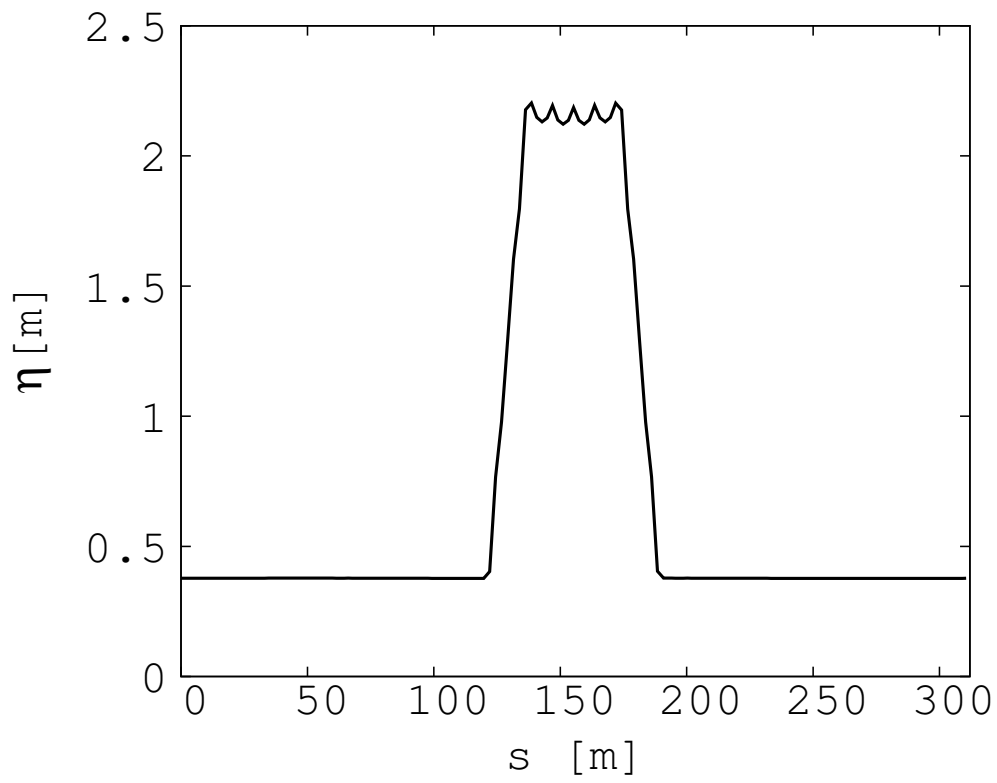


Figure 70: Dispersion function for p_0 in half of the ring. The plot is centered on the arc.

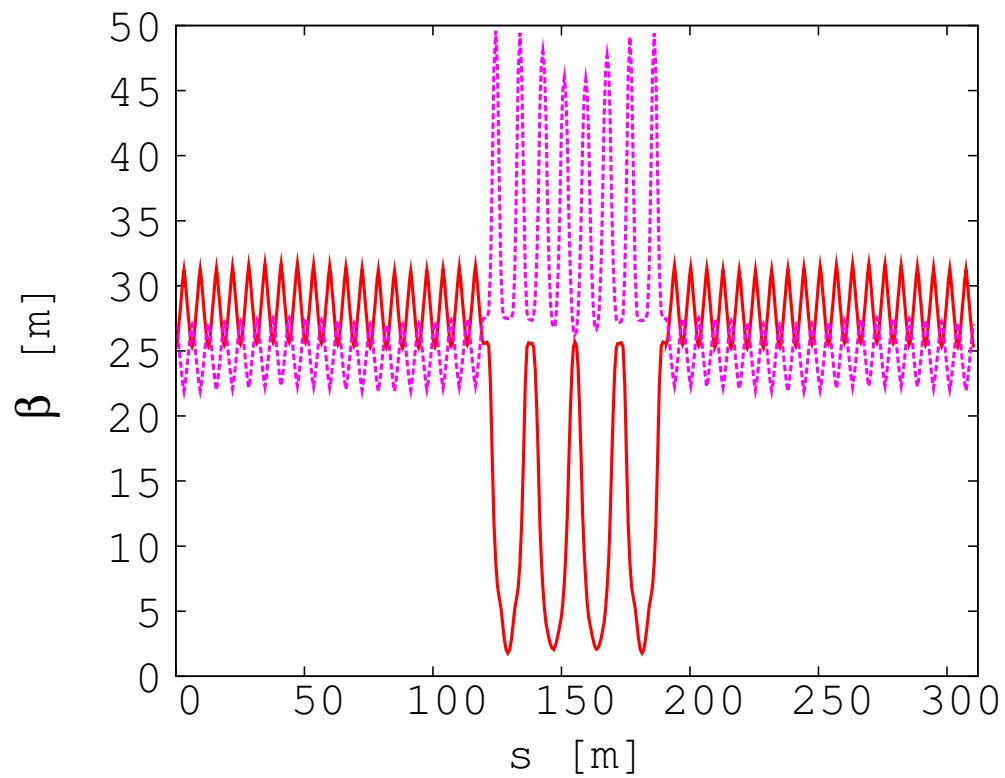


Figure 71: Horizontal (plain red) and vertical (dotted purple) periodic beta-functions of half of the ring for p_0 . The plot is centered on the arc.

4.5.3 Decay ring instrumentation

The goal of the beam instrumentation for nuSTORM is twofold. First, the instrumentation is needed in order to determine the neutrino flux at the near and far detectors with an absolute precision of $< 1\%$. Both the number of neutrinos and their energy distribution must be determined. If both the circulating muon flux in the storage ring is known on a turn-to-turn basis, and the orbit and orbit uncertainties (uncertainty on the divergence) are known accurately, then the neutrino flux and energy spectrum can be predicted with equal precision. Our measurement goals for the suite of beam instrumentation diagnostics for the decay ring are summarized below:

1. Measure the circulating muon intensity (on a turn by turn basis) to 0.1% absolute.
2. Measure the mean momentum to 0.1% absolute.
3. Measure the momentum spread to 1% (FWHM).
4. Measure the tune to 0.01.

Second, from the accelerator standpoint, in order to commission and run the storage ring, turn-by-turn measurements of the following parameters are crucial: trajectory, tune, beam profile and beam loss. Our current estimate of these requirements is summarized in Table 17 below.

Table 17: Decay ring instrumentation specifications

	Absolute accuracy	Resolution
Intensity	0.1%	0.01%
Beam position	5 mm	1 mm
Beam profile	5 mm	1 mm
Tune	0.01	0.001
Beam loss	1%	0.5%
Energy	0.5%	0.1%
Energy spread	1%	0.1%

4.5.3.1 Beam intensity

In order to measure the circulating muon intensities, one option is to use a toroid-based Fast Beam Current Transformer (FBCT), such as the one recently developed at CERN for L4 [202] and shown in Fig. 72. Its specifications are given in Table 18. It consists of a one turn calibration winding and a 20 turn secondary winding, wound on a magnetic core and housed in a 4 layer shielding box. The mechanical dimensions will have to be adapted to the large beam pipe of nuSTORM. It should be noted that obtaining an absolute precision of 0.1% will be challenging. Problems associated with the pulsed calibration and with EMI will influence the absolute accuracy of the FBCT.

4.5.3.2 Beam position

Button beam-position monitors (BPMs) are, in general, cheap and their frequency response fits very well with that of nuSTORM. They are widely used in the LHC. A photo of the 25mm diameter button is shown

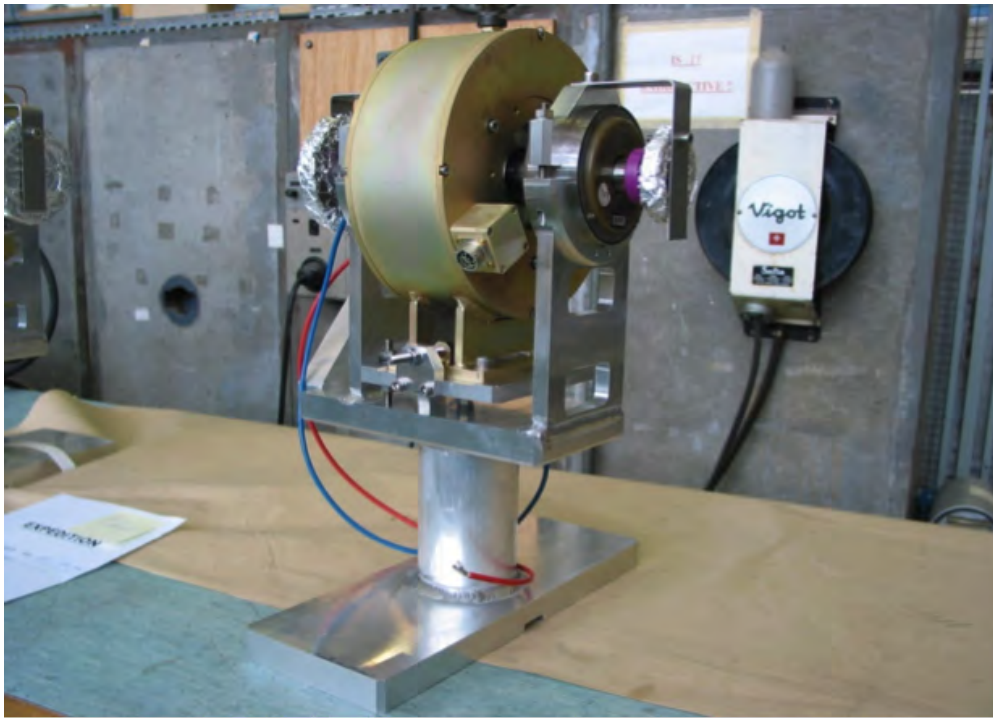


Figure 72: CERN L4 beam current transformer

Table 18: FBCT parameters

Droop @ 500 μ s	0.5%
Bandwidth	10 MHz
Accuracy	\simeq 1%
Resolution	\simeq 10 μ A
Rise time	35 ns

in Fig. 73. Due to the large vacuum chamber size and the, at present, uncertainties regarding the circulating

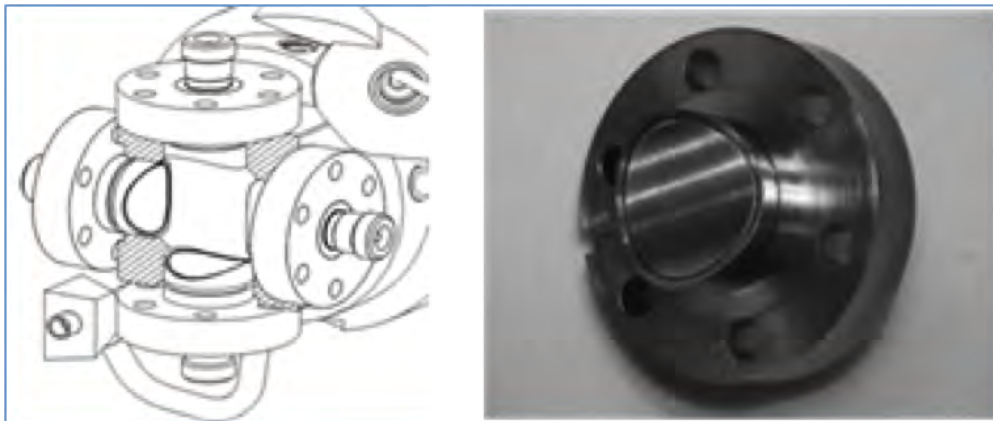


Figure 73: LHC beam-position monitor button

beam parameters, it is difficult to estimate the ultimate resolution which can be obtained. However, we can estimate the resolution assuming the following: a 100mm diameter button, bunch length of 4 ns, bunch

intensity of 5×10^8 and an input noise of $2\text{nV}/\sqrt{\text{Hz}}$. With these assumptions, the expected electrode signal can be simulated and is shown in Fig. 74. As a first order approximation the 15mV peak amplitude on the button corresponds to 50V/mm in a 600mm diameter vacuum chamber. With the assumed bandwidth and

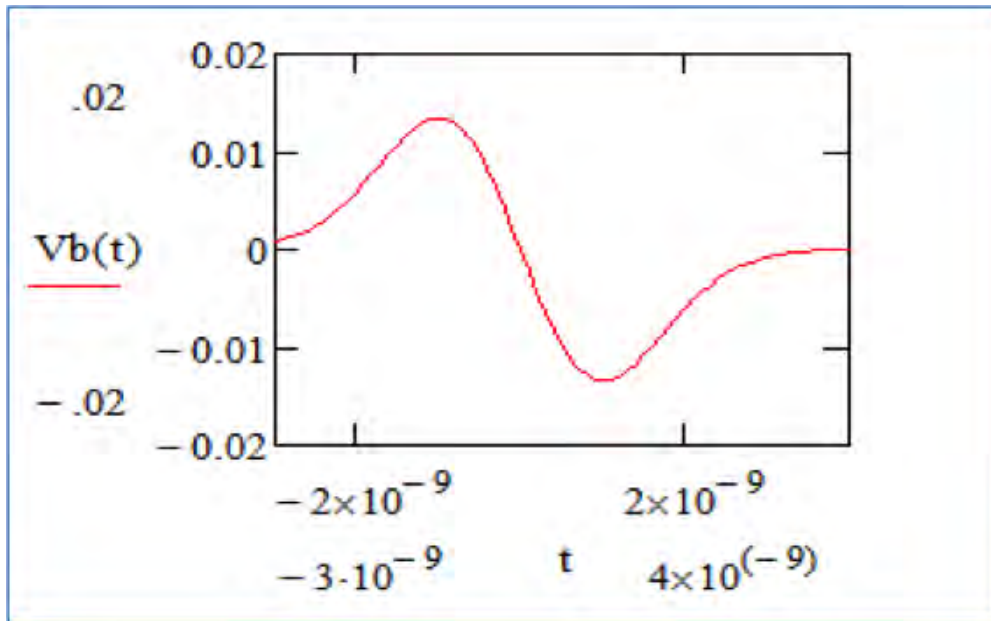


Figure 74: Button impulse response

noise of the system (output noise $\sim 30\mu\text{V}$), the expected resolution is on the order of 5 mm with a signal to noise ratio of 10. This single bunch, single turn resolution can of course be improved by averaging over all bunches, i.e., by a factor of up to 10.

4.5.3.3 Transverse profile measurements

Due to the relatively low intensities (compared to primary or secondary beamlines) and very short lifetime ($100\mu\text{s}$), our first estimations indicate that using Ionization Profile Monitors (IPM) to measure the transverse profiles is not feasible. Other detectors based on ionization (MWPC, IC, GEM) are destructive and would require a quite complicated design. (The use of low-mass MWPC is possible with further study, however.) The use of wire scanners is not possible due to the short beam lifetime.

Destructive measurement techniques using either scintillation screens or SEM-strips can be utilized. One option is to adapt the LHC dump line BTV to nuSTORM. The BTV consists of a 2 m long by 60 cm diameter vacuum tank (see Fig. 75). In this design, the fixed scintillation screen is observed with a camera, which is read out using a VME based control and data acquisition card. We estimate that this system could provide an overall position accuracy of ~ 2 mm in the nuSTORM decay ring. As designed for the LHC dump line, the system can only be used for diagnostics. It would have to be taken out of the beam during running due to the mass of the screen. However, investigating whether a low-mass screen option is possible is worth further study. The specification on the maximum tolerable material budget in the screen can be determined once we have the decay ring lattice fixed and have circulating beam in our G4Beamline simulation.

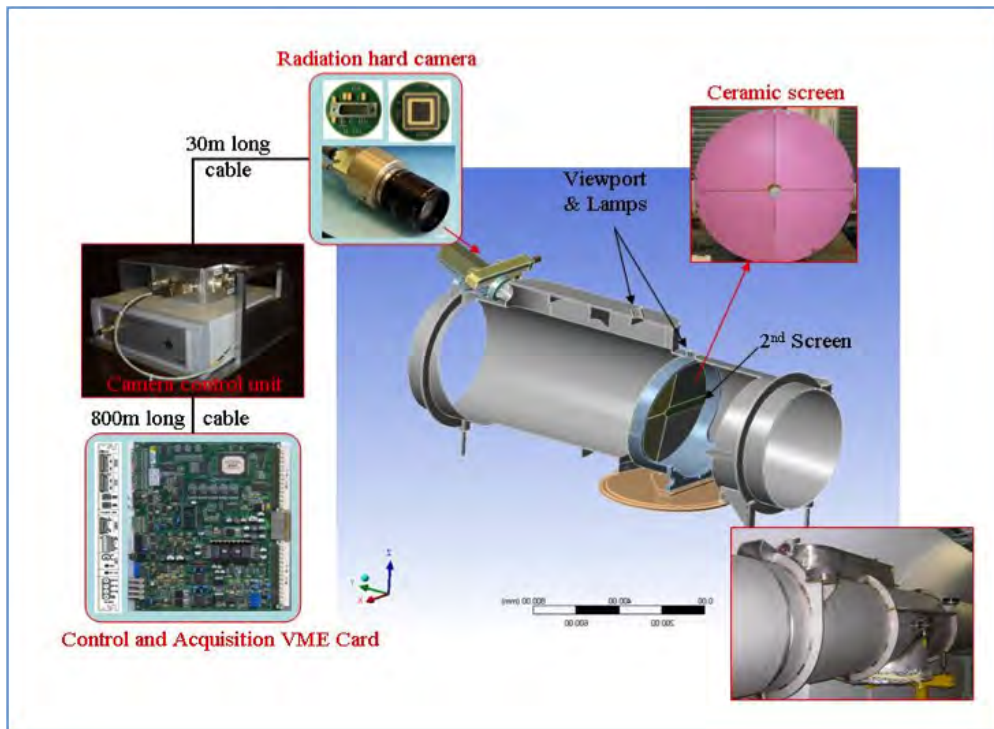


Figure 75: LHC dump line BTV

4.5.3.4 Tune measurements

For the measurement of the non-integer part of the nuSTORM tune we propose to use the Direct Diode Detection Base-Band Q (3D-BBQ) developed at CERN by M. Gasior [203] and shown schematically in Fig. 76. This very sensitive method allows for the observation of very small amplitude modulations on high level signals. The pulses obtained from any of the beam position monitors are connected to simple diode detectors which convert the amplitude modulation of the BPM pulses to a signal in the audio frequency range. The dominate part of the BPM signal is related to the beam intensity, and becomes a DC voltage. This DC component is easily removed using a simple capacitor at the detector output. The two base band signals are then subtracted in a difference amplifier and digitized for tune calculations in the frequency domain.

Due to our uncertainty on the bunch intensities at this time, it is, at present, difficult to estimate if a tune kicker is needed to enhance the betatron amplitudes to obtain the required tune and time resolution. At first estimate, we believe that connecting one or several BPMs to the system should be sufficient.

4.5.3.5 Beam loss measurements

Beam loss monitors would be used mostly for diagnosing the performance of the ring with emphasis on the injection point using some monitors in the straight sections and in the arcs. We propose to use “slow” ionisation chambers (Fig. 77) for integration of the total loss around the ring and diamond-based fast secondary emission monitors (Fig. 78) for observation of the “fast” injection losses. Both types of detectors are sensitive to charged particles only.

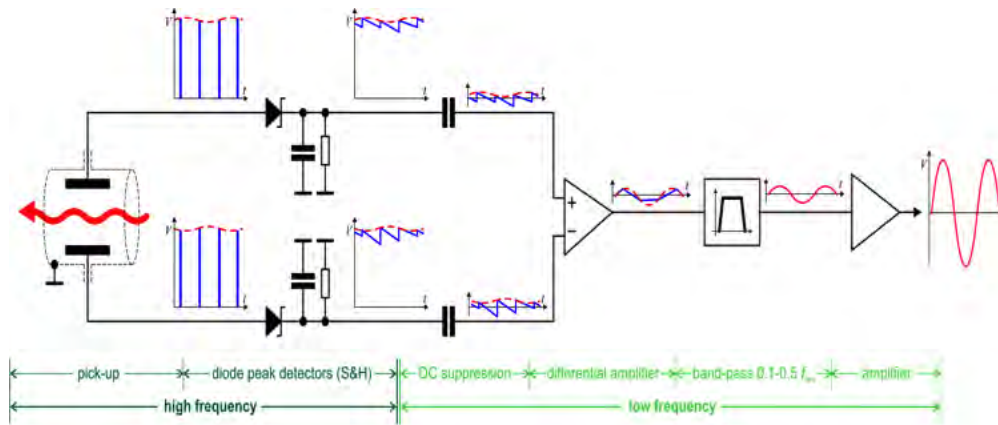


Figure 76: Base-band tune measurement principle

The ionization chamber consists of a 60 cm long stainless steel cylinder, with parallel Al electrodes separated by 0.5 cm to which a voltage of 1.5 kV is applied to every second electrode. The entire volume is filled with Nitrogen gas. The output current from the grounded electrodes is then proportional to the beam loss. The diamond detector consists of a 10 mm × 10 mm × 0.5 mm polycrystalline chemical vapor

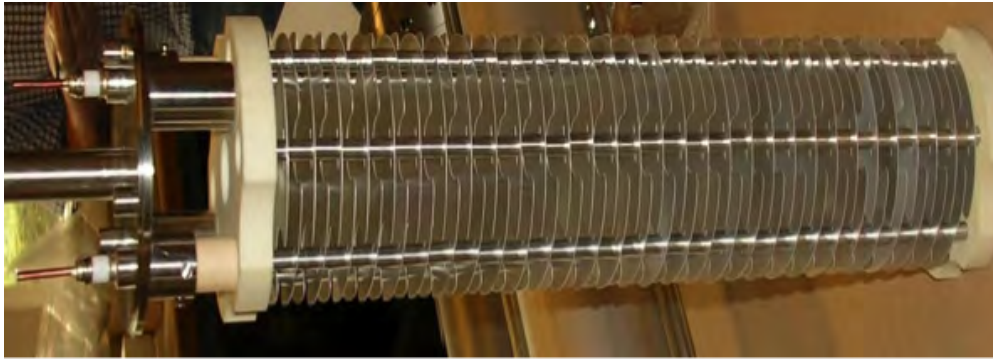


Figure 77: Photograph of an ionization chamber for total beam loss (slow) measurements

deposition (pCVD) diamond substrate coated on each side with 200 nm thick gold electrodes. A biasing voltage of ~ 500 V is used. A 40 dB broadband radiation hard current amplifier with a bandwidth 100 MHz to 2 GHz is needed to amplify the very low currents.

4.5.3.6 Summary

In the above sections, we have shown how existing beam instrumentation or extrapolations from existing designs can meet the needs of nuSTORM and gives the basis for making realistic cost estimates for the instrumentation. However, obtaining full knowledge regarding how well the instrumentation will perform in the nuSTORM decay ring will only come after the lattice design is finalized (addition of higher-order correctors). Once this has been accomplished, we then have the tools in place within the G4Beamline simulation framework to understand, in detail, how this instrumentation will perform.



Figure 78: Diamond-based secondary emission monitor

4.6 A future 6D muon ionization cooling experiment

Fig. 79 shows a schematic of the decay ring. As is described in section 4.4, 5 GeV/c pions are injected at the beginning of the straight section of the ring. With the 185 m length for the straight, $\sim 48\%$ of the pions decay in the injection straight. Since the arcs are set for the central muon momentum of 3.8 GeV/c, the pions remaining at the end of the straight will not be transported by the arc. The power contained within the pion beam that reaches the end of the injection straight is 2 kW–3 kW making it necessary to guide the undecayed pion beam into an appropriate absorber.

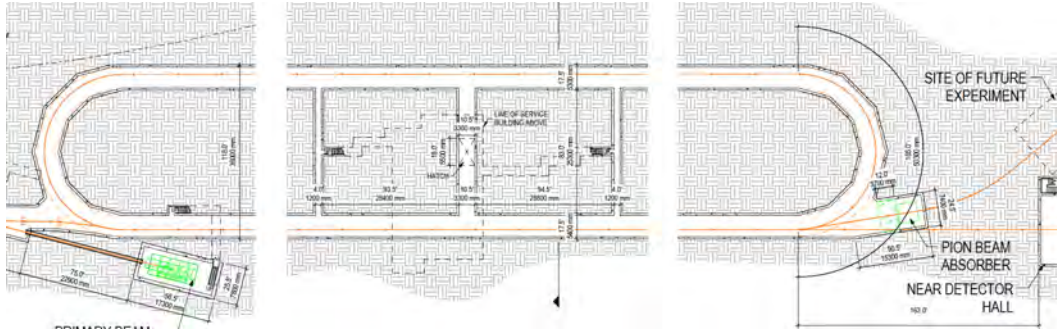


Figure 79: Schematic of the nuSTORM decay ring.

As discussed earlier, another BCS, which is just a mirror reflection of the injection BCS, is placed at the end of the decay straight. It extracts the residual pions and muons which are in the 5 ± 0.5 GeV/c momentum range. These extracted muons will enter the absorber along with pions in this same momentum band.

However, if the absorber is “redefined” to be a “degrader” capable of stopping the pions but allowing muons above a certain energy to pass, then a low-energy muon beam appropriate for a 6D muon cooling experiment can be produced. The left panel of Fig. 80 shows the momentum distribution for the first pass of muons at the end of the decay-ring straight. The green band indicates the momentum acceptance of the decay ring. The red band covers the same momentum band as the input pions and these muons will be extracted along with the remaining pions. If the degrader is sized appropriately, a muon beam of the desired momentum for a 6D cooling experiment will emerge downstream of the degrader. The right panel of Fig. 80 shows a visualization of a G4Beamline [198] simulation of the muons in the pion momentum band ($5 \pm 10\%$ GeV/c) propagating through a 3.48 m thick iron degrader. The left panel of Fig. 81 shows the $x - y$ distribution of the muon beam exiting the degrader while the right panel shows the $x - x'$ distribution. Figure 82 shows the muon momentum distribution of the muons that exit the degrader. Our initial estimate is that, in the momentum band of interest for a six-dimensional (6D) cooling experiment (100–300 MeV/c), we will have approximately 10^{10} muons in the $1.6 \mu\text{sec}$ spill.

Advanced R&D on the high intensity 6D ionization cooling channel required for a Muon Collider could be pursued using the nuSTORM facility and this muon beam. The two key 6D cooling channels currently under detailed study can be tested at the nuSTORM facility without affecting the main neutrino activities: the Guggenheim and the Helical Cooling Channel (layouts in Fig. 83–84). After selection of one of these cooling schemes and a successful bench test, the hardware for the section of the cooling channel long enough to demonstrate 6D cooling could be set up at the nuSTORM facility in order to run a test demonstration experiment with the intense muon beam. Preliminary studies with one and two cells of both the initial

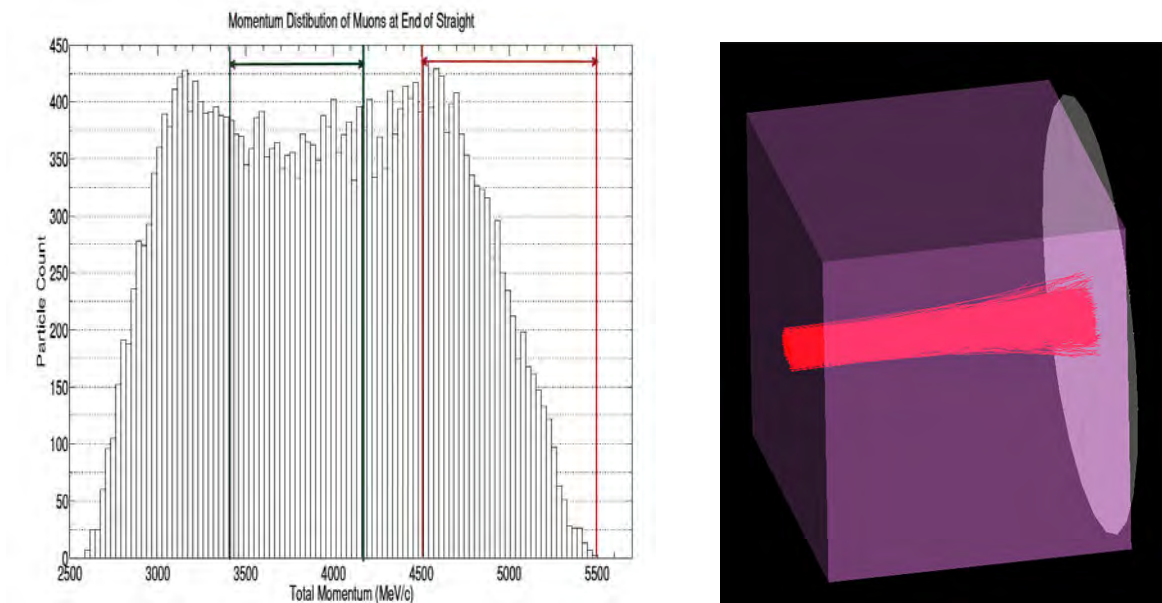


Figure 80: Left panel: Momentum distribution of muons after the first straight. Right panel: Visualization of muons in the degrader.

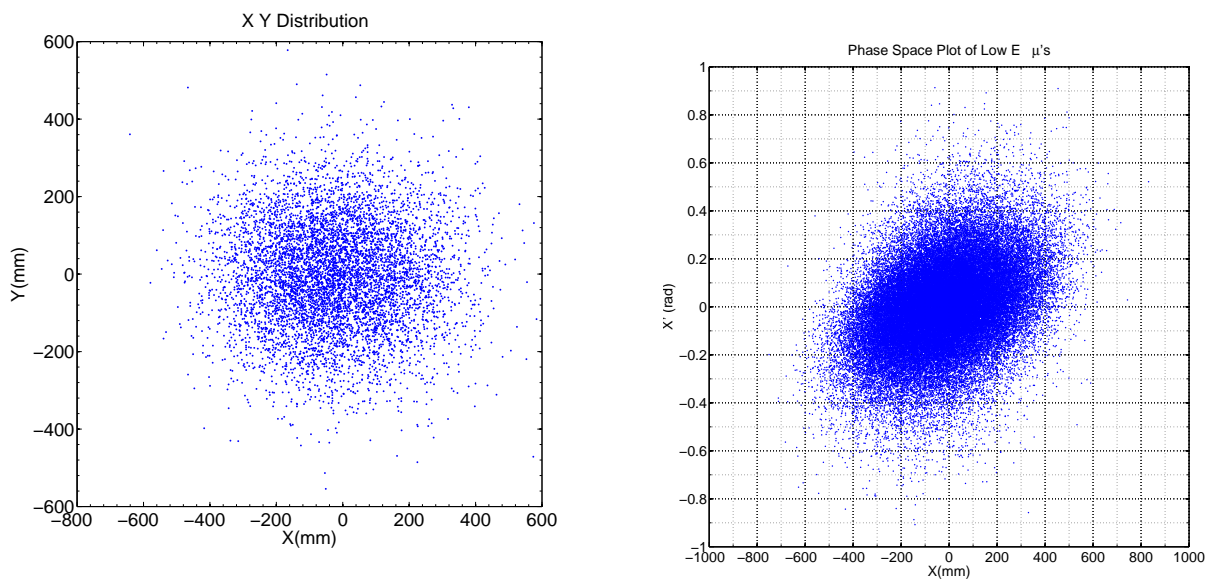


Figure 81: Phase-space of the muon beam as it leaves the degrader. Left panel: $x - y$ distribution; Right panel: $x - x'$ distribution.

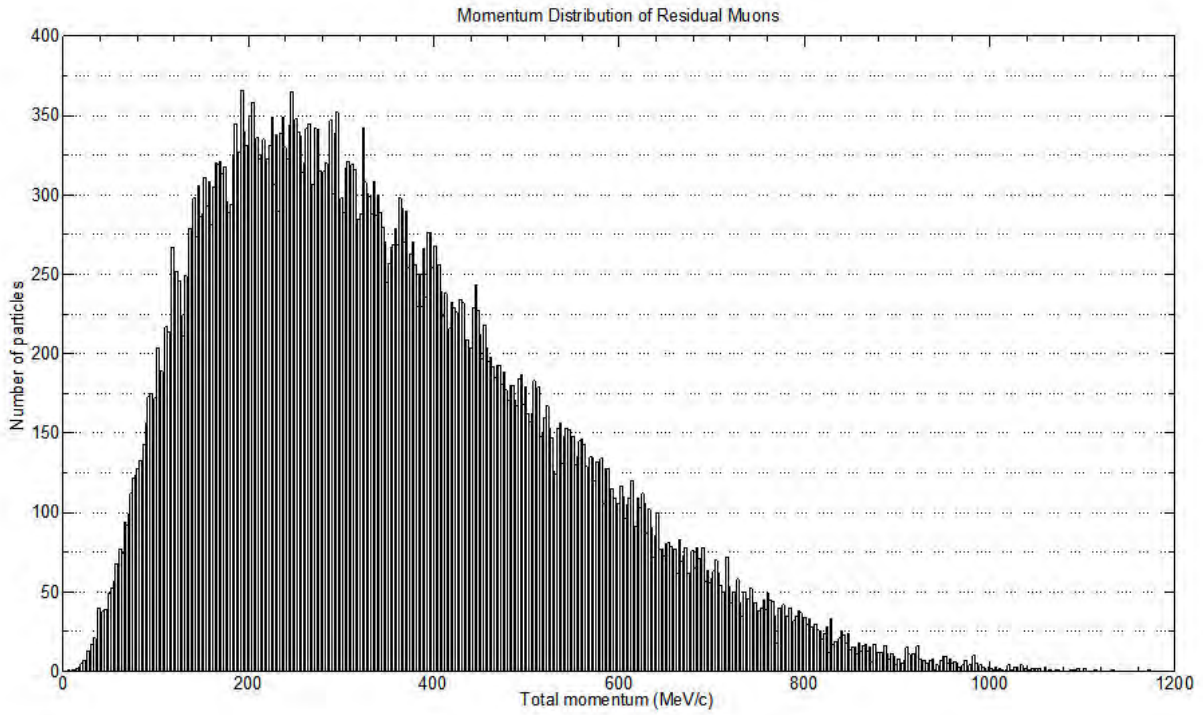


Figure 82: Muon momentum distribution after degrader.

Table 19: Percentage of muons surviving one and two cells of the 201 MHz and 805 MHz Guggenheim channel, and its dependence on the degrader length.

Degrader [mm]	201 MHz, one cell	201 MHz, two cells	805 MHz, one cell	805 MHz, two cells
3500	24%	8.6%	4.7%	0.6%
3480	24%	8.5%	4.9%	0.6%
3460	24%	8.4%	5.1%	0.6%

(with 201 MHz RF) and the final (with 805 MHz RF) stages of the Guggenheim cooling channel suggest promising muon transmission rates. These are summarized in Table 19. The corresponding momentum distribution and phase portraits are shown in Fig. 85.

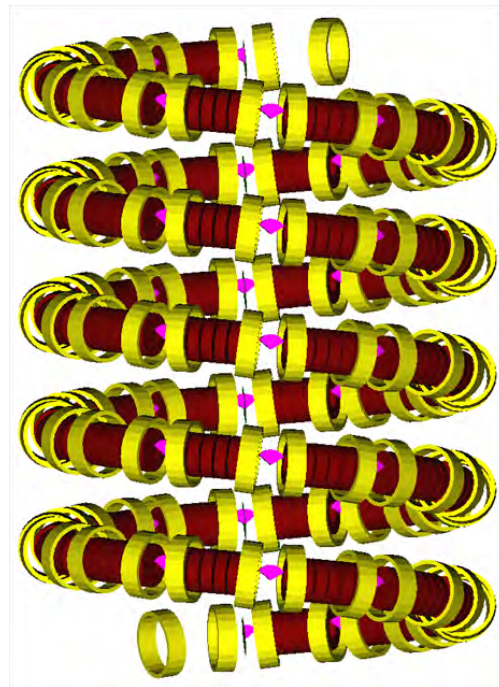
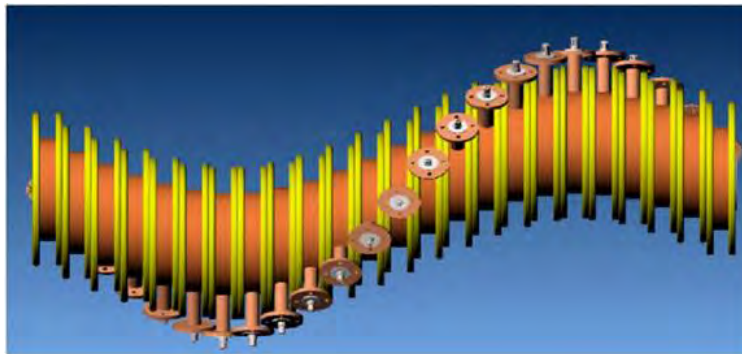
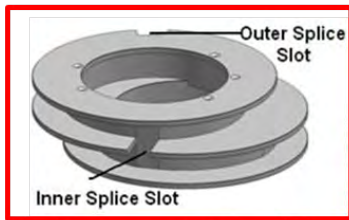


Figure 83: Layout of the initial stages of the Guggenheim cooling channel. Yellow: magnetic coils to generate focusing and bending field required for emittance exchange; magenta: liquid Hydrogen wedge absorbers to reduce momentum; red: RF cavities to restore momentum lost in the absorbers.



M. Yu et al., FNAL TD-11-001

Dummy RF cavity



Gas-filled RF test cell
to study plasma loading
(K. Tanehara et al. IPAC'12)

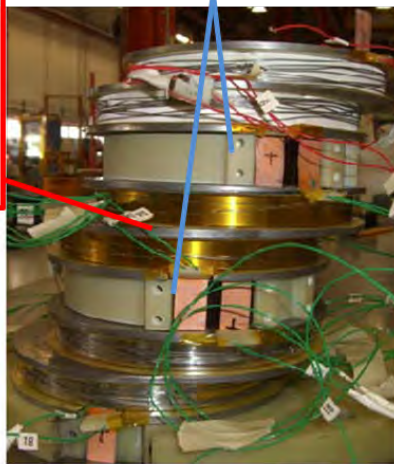


Figure 84: Top: conceptual drawing of the Helical Cooling Channel; bottom: test coil assembly producing helical solenoid field.

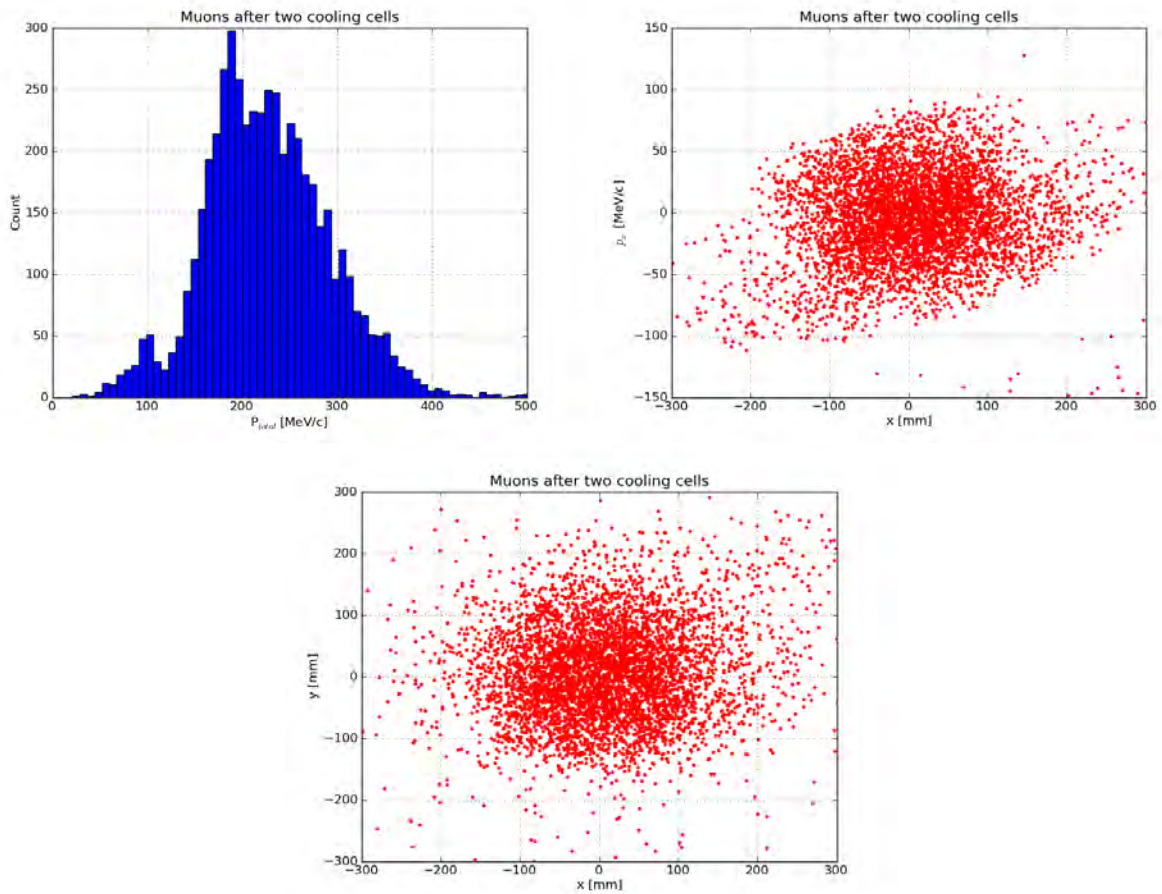


Figure 85: Top-left: muon momentum distribution after passing through two cells of the initial 201 MHz Guggenheim cooling channel; Top-right: $(x - p_x)$ phase portrait of the distribution; bottom: $(x - y)$ phase portrait of the distribution.

5 nuSTORM Conventional Facilities

The nuSTORM Conventional Facilities are anticipated to consist of six (6) functional areas consisting of the Primary Beamline, Target Station, Transport Line/Muon Decay Ring, Near Detector Hall, Far Detector Hall and the Site Work.

The facilities will be located in an area south of the existing Main Injector accelerator and west of Kautz Road on the Fermilab site. In general terms, a proton beam will be extracted from the existing Main Injector at the MI-40 absorber, directed east towards a new below grade target station, pion transport line and muon decay ring. The neutrino beam will be directed towards a Near Detector Hall located 20 m East of the muon decay ring and towards the Far Detector located approximately 1900 m away in the existing D0 Assembly Building (DAB). Fig. 86, below, shows a site photo with the nuSTORM Conventional Facilities superimposed. We have also considered an East site for nuSTORM which would put all of the facility East



Figure 86: Fermilab site view looking North and showing the nuSTORM facilities.

of Kautz Road. This eliminated any potential interference with existing infrastructure near the main site, in the event there would be significant future expansions to the nuSTORM facility (see Fig. 87), but requires a long (≈ 510 m) primary proton beam line from the Main Injector. The current West site does not impact existing infrastructure, while still allowing for future expansion. Full details of the nuSTORM Conventional Facilities are given in the nuSTORM project definition report [204]. DAB provides an ideal space for location of the far detector(s) for the short-baseline oscillation program. With relatively minor retro-fitting, the DAB pit area can accommodate a 1.3 kT Fe-scintillator detector (SuperBIND, see Section 6) while providing enough space for a future kT-scale magnetized LAr detector. Fig. 88 shows a 3D view of the setup in DAB indicating the positions of SuperBIND (left) and a conceptualized LAr detector set next to the D0 experimental hall. The height of the area allows approximately 6' of heavy concrete overburden below the crane (indicated in the figure above the SuperBIND detector).



Figure 87: Fermilab site view looking North and showing the nuSTORM facilities at the East site.

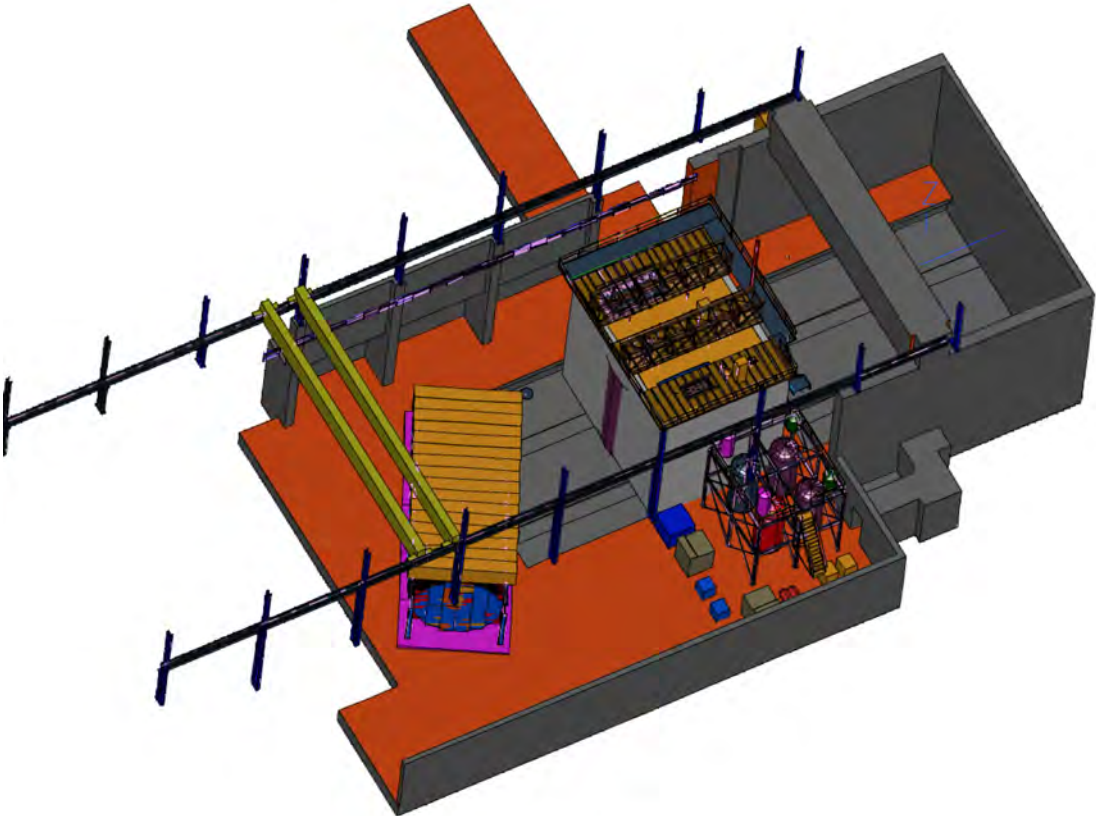


Figure 88: Schematic of far detector hall (DAB) showing SuperBIND and demonstrating that there is room to add another detector (a conceptualized kT-scale magnetized LAr detector is shown) at some future date.

6 Far Detector - SuperBIND

The Super B Iron Neutrino Detector (SuperBIND) is an iron and scintillator sampling calorimeter which is similar in concept to the MINOS detectors [205]. We have chosen a cross section of 6 m in order to maximize the ratio of the fiducial mass to total mass. The magnetic field will be toroidal as in MINOS and SuperBIND will also use extruded scintillator for the readout planes. Details on the iron plates, magnetization, scintillator, photodetector and electronics are given below. Fig. 89 gives an overall schematic of the detector. We note that within the Advanced European Infrastructures for Detectors at Accelerators (AIDA)

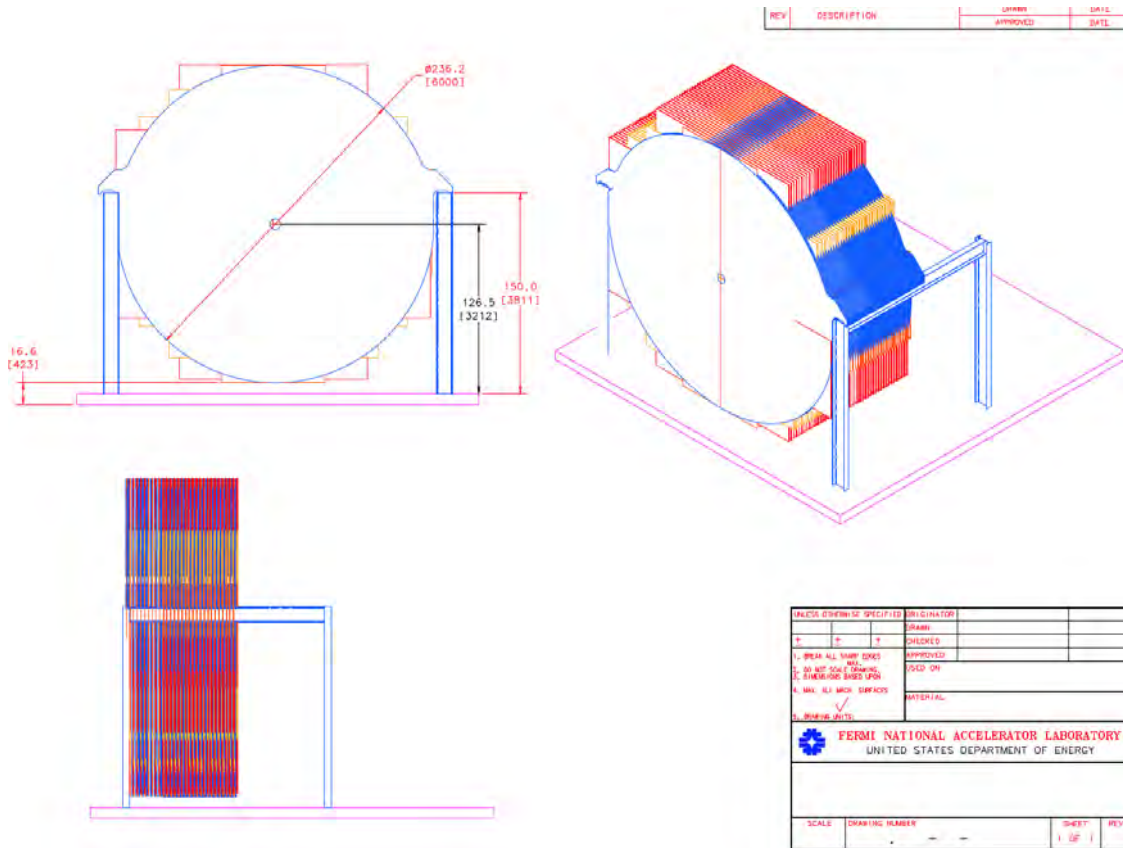


Figure 89: Far Detector concept

project [206], whose time line runs from 2011 to 2015, detectors similar to those planned for nuSTORM will be built and characterized at CERN. The motivation is to test the capabilities for charge identification of $\leq 5\text{GeV}/c$ electrons in a Totally Active Scintillator Detector and $\leq 5\text{ GeV}/c$ muons in a Magnetized Iron Neutrino Detector (MIND). These detector prototypes will provide further experience in the use of STL technology, and SiPMs and associated electronics, to complement the already large body of knowledge gained through past and current operation of this type of detector.

6.1 Iron Plates

For the Iron plates in SuperBIND, we are pursuing the following design strategy. The plates are round with an overall diameter of 6 m and a thickness of 1.5 cm. Our original engineering design used 1 cm plates,

but we have simulated the detector performance for 1 cm, 1.5 cm and 2 cm thick plates. The baseline is now 1.5 cm. They are fabricated from two semicircles that are skip welded together. We currently plan to hang the plates on ears as was done for MINOS, but there is an option to stack the plates in a cradle using a strong-back when starting the stacking. We envision that no R&D on the iron plates will be needed. Final specification of the plate structure would be determined once a plate fabricator is chosen.

6.2 Magnetization

As was mentioned above, MIND will have a toroidal magnetic field like that of MINOS. For excitation, however, we plan to use the concept of the Superconducting Transmission Line (STL) developed for the Design Study for a Staged Very Large Hadron Collider [207] with possible extensions based on recent superconductor, cable-in-conduit development that has been carried out for ITER (see Section ??). Minimization of the muon charge mis-identification rate requires the highest field possible in the iron plates. SuperBIND requires a much large excitation current per turn than that of the MINOS near detector (40 kA-turns). We have simulated 240kA-turns. The magnetization implementation plan is described in Section 6.2.2.

6.2.1 Magnetic Field Map

Utilizing the SuperBIND plate geometry shown in Fig. 89, a 2-d finite element magnetic field analysis for the plate was performed. Fig. 90 shows the results of those calculations. For this analysis, a 20 cm diameter hole for the STL was assumed, the CMS steel [208] BH curve was used and an excitation current of 240 kA-turn was assumed.

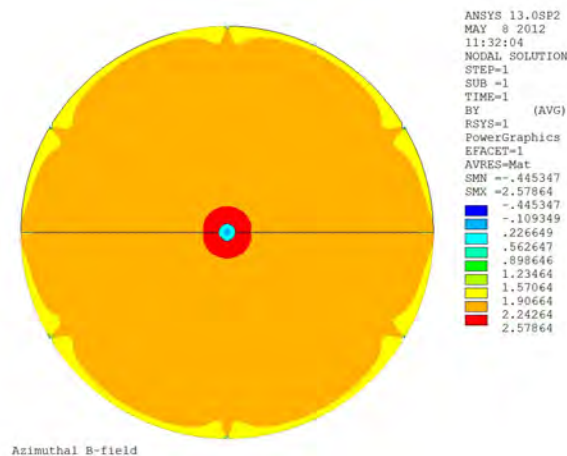


Figure 90: Toroidal Field Map

6.2.2 SCTL implementation design

The superconducting magnet system for SuperBIND is based on NbTi superconductor cooled by the forced-flow LHe. Because of the dimensions of the detector (6 m diameter and 16 m length), it is reasonable to use

Table 20: Magnet parameters for SuperBIND.

Name	Unit	Value
Iron core outer diameter	6.0	m
Iron core inner diameter	0.2	m
Iron core length	15.82	m
Iron plate thickness	15	mm
Number of plates	440	
Space between plates	21	mm
Number of superconducting racetrack coils	8	
Superconducting cable length	320	m
Racetrack coil current	30	kA
Total current	240	kA-turns
Peak field on the coil	0.83	T
Inductance	40	mH
Total stored energy	18	MJ

the superconducting transmission line approach proposed by the Hon. G. W. Foster and successfully tested for the VLHC [207, 209]. This transmission line was capable of carrying up to 100 kA and was used to generate the 2 T field in the double aperture dipole magnet [210] of the VLHC. Because the line was very compact (80 mm OD), this approach is very cost effective in that it eliminates a large and expensive cryostat. The SuperBIND magnet is specified to be excited by 240 kA-turns. We have chosen a 30 kA current level for the transmission line superconductor in order to provide a more homogeneous field distribution in the iron core and to reduce the current and Lorentz forces on the superconductor. The total number of transmission line turns in this case is eight. The superconducting magnet system has parameters shown in Table 20. The magnet was modeled by the TOSCA OPERA3d code. The model geometry is shown in Fig. 91. Because

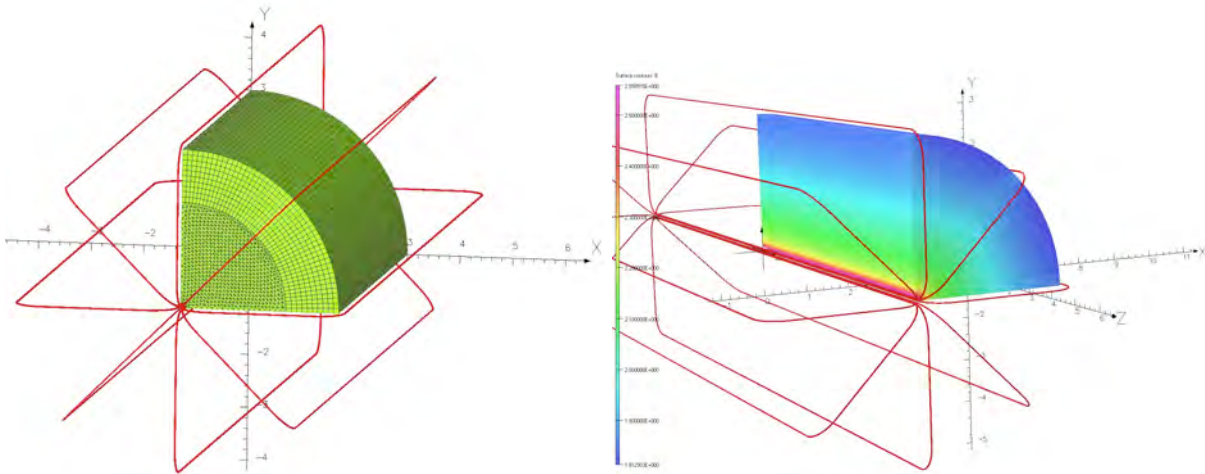


Figure 91: Magnetic field calculation geometry (left), and flux density in the iron (right).

the iron plates are spaced by approximately 21 mm, the iron properties in the z direction were modeled as anisotropic, with a packing factor of 0.417. The effective flux density distribution is shown in Fig. 92. The

superconducting transmission line for the VLHC is shown in Fig. 93. For the proposed toroidal magnet

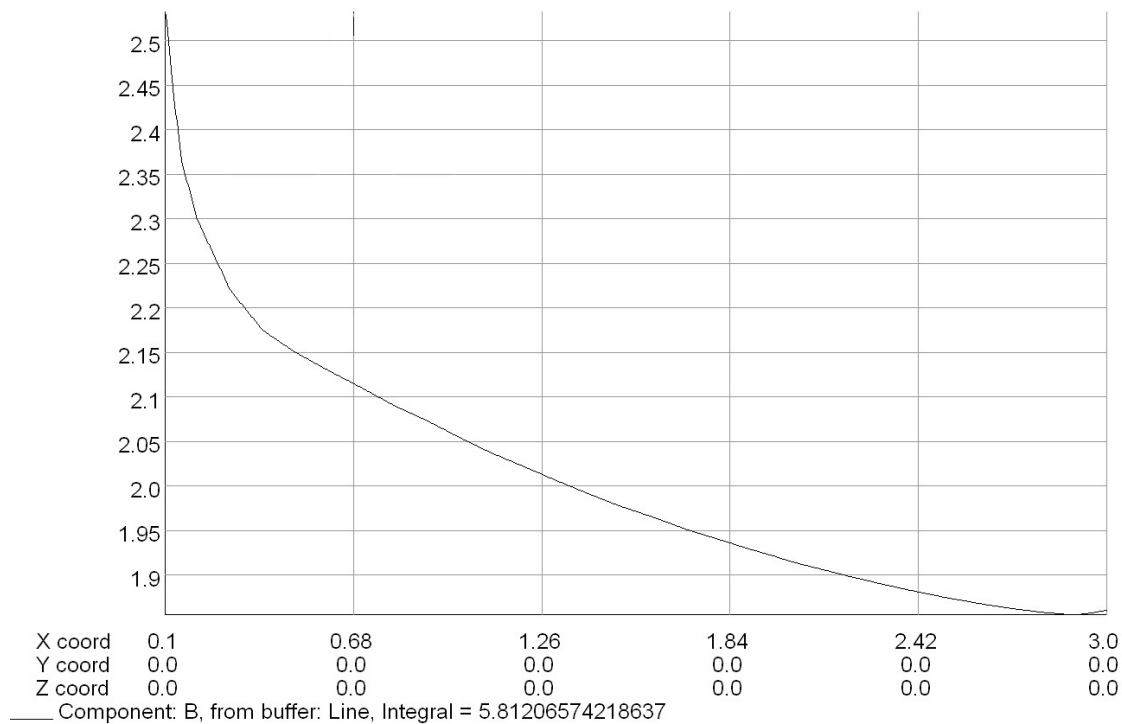


Figure 92: Flux density distribution in the radial direction in the iron.

system configuration, the most critical parameters are the maximum field and the Lorentz forces on the superconducting coils. The peak effective magnetic field in the iron is 2.5 T which drops to 1.85 T at a radius of 3 m. The peak field on the superconductor is 0.83 T on the coil inner radius. The radial Lorentz force component on the inner conductor is -271 kN (-1700 kg/m), and on the outer, 40 kN (250 kg/m). The longitudinal force component for the radial conductors is 2.4 kN (80 kg/m). These force loads (except the force on the inner conductor) are in the range of the capability of the VLHC transmission line design where the most critical elements are the Ultem rings (spiders) supporting the cold cable mass inside the vacuum shell (See Fig. 93). The inner part of coil will see large radial forces directed to the center. This is why a stainless steel slotted tube is needed in the center (See Fig. 94). The inner coil assembly cold mass has a 120 mm diameter and is cooled by forced-flow LHe through a central hole of 40 mm diameter. The cold mass is supported by Ultem rings in the same way as shown in Fig.93. Eight straight NbTi bars are mounted inside the slotted central tube with the outer aluminum tube. The whole cold-mass assembly is impregnated with an epoxy resin. Coil bars are electrically insulated from the supporting tube and an outer aluminum shell. During cool down, the Al shell provides a pre-stress for the coil, which increases the superconducting coil mechanical stability. The cold mass is mounted inside a stainless steel vacuum vessel of 200 mm diameter and includes a nitrogen shield. Super-insulation is wrapped around the cold mass and the nitrogen shield.

The most complicated part of the design is the transition area between the inner part of the coil and eight transmission lines surrounding the iron core (detector), which are electrically connected in series. The final superconductor splices will have to be made after the assembly forming the eight turns is in place. The outer transmission line vacuum vessels should be rigidly attached to the detector iron with a high angular accuracy to eliminate transverse forces. An option that could be applied, in order to reduce the force on the

TRANSMISSION LINE MAGNET

100 kA Drive Conductor

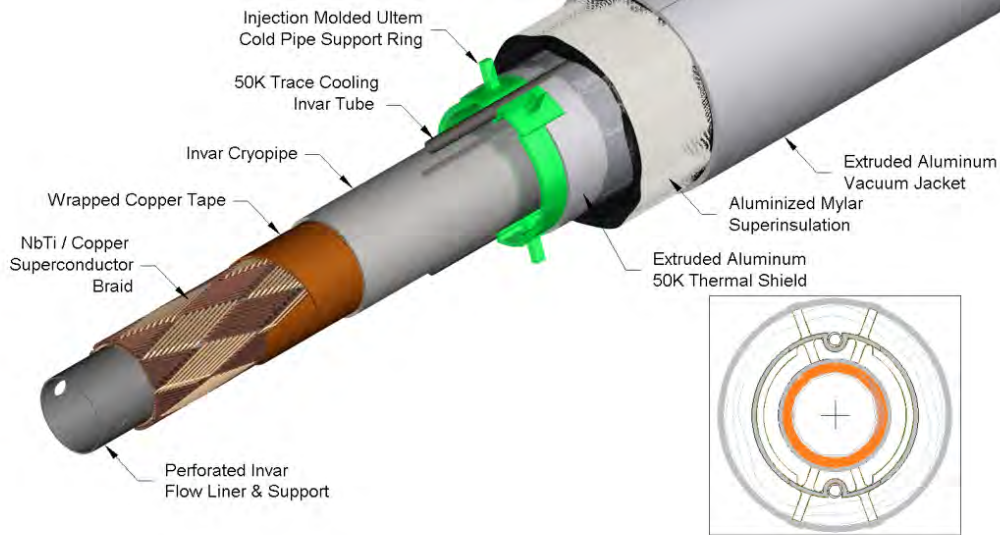


Figure 93: Superconducting transmission line for the VLHC.

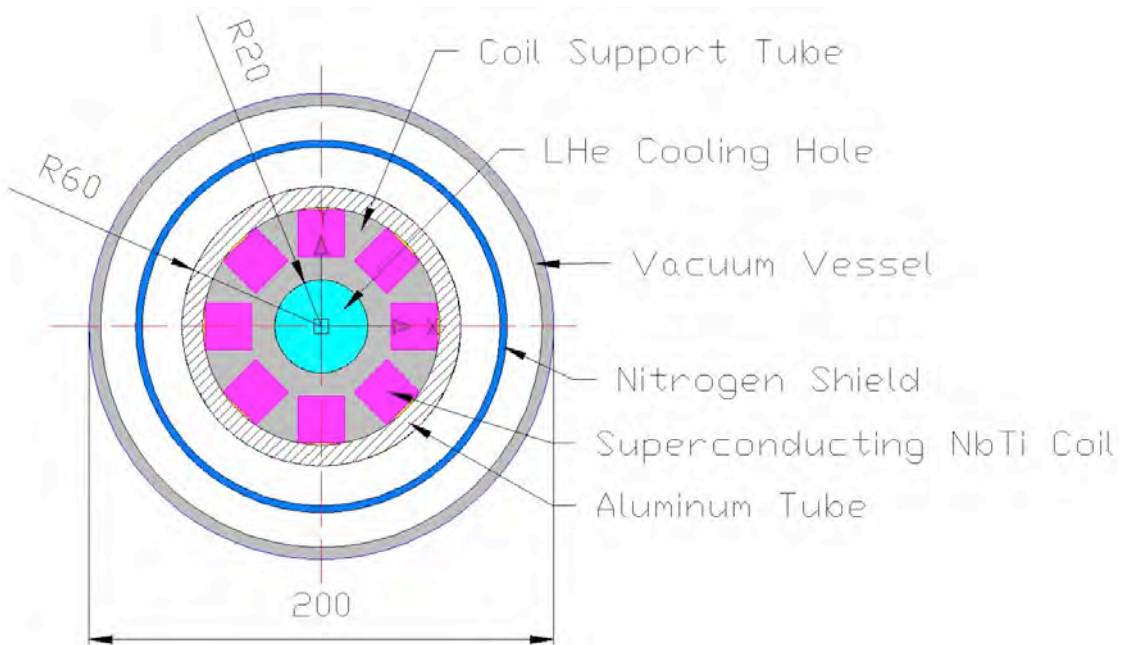


Figure 94: The cross-section of the coil inner assembly.

outermost conductors, is to put them in slots in the iron.

The NbTi superconducting coil cable could be assembled from SSC type Rutherford cables used in [210], or an ITER type cable in a conduit conductor (CICC) [211]. The NbTi CICC is widely used for ITER correction coils, poloidal coils, buses, manifold cables (See Fig. 95). The production technology and facilities are developed, and cables have been tested in Europe, Russia, and China [212–214]. CICC has direct cooling through the cooling hole for large currents (Toroidal and Central Solenoid coils) or cooling between cable strands (Correction coils, Busbars). The transmission line is one of the cost drivers of large supercon-

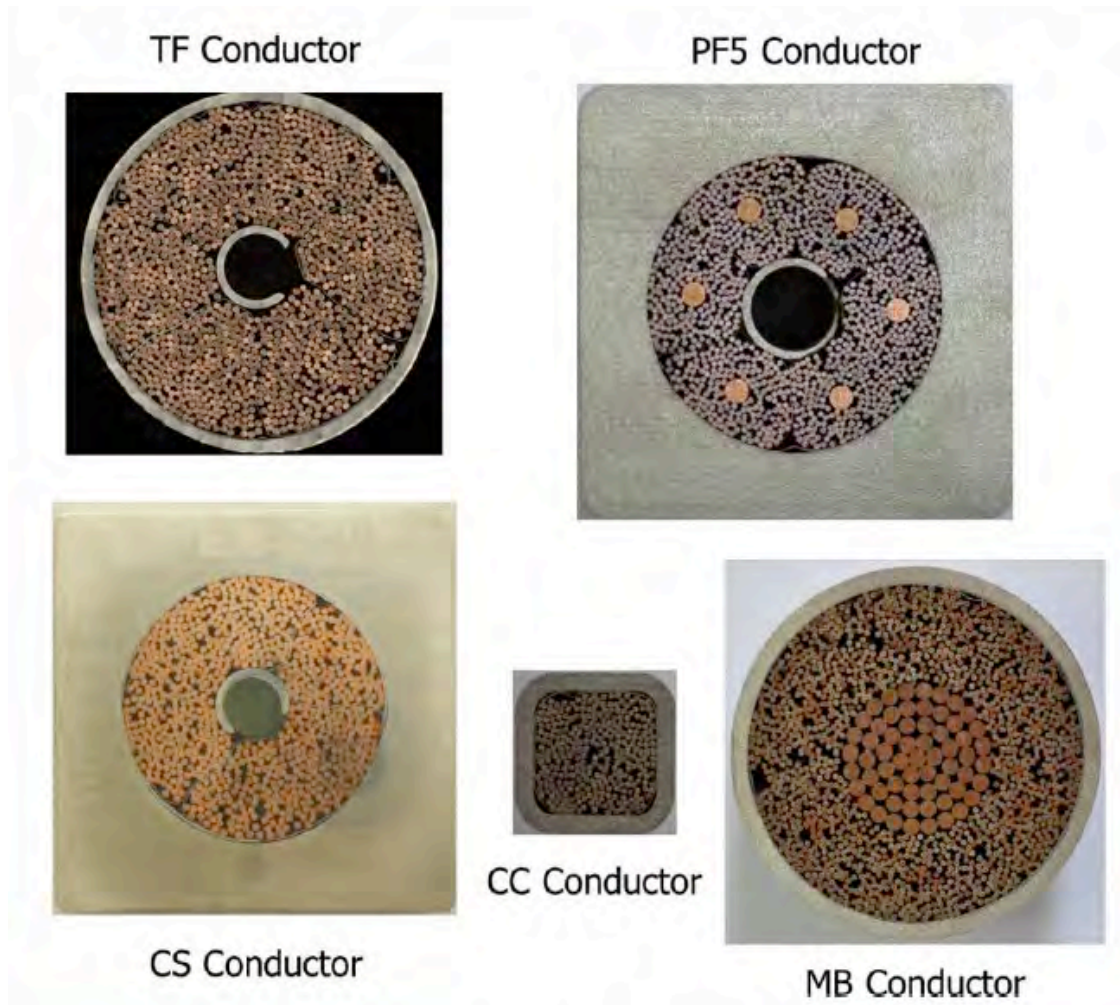


Figure 95: ITER superconducting cables.

ducting magnet systems. For the VLHC it was estimated at \$500/m. For 320 m of total transmission line length in the case of SuperBIND, this would be \$160k. The ITER project evaluated in-kind contributions for the correction coils cost of CICC at \$220/m [211]. This is equivalent to the cost analysis that was done for the VLHC in that the estimation also includes the cost of vacuum and shield tubes, Ultem spacers, and super-insulation.

6.3 Detector planes

6.3.1 Scintillator

Particle detection using extruded scintillator and optical fibers is a mature technology. MINOS has shown that co-extruded solid scintillator with embedded wavelength shifting (WLS) fibers and PMT readout produces adequate light for MIP tracking and that it can be manufactured with excellent quality control and uniformity in an industrial setting [215]. Many experiments use this same technology for the active elements of their detectors, such as the K2K Scibar [216], the T2K INGRID, P0D, and ECAL [217] and the Double-Chooz cosmic-ray veto detectors [218].

Our concept for the readout planes for SuperBIND is to have both a x and a y view between each Fe plate. Our simulations are now using a scintillator extrusion profile that is $0.75 \times 2.0 \text{ cm}^2$. This gives both the required point resolution and light yield.

6.3.2 Scintillator extrusions

The existing SuperBIND simulations have assumed that the readout planes will use an extrusion that is $0.75 \text{ cm} \times 2.0 \text{ cm}$. A 2 mm hole down the centre of the extrusion is provided for insertion of the wavelength shifting fiber. This is a relatively simple part to manufacture and has already been fabricated in a similar form for a number of small-scale applications. The scintillator strips will consist of an extruded polystyrene core doped with blue-emitting fluorescent compounds, a co-extruded TiO_2 outer layer for reflectivity, and a hole in the middle for a WLS fiber. Dow Styron 665 W polystyrene pellets are doped with PPO (1% by weight) and POPOP (0.03% by weight), which is the MINOS formulation. The strips have a white, co-extruded, 0.25 mm thick TiO_2 reflective coating. This layer is introduced in a single step as part of a co-extrusion process. The composition of this coating is 15% TiO_2 in polystyrene. In addition to its reflectivity properties, the layer facilitates the assembly of the scintillator strips into modules. The ruggedness of this coating enables the direct gluing of the strips to each other and to the module skins which results in labour and time savings. This process has now been used in a number of experiments.

Work is under way towards the development of a reflective coating using titanium dioxide (TiO_2) in low-density polyethylene (LDPE). Because polyethylene (PE) and polystyrene (PS) are not miscible, the TiO_2 -doped PE coating does not bind to the PS-based scintillator core during the co-extrusion process as it occurs in the current arrangement which uses a TiO_2 -doped PS coating on the PS-based scintillator core. The TiO_2 -doped PS coating provides a diffuse interface whereas the TiO_2 -doped PE coating traps a layer of air; thus enabling a higher degree of total internal reflection of the light produced in the scintillator. Preliminary light yield results using a radioactive source indicate that a PE coated scintillator sample has a light yield approximately 20% higher than that of a scintillator sample wrapped in a layer of Tyvek which, until now, has been the best reflective material. More effort is needed to determine the level of improvement in light yield, such as a direct comparison of the two TiO_2 -doped polymer coatings (PS and PE) and to study the conditions that a PE coating requires regarding gluing and assembly of the finished scintillator strips into detector modules. Fig. 96 shows a prototype scintillator extrusion with TiO_2 -doped LDPE cladding.

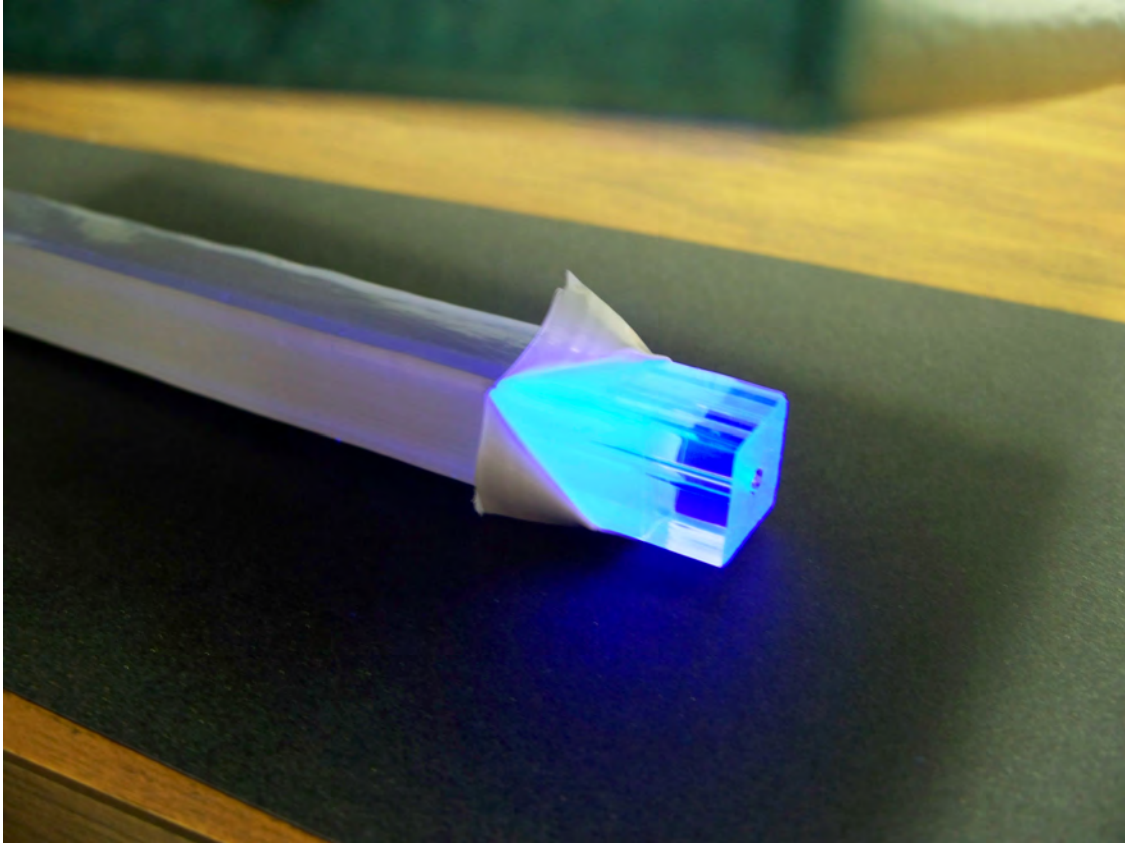


Figure 96: TiO₂ doped LDPE coated scintillator extrusion.

6.4 Photo-detector

Given the rapid development in recent years of solid-state photodetectors based on Geiger mode operation of silicon avalanche photodiodes, we have chosen this technology for SuperBIND. Although various names are used for this technology, we will use silicon photomultiplier or SiPM.

6.4.1 SiPM Overview

SiPM, which stands for Silicon Photo Multiplier, is the common name for a relatively new type of photo detector formed by combining many small avalanche photodiodes operated in the Geiger mode to form a single detector [219, 220]. The first generation of these detectors used a polysilicon resistor connected to each avalanche photodiode forming a pixel. Pixel sizes vary, and can be anywhere from 10×10 microns to 100×100 microns. All the diodes are connected to a common electrical point on one side, typically through the substrate, and all the resistors are connected to a common grid with metal traces on the other side to form a two node device. A typical SiPM will have from 100 to 10,000 of these pixels in a single device, with the total area of from 1 to 16 mm². Because all the diode and the individual quenching resistors are connected in parallel, the SiPM device as a whole appears as a single diode. In operation, the device appears to act somewhat like a conventional APD, but in detail it is radically different. Because the diodes are operated in the Geiger mode, and because every pixel of the SiPM device is nearly identical, the sum of the fired pixels gives the illusion of an analog signal that is proportional to the incident light, but it is an essentially digital device. Also, because the individual pixels operate in Geiger mode, and are individually quenched, SiPMs are typically designed to operate at very large gains, of up to 10^6 , which significantly simplifies the electronics and reduces the costs and associated technical and schedule risks.

SiPMs have a number of advantages over conventional photo multiplier tubes, including high photon detection efficiency, complete immunity to magnetic fields, excellent timing characteristics, compact size and physical robustness. They are immune to nuclear counter effects and do not age. They are particularly well suited to applications where optical fibers are used, as the natural size of the SiPM is comparable to that of fibers. But the most important single feature of the SiPM is that it can be manufactured in standard microelectronics facilities using well established processing. This means that huge numbers of devices can be produced without any manual labor, making the SiPMs very economical as the number of devices grows. Furthermore, it is possible to integrate the electronics into the SiPM itself, which reduces cost and improves performance. Initial steps have been taken in this direction, though most current SiPMs do not have integrated electronics. But it is widely recognized that this is the approach that makes sense in the long run for many applications. It improves performance and reduces cost, and can be tailored to a specific application. As the use of SiPMs spreads, so will the use of custom SiPMs with integrated electronics, just as ASICs have superseded standard logic in micro electronics. The photo counting capabilities of the SiPM are unmatched, as can be seen in Fig. 97 (right) from [221]. As is the case with other microelectronics devices, SiPMs can be customized for different applications, and currently there are a number of manufacturers providing different SiPMs of many different sizes and flavors. Some of the notable manufacturers that offer a variety of devices for purchase are (in alphabetical order): Advansid, Hamamatsu, Ketek and SensL. At a recent AIDA meeting [206] focussing on SiPM development, over 100 vendors were identified world-wide that are working on SiPM technology or are considering entering the market.

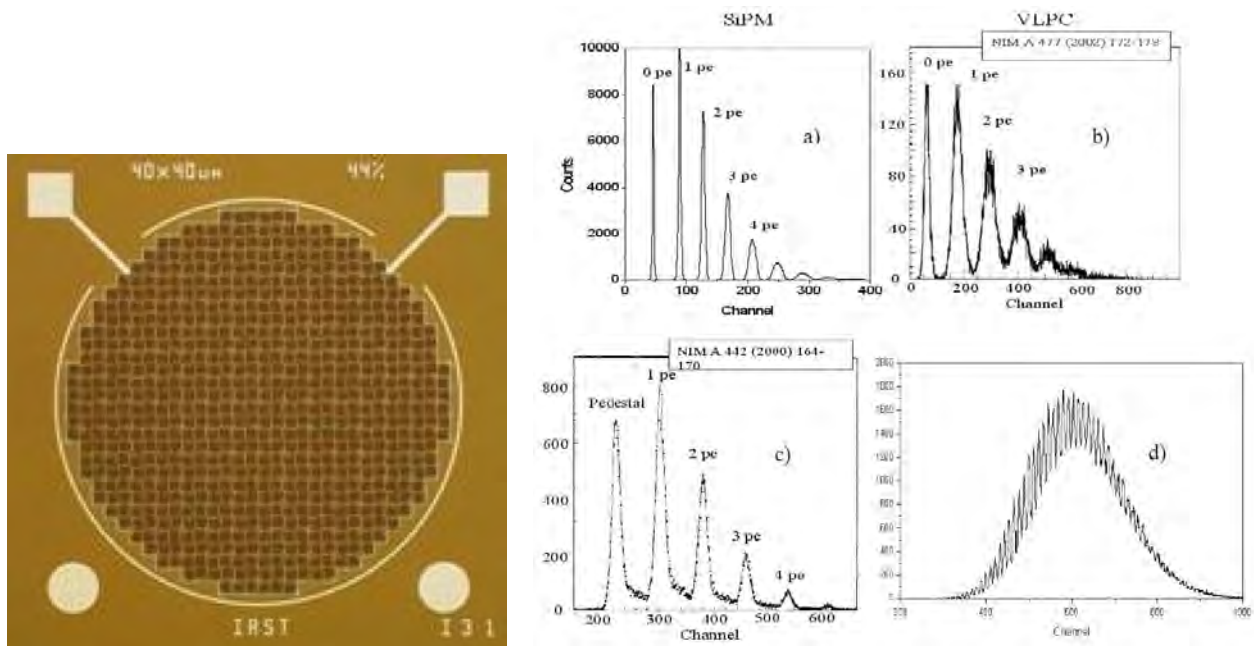


Figure 97: Photograph of SiPM (left) and SiPM photon counting capability (a) compared to VLPC (b) and HPD (c) . The SiPM pulse height spectrum (d) for an intense light burst with a mean photoelectron number of 46 is also shown.

6.4.2 Readout Electronics

The appropriate approach for instrumenting a large system revolves around the tradeoff between R&D and production costs. For smaller systems, building a system around commercial, off-the-shelf (COTS) parts is an excellent choice that minimizes engineering labor. This is the approach taken by the mu2e experiment (approximately 16 thousand SiPMs). Another common approach for systems that are sufficiently large, is to develop an application specific integrated circuit (ASIC) for the particular experiment. This can provide levels of functionality and integration that are well beyond anything that can be achieved with COTS. This is the approach taken by NOVA. This will often result in exceptional performance, far beyond what can be achieved with COTS parts, but requires a great deal of engineering and significant technical and schedule risks that must be carefully managed. A variation of this approach, to adopt existing ASICs from other experiments, is an attractive option for medium sized experiments such as MINER|*nu*A and T2K. At this point, the field has a great deal of institutionalized experience on which to draw, and this allows costs for the electronics to be projected with good accuracy, even at the early stages of a proposal. The key is that the SiPM is very well matched to the requirements of the detector- with very large gain, excellent photon detection efficiency (PDE) and immunity to magnetic fields. This makes the electronics much less challenging, meaning the risks are low and the costs well understood. SiPMs and related technologies continue to develop at a rapid pace. One of the most interesting approaches, with the greatest potential impact on the readout electronics is the development of SiPMs using standard CMOS processing. This implies that the photodetector could be integrated with the readout chip as one device. Currently, a number of companies are working on integrating electronics and SiPM detectors on the same wafer. The first such device was announced by Philips in 2009 and a complete system for evaluation of this technology is commercially available. The system features a fully digital SiPM with active quenching and it is reasonable to expect

that this technology will continue to advance and new devices with lower costs and better performance will appear.

The first approach described above presents many options to use commercially available analog SiPMs coupled to COTS electronics. Many excellent devices are available, and this is the approach taken so far by existing experiments and those planned for the near future. The mu2e experiment is considering this approach for the cosmic ray veto system (about 16k SiPMs in the baseline design.) This has the advantage of low technical risk and well understood cost. A typical implementation of the electronics might be based on commercial AFE (analog front end) chips and FPGAs, with Ethernet readout. An example of a preliminary design for mu2e is shown in Fig. 98. The second approach, adopting commercially existing SiPMs to an

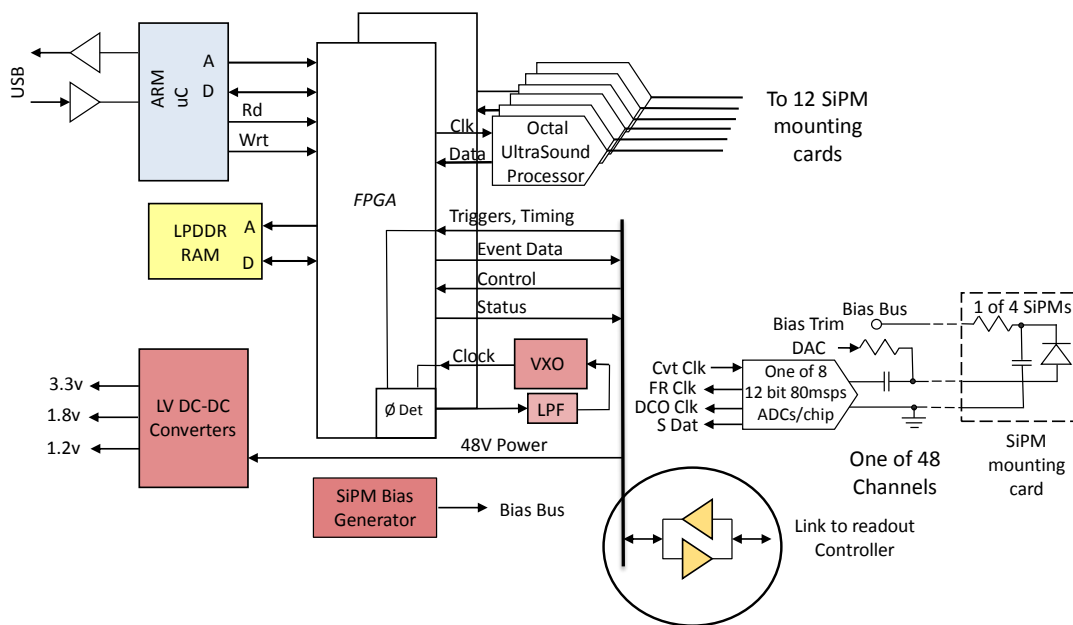


Figure 98: Example of a COTS readout card for SiPMs [222].

ASIC designed specifically for SiPMs (or one that would work well with SiPMs). This approach requires a great deal less engineering than developing a custom chip and significantly reduces the technical risk, but requires a careful evaluation of the available devices and a clear understanding of the needs of the experiment. However, there are many similarities between different experiments in high energy physics and the popularity and interest in SiPMs is driving development for various applications. Some examples of ASICs that have been used (or are being developed for use) with SiPMs are the TriP-t (developed at Fermilab for D0, used by T2K), the DRS4 (developed by PSI), TARGET (developed for Cherenkov Telescope Array) as well as EASIROC and SPIROC and similar chips developed by the Omega group at IN2P3 in Orsay. The ASIC developed for NOVA might also be a viable option. Developing a new ASIC or optimizing an existing ASIC would also be an option. By evaluating the experience of recent projects such as Minerva, T2K,

NOvA, we can estimate that the cost per channel for this approach is likely to be below \$10 per channel for the electronics (everything from photo detector to the DAQ, including bias, power, slow control, etc.). The total system costs, including R&D, engineering, prototyping, firmware development, we estimate to be about \$30 per channel. A reasonable estimate for the cost of SiPMs, including yield, dicing and testing carried out by the manufacturer is about \$2 to \$5 per square mm.

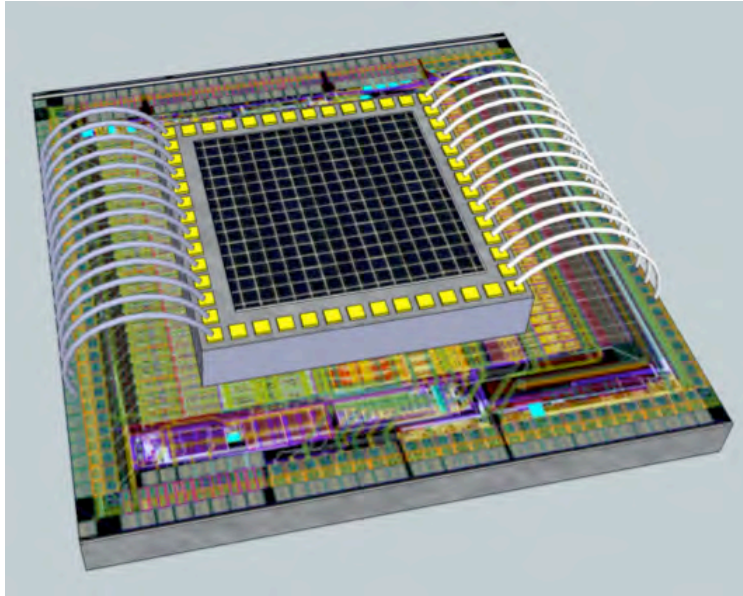


Figure 99: A possible configuration for a hybrid approach is shown. The top chip is a SiPM, wire bonded to a readout chip on the bottom. A picture of the EASIROC is used for the bottom chip. The overall size of the device is 4mm by 4mm..

The third approach is to develop a fully custom solution, using either analog or digital SiPMs optimized specifically for the experiment. This approach could potentially significantly reduce the per channel cost of both the photodetector and electronics but involves higher technical risk and requires larger initial R&D investment. This is clearly the best approach for a sufficiently large detector system. An alternative approach would be to slightly modify an existing SiPM to allow many connections between the SiPM and a readout ASIC in order to develop a hybrid solution (a near-digital SiPM), where a few SiPM pixels are routed to an output pad so that they can be wire bonded to a readout chip. This would provide most of the benefits of a full digital SiPM, but with a much shorter and simpler development effort. A conceptual design for this approach is show in Fig. 99.

7 ν Flux at near detector hall

The near detector hall at nuSTORM presents opportunities for both oscillation physics and neutrino cross section measurements. For the calculations given below, we have assumed that the hall will be located at $\sim 50\text{m}$ from the end of the straight. However, the current siting plan (see [204]) has the near detector hall located 20 m from the end of the straight. The neutrino flux at the 50 m position has been calculated and the representative number of events (per 100T fiducial mass) for a 10^{21} POT exposure is given in Fig. 100, left for ν_e and right for $\bar{\nu}_\mu$.

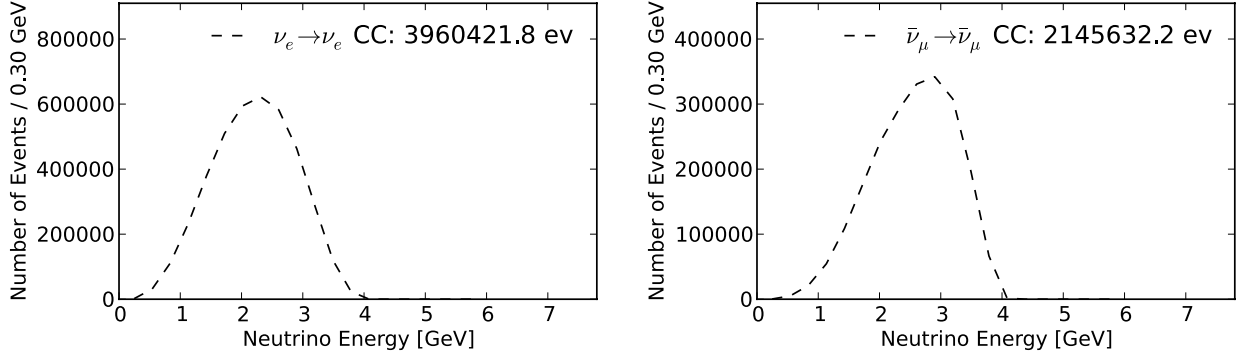


Figure 100: ν_e spectrum at near detector (Left), $\bar{\nu}_\mu$ (Right).

Channel	N_{evts}
$\bar{\nu}_\mu$ NC	844,793
ν_e NC	1,387,698
$\bar{\nu}_\mu$ CC	2,145,632
ν_e CC	3,960,421

Table 21: Event rates at near detector (for 100T) with μ^+ stored

Channel	N_{evts}
$\bar{\nu}_e$ NC	709,576
ν_μ NC	1,584,003
$\bar{\nu}_e$ CC	1,784,099
ν_μ CC	4,626,480

Table 22: Event rates at near detector (for 100T) with μ^- stored

7.1 For short-baseline oscillation physics

A near detector is needed for the oscillation disappearance searches and our concept is to build a near detector that is identical to SuperBIND, but with approximately 200T of fiducial mass. A muon ‘‘catcher’’ will most likely be needed in order to maximize the usefulness of the ‘‘as-built’’ detector mass. Before a final specification for this near detector can be made, more detailed analyses of the disappearance channels will have to be done along with an evaluation of its use as a muon spectrometer for ν interaction experiments.

8 Short-Baseline Experiment

8.1 Neutrino Flux

The number of muon decays (N_μ) for nuSTORM can be defined in terms of the following:

$$N_\mu = (\text{POT}) \times (\pi \text{ per POT}) \times \epsilon_{\text{col}} \times \epsilon_{\text{trans}} \times \epsilon_{\text{inj}} \times (\mu \text{ per } \pi) \times A_{\text{dyn}} \times \Omega \quad (3)$$

where (POT) is the number of protons on target, ϵ_{col} is the collection efficiency, ϵ_{trans} is the transport efficiency, ϵ_{inj} is the injection efficiency, (μ per π) is the chance that an injected pion results in a muon within the ring acceptance, A_{dyn} is the probability that a muon within the decay ring aperture is within the dynamic aperture, and Ω is the fraction of the ring circumference that directs muons at the far detector. The nuSTORM sensitivities described here assume 10^{21} POT using 120 GeV protons. From section 4.4, we obtain $\simeq 0.094 \pi/\text{POT}$. From the G4Beamline simulation of pion capture, transport, injection and propagation along the first straight, we obtain 8×10^{-3} muons at the end of the first straight (within the $3.8 \text{ GeV}/c \pm 10\%$ momentum band) per proton on target based on the $0.094 \pi/\text{POT}$. From Section 4.5.1, A_{dyn} is 0.6 and Ω is 0.39. This results in approximately 1.9×10^{18} useful μ decays. With a 1kT fiducial mass far detector located at approximately 2 km from the end of the decay ring straight, we have the following raw event rates:

Neutrino mode with stored μ^+ .				
Channel	$N_{\text{osc.}}$	N_{null}	Diff.	$(N_{\text{osc.}} - N_{\text{null}})/\sqrt{N_{\text{null}}}$
$\nu_e \rightarrow \nu_\mu$ CC	332	0	∞	∞
$\bar{\nu}_\mu \rightarrow \bar{\nu}_\mu$ NC	47679	50073	-4.8%	-10.7
$\nu_e \rightarrow \nu_e$ NC	73941	78805	-6.2%	-17.3
$\bar{\nu}_\mu \rightarrow \bar{\nu}_\mu$ CC	122322	128433	-4.8%	-17.1
$\nu_e \rightarrow \nu_e$ CC	216657	230766	-6.1%	-29.4
Anti-neutrino mode with stored μ^- .				
Channel	$N_{\text{osc.}}$	N_{null}	Diff.	$(N_{\text{osc.}} - N_{\text{null}})/\sqrt{N_{\text{null}}}$
$\bar{\nu}_e \rightarrow \bar{\nu}_\mu$ CC	117	0	∞	∞
$\bar{\nu}_e \rightarrow \bar{\nu}_e$ NC	30511	32481	-6.1%	-10.9
$\nu_\mu \rightarrow \nu_\mu$ NC	66037	69420	-4.9%	-12.8
$\bar{\nu}_e \rightarrow \bar{\nu}_e$ CC	77600	82589	-6.0%	-17.4
$\nu_\mu \rightarrow \nu_\mu$ CC	197284	207274	-4.8%	-21.9

Table 23: Raw event rates for 10^{21} POT (for stored μ^+ and stored μ^-) for best-fit values for the LSND anomaly figure-of-merit.

In addition to the μ decay beam, we also have a high-intensity π decay neutrino beam, $\bar{\nu}_\mu^{(\pi)}$, from the straight section (at injection into the ring) which can easily be time separated from the μ decay beam. This $\bar{\nu}_\mu^{(\pi)}$ is roughly the same intensity as the integrated $\bar{\nu}_\mu^{(\pi)}$ beam from the stored μ decays.

8.2 Monte Carlo

A detailed detector simulation and reconstruction program has been developed to determine the detector response for the far detector in the short baseline experiment. The simulation is based on software developed for the Neutrino Factory Magnetized Iron Neutrino Detector (MIND) [223].

8.2.1 Neutrino Event Generation and Detector Simulation

An effort was made to ground the simulation in a software framework common to other neutrino simulation efforts. GENIE [224] is used to generate neutrino events in steel and scintillator. Events are passed to a GEANT4-based [225] simulation for the propagation of the final-state particles through successive steel and scintillator layers. This simulation includes hadron interactions simulated by the QGSP.BERT physics list [225].

The simulation allows for the customization of the detector layers and overall dimensions for the purpose of detector optimization studies. For the purpose of the results described here, the detector is composed of modules consisting of a 1.5 cm steel plate and a 1.5 cm thick scintillator plane with a 0.5 cm air gap between modules. For a detector 6 m in diameter, 343 modules are required to make up the 1.3 kTon far detector, for a total length of 12.4 m. Some optimization of the detector configuration has been done including variations in the steel plate thickness and the scintillator thickness and an equal thickness of both provides the best outcome in reconstruction efficiency and physics performance.

Hits in the scintillator are grouped into clusters, smearing the detector hit position, and energy deposition of the accumulated hits is attenuated in a simple digitization algorithm applied prior to reconstruction. A double ended readout is assumed for this digitization. It is assumed that each Silicon photo-multiplier readout receives 1/4 of the energy deposited in a 2×2 cm² unit cell, attenuated over the distance between the hit position and the edge of the detector. The detector performance is not strongly affected by the cell size, which is determined by the transverse width of the scintillator bars. Simulations have been run with scintillator bar widths from 1 cm to 3 cm and there was very little change in the performance.

Some assumptions were made for the light yield and electronics performance. The attenuation length in the wavelength shifting fibers is assumed to be 5 m. The SiPMs are assumed to have an energy resolution of 6% with a conservative threshold of 4.7 photo-electrons and a photodetector quantum efficiency of $\sim 30\%$ [205]. A minimum ionizing particle produces up to 80 photo-electrons in a scintillator bar so a high detection efficiency is expected. Simulations ran with a lower collection threshold of 2 photo-electrons find no significant change in the detection efficiency.

Magnetization within the steel is introduced with an empirically derived formula. The magnetic field is parametrized as:

$$B_\phi(r) = B_0 + \frac{B_1}{r} + B_2 e^{-Hr} ; \quad (4)$$

where $B_0 = 1.36$ T, $B_1 = 0.04$ T m, $B_2 = 0.80$ T, and $H = 0.16$ m⁻¹. This parametrization and the field along the 45° azimuthal direction are shown in Fig. 101. The difference between the field map of the steel plate and the parametrization is less than 1%. The polarity of the magnetic field was chosen to focus negative charges towards the center of the detector for the study of ν_μ interactions.

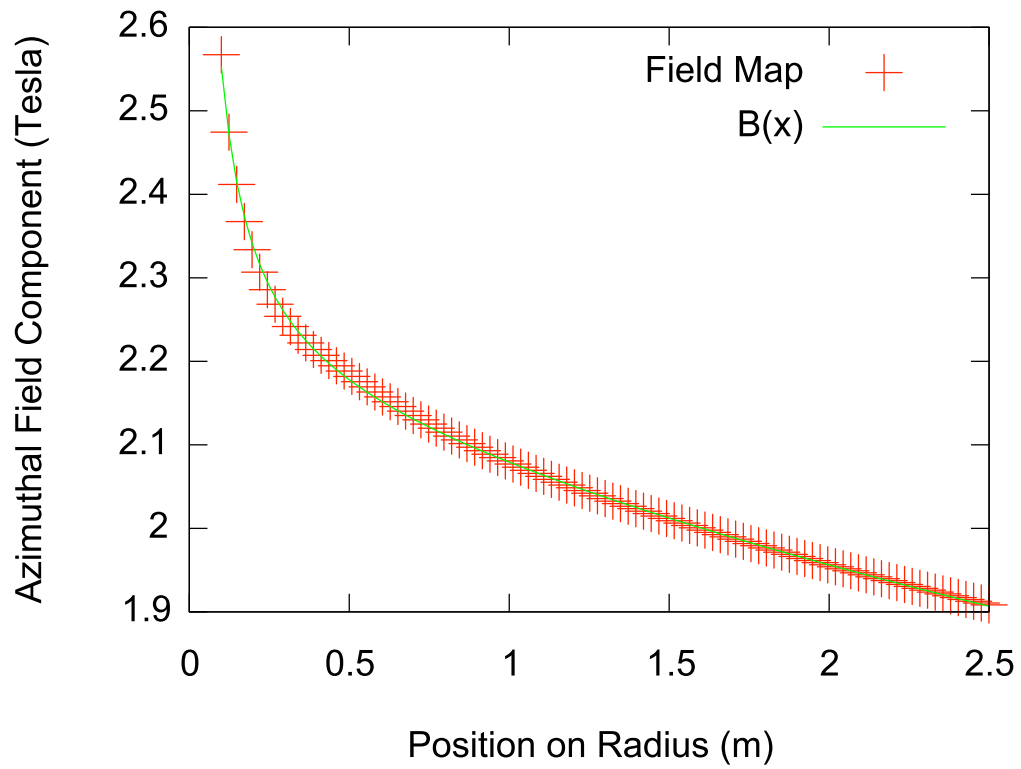


Figure 101: The magnetic field magnitude as a function of radius along the 45° azimuth with the parametrization used in the detector simulation.

8.2.2 Event Reconstruction

The reconstruction uses multiple passes of a Kalman-filter algorithm to identify muon trajectories within events and to determine the momentum and charge of an identified track. Multiple tracks are identified within the simulation, and all identified tracks are fit to determine the length of the tracks. The longest track is chosen as the prospective muon track for the event and all other tracks are assumed to be the result of pion production or electron showers. The secondary tracks are important in the case of resonant pion production where there may be a visible pion at a lower angle than the muon track.

The Kalman filtering and fitting algorithms are supplied by the RecPack software package [226]. Geometrical information from the track including the length of the track, the direction of bending in the magnetic field, and the pitch of the track are used at various points in this procedure to provide initial state information to the Kalman filter. The momentum and charge is determined from the track curvature.

The hadron reconstruction is not yet well developed, so the neutrino energy is reconstructed by using the quasi-elastic approximation, if no hadronization is visible. If there are secondary tracks or hits that are not associated with a track, the true hadron energy is smeared according to the results of the MINOS CalDet test beam results[205]:

$$\frac{\delta E_{had}}{E_{had}} = \frac{0.55}{\sqrt{E_{had}}} + 0.03. \quad (5)$$

A future SuperBIND prototype, such as the AIDA MIND [206] prototype, is anticipated to refine this measurement.

8.3 Data Analysis

Following the reconstruction, the events are analyzed to select events with well reconstructed muon tracks, and remove tracks that are mis-identified from pions or electron showers. This analysis for appearance and disappearance experiments differs in the charge of the muon that is selected for the signal. For the appearance analysis the charge of the muon signal is opposite to that of the muon in the storage ring, while the disappearance analysis signal is a like sign muon. For the following discussion, a paired experiment with stored μ^+ is considered.

8.3.1 Appearance

To achieve the target of 10σ significance for the LSND anomaly the background efficiency must be reduced to less than a few parts in 10^5 . This can be achieved with a cuts based analysis such as that previously used for the neutrino factory [223], but a multivariate analysis is preferred as it yields more robust results overall. Both analyses are described here.

The cuts based approach relies on the sequence of cuts shown in Table 24. The majority of these cuts are made to ensure that the trajectory-fit is of good quality. Cuts are made to remove events that are not successfully reconstructed, with a starting position closer than 1 m from the end of the detector. Events are rejected if the reconstructed muon track has fewer than 60% of all detector hits assigned to the trajectory, the momentum is greater than 1.6 times the maximum neutrino energy, or the charge of the fitted trajectory does not match the charge derived from a geometric definition of the curvature.

Table 24: The cuts used in an analysis of a nuSTORM ν_μ appearance analysis with SuperBIND.

Variable	Description
Trajectory Identified	There must be at least one trajectory identified in the event.
Successful Fit	The longest identified trajectory must be successfully fit.
Maximum Momentum	The momentum of the longest trajectory is less than 6 GeV/c.
Fiducial	The longest trajectory must start prior to the last 1 m of the detector.
Minimum Nodes	the fit to the longest trajectory must include more than 60% of the hits assigned to trajectory by the filter.
Curvature Ratio	$(q_{init}/p_{range}) \times (p_{fit}/q_{fit}) > 0$
Track Quality	$\log P(\sigma_{q/p}/(q/p) CC) - \log P(\sigma_{q/p}/(q/p) NC) < -0.5$
NC Rejection	$\log P(N_{hits} CC) - \log P(N_{hits} NC) > 7$

Table 25: The fraction of events left after cuts are applied to the simulations of the indicated species in the nominal SuperBIND detector when the appearance of a μ^- in an event is defined as the experimental signal. Determined from simulations of 1.5×10^6 ν_μ CC and $\bar{\nu}_\mu$ CC interactions and 5×10^6 $\bar{\nu}_\mu$ NC, ν_e CC, and ν_e NC interaction events.

Event Cut	Interaction Type and Species				
	ν_μ CC(%)	$\bar{\nu}_\mu$ CC ($\times 10^3$)	ν_e CC ($\times 10^3$)	$\bar{\nu}_\mu$ NC ($\times 10^3$)	$\bar{\nu}_e$ CC ($\times 10^3$)
Successful Reconstruction	71.1%	51.2	482	102	166
Fiducial	70.8%	50.1	474	101	164
Maximum Momentum	68.8%	32.1	397	82.6	135
Fitted Proportion	67.9%	30.4	388	80.5	132
Curvature Ratio	48.5%	12.7	266	52.0	85.5
Track Quality	41.7%	2.3	40.1	13.8	47.5
NC Rejection	13.8%	0.004	0.008	0.003	0.008

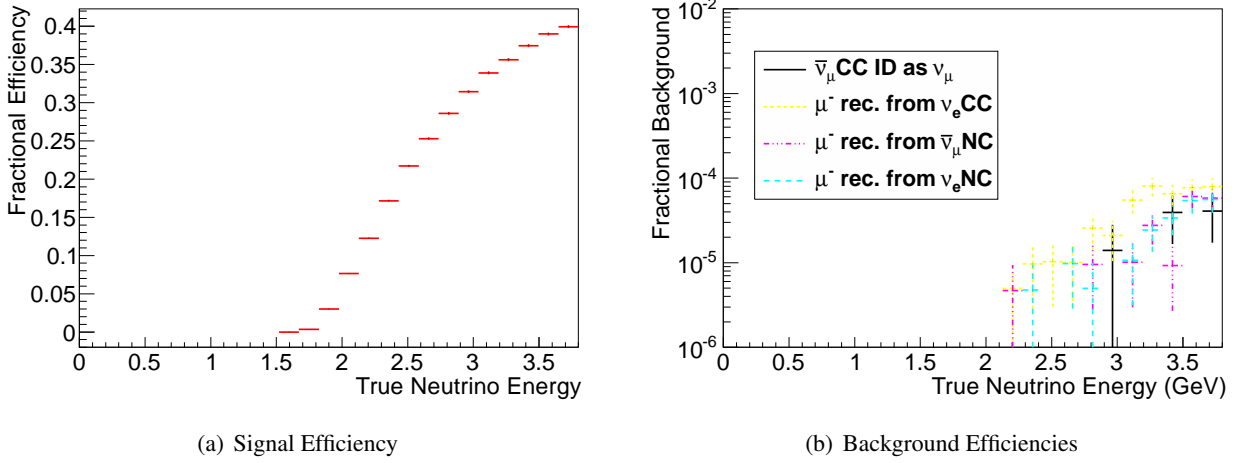


Figure 102: Signal and background efficiencies for the detection of a μ^- signal that will be present when μ^+ are contained in the nuSTORM storage ring as determined by the cuts based analysis.

Two further cuts—the track quality and NC rejection cuts—affect the ratio of signal to background. The track quality cut is based on the relative error of the inverse momentum of the candidate muon $|\sigma_{q/p}/(q/p)|$ where q is the charge of the muon and p is its momentum. Probability distribution functions, $P(\sigma_{q/p}/(q/p))$, are generated from pure charged-current (CC) and neutral-current (NC) samples. A log-likelihood ratio, $\mathcal{L}_{q/p}$, is created from the ratio of the CC and NC probabilities for a given trajectory:

$$\mathcal{L}_{q/p} = \log \left(\frac{P(\sigma_{q/p}/(q/p)|CC)}{P(\sigma_{q/p}/(q/p)|NC)} \right). \quad (6)$$

An event is accepted if $\mathcal{L}_{q/p} > -0.5$. The NC rejection cut is likewise defined using a log-likelihood ratio defined using the number of hits used in a fit to a particular trajectory, N_{hit} , for CC and NC samples. It has found that the background rejection can be reduced to below parts in 10^{-5} if:

$$\mathcal{L}_{CC} = \log \left(\frac{P(N_{hit}|CC)}{P(N_{hit}|NC)} \right) > 7. \quad (7)$$

The impact of all of these cuts on the simulated event samples is shown in Table 25. The signal and background efficiencies are shown in Fig. 102(a) and 102(b), respectively.

An important limitation of this approach is the high energy threshold and the lack of plateau in the signal efficiency. This is a result of the restrictive nature of the cuts necessary to achieve the required background rejection. The \mathcal{L}_{CC} cut is particularly responsible for the shape of this threshold as the number of hits in a trajectory is a measure of the longitudinal momentum. The cut on \mathcal{L}_{CC} has the strongest impact on reducing the background, so it can not be relaxed in this analysis. The alternative is to introduce additional variables, but this has been demonstrated to only reduce the signal efficiency in a cuts based framework. For this reason a multi-variate analysis was tested for use in SuperBIND.

The multi-variate analysis is facilitated by the ROOT based TMVA package[227]. This analysis outperforms the cuts based analysis by offering a lower energy signal threshold and increasing the sensitivity of the experiment to oscillations.

The analysis is trained to discriminate between ν_μ charge current (CC) interaction signal events and $\bar{\nu}_\mu$ neutral current (NC) interaction background events using a set of five parameters to define a classifier variable. The majority of these parameters were chosen from the experience of the MINOS experiment [228].

Table 26: Variables used in the analysis of events in the SuperBIND simulation. Variables in 26(a) are used in the definition of the classifier, while the cuts in 26(b) are fixed.

(a) Variables used in the multivariate analysis.

Variable	Description
Track Quality	$\sigma_{q/p}/(q/p)$, the error in the trajectory curvature scaled by the curvature
Hits in Trajectory	The number of hits in the trajectory
Curvature Ratio	$(q_{init}/p_{range}) \times (p_{fit}/q_{fit})$: comparison of the initial guess of the curvature to the Kalman fit result.
Mean Energy Deposition	Mean of energy deposition of hits in fit of the trajectory
Variation in Energy	$\sum_{i=0}^{N/2} \Delta E_i / \sum_{j=N/2}^N \Delta E_j$ where the energy deposited per hit $\Delta E_i < \Delta E_{i+1}$.

(b) Preselection variables.

Variable	Description
Trajectory Identified	There must be at least one trajectory identified in the event.
Successful Fit	The longest identified trajectory must be successfully fit.
Maximum Momentum	The momentum of the longest trajectory is less than 6 GeV/c.
Fiducial	The longest trajectory must start prior to the last 1 m of the detector.
Minimum Nodes	The fit to the longest trajectory must include more than 60% of the hits assigned to the trajectory by the filter.
Track Quality	$\sigma_{q/p}/(q/p) < 10.0$
Curvature Ratio	$(q_{init}/p_{range}) \times (p_{fit}/q_{fit}) > 0$

Table 26(a) summarizes these parameters. A set of preselection cuts, detailed in Table 26(b) are applied to limit the analysis to the subset of events containing useful data. These preselection cuts are common to both analyses, as their purpose of removing poor tracks is unchanged. The multi-variate analysis is trained using a variety of methods, but the best performance is achieved using a Boosted Decision Trees (BDT). Based on the performance of this method, shown in Fig. 103, events are selected if the BDT classifier variable is greater than 0.86. The optimized analysis produces the efficiency contours in signal and backgrounds shown in Fig. 104. Other methods including a neural network (MLPBNN) and the k Nearest Neighbor (kNN) method were tested but they do not produce sufficient background rejection to achieve the statistical aims for the appearance analysis. The BDT method has a much greater integrated efficiency than the previously developed cuts based analysis with a lower energy threshold.

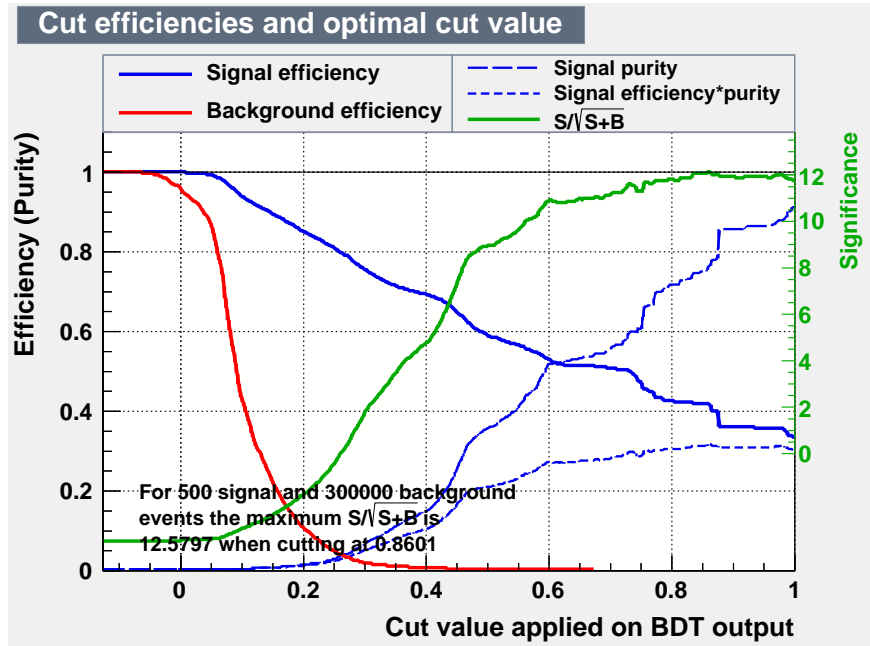
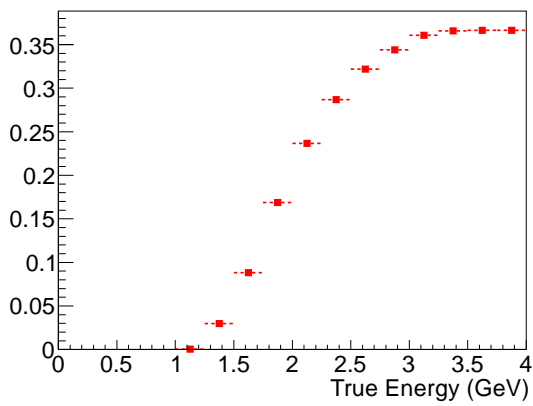


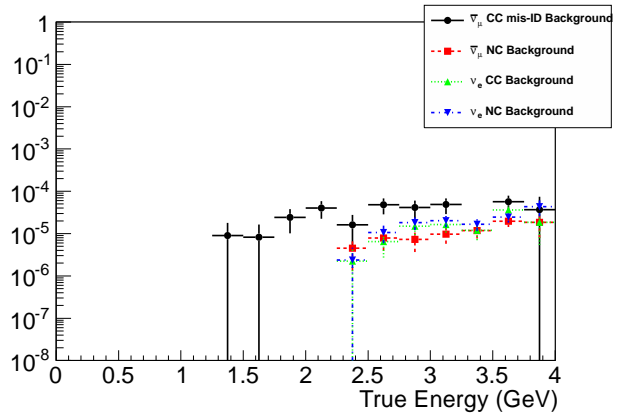
Figure 103: Results from training the BDT method to simulations of $\nu_{\mu}CC$ signal events and $\bar{\nu}_{\mu}$ background events, assuming a realistic number of events.

8.3.2 $\bar{\nu}_{\mu}$ Disappearance

The $\bar{\nu}_{\mu}$ disappearance analysis has a different optimization criteria from that of the appearance analysis. A disappearance experiment relies on the difference between the shape of the oscillated spectrum versus that of the unoscillated spectrum. An optimization based on a χ^2 statistic comparing these two spectra is used, assuming a 3+1 neutrino model with $\Delta m_{14}^2 = 0.89 \text{ eV}^2$ and $\sin^2 2\theta_{\mu\mu} = 0.09$. The conclusion of this optimization is that a neural network method (MLPBNN) shows the best response when events with a classifier variable greater than 0.94 is selected. The background and efficiency curves for this optimization are shown in Fig. 105. In this particular case, the energy threshold is below 1 GeV because background efficiencies on the order of 1% are reasonable. A similar optimization was not done using a cuts-based framework.

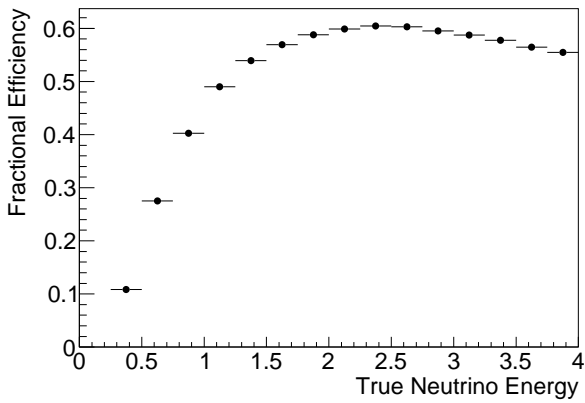


(a) Signal Efficiency

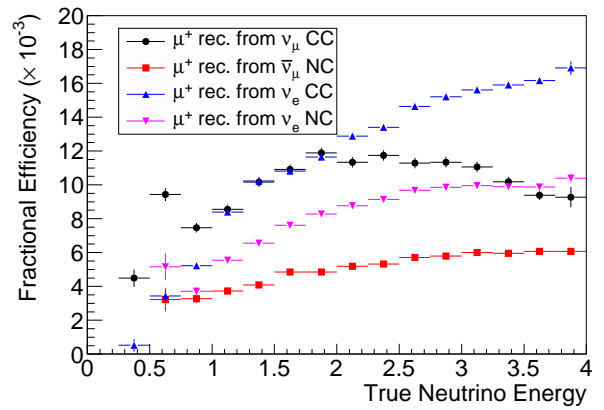


(b) Background Efficiencies

Figure 104: Signal and background efficiencies for the detection of a μ^- signal that will be present when μ^+ are contained in the nuSTORM storage ring as determined by a boosted decision tree multivariate analysis.



(a) Signal Efficiency



(b) Background Efficiency

Figure 105: Efficiency curves for the $\bar{\nu}_\mu$ disappearance analysis produced from the optimized analysis.

8.4 Sensitivities

The appearance of ν_μ , via the channel $\nu_e \rightarrow \nu_\mu$, gives nuSTORM broad sensitivity to sterile neutrinos and directly tests the LSND/MiniBooNE anomaly. The oscillation probabilities for both appearance and disappearance modes are:

$$P_{\nu_e \rightarrow \nu_\mu} = 4|U_{e4}|^2|U_{\mu4}|^2 \sin^2\left(\frac{\Delta m_{41}^2 L}{4E}\right); \text{ and} \quad (8)$$

$$P_{\nu_\alpha \rightarrow \nu_\alpha} = 1 - [4|U_{\alpha4}|^2(1 - |U_{\alpha4}|^2)] \sin^2\left(\frac{\Delta m_{41}^2 L}{4E}\right). \quad (9)$$

The detector is designed for the appearance signal $\nu_e \rightarrow \nu_\mu$; the CPT conjugate of the channel with which LSND observed an anomaly, $\bar{\nu}_\mu \rightarrow \bar{\nu}_e$. Although it is clear from equation 8 that the appearance channel is doubly suppressed relative to the disappearance channel, the experiment is much more sensitive to the appearance channel because the backgrounds for wrong-sign muon searches can be suppressed more readily. The systematic effects, while common to both channels, will have different impacts on their respective sensitivities to a sterile neutrino signal.

8.4.1 Systematics

Systematic uncertainties for short baseline ν_μ oscillation experiments at nuSTORM have been given some consideration [229]. The great benefit of using a muon beam as a neutrino source is that many of the beam related systematics may be reduced significantly. A list of systematics taken from the existing literature is given in Table 27, with the anticipated systematic uncertainties for nuSTORM short baseline experiments.

The leading systematic uncertainties for a short baseline experiment at nuSTORM are in the prediction of the flux convoluted with the cross section at the far detector. Based on the estimates made for the 25 GeV neutrino factory[230], the neutrino beam from the muon decay ring should be known to 0.1% based on the characteristics of the muon beam. The characterization would be accomplished with a combination of beam current transformers, beam position monitors, polarimeters, and wire scanners. The low current in the nuSTORM ring may reduce the precision of these measurements, and the flux uncertainty, to 1-3%, conservatively.

A leading cause of uncertainties particular to the cross sections are differences in the quasi-elastic interactions between neutrinos and anti-neutrinos for both ν_e and ν_μ . These cross-sections are anticipated to be measured at the nuSTORM near detector site using runs of stored μ^+ and μ^- . The uncertainty of such measurements would then be dominated by the flux uncertainty. The MINOS experiment sets an uncertainty on the convoluted flux with the cross-section of 4% for the signal [228]. Background uncertainties are further limited by the ability to reproduce the false signal backgrounds in neutral current events. In this context the MINOS experiment assesses a 40% normalization error [228] due to uncertainties in the associated production mechanisms such as the resonant pion production and a 15% uncertainty in the hadronic model. Again it is likely that refined measurements at nuSTORM will reduce these systematic uncertainties.

Other systematics and backgrounds have also been considered. The potential variation in the thickness of the steel plate has been considered based on the MINOS construction specifications. These variations

Table 27: Systematic uncertainties expected for a short baseline muon neutrino appearance experiment based at the nuSTORM facility.

Uncertainty	Known Measures			Expected Contribution	
	Signal	Background	Reference	Signal	Background
Source luminosity	1%	1%	[229]	1%	1%
Cross section	4%	40%	[232]	0.5%	5%
Hadronic Model	0	15%	[233]	0	8%
Electromagnetic Model	2%	0	[233]	0.5%	0
Magnetic Field	<1%	<1%	[229]	<1%	<1%
Steel	0.2%	0.2%	[229]	0.2%	0.2%
Total	5%	43%		1%	10%

have a direct impact on the magnetic field production, and particle range in the detector. A simulation was run with random variations in the steel plates. The simulation showed a negligible impact on the ability of the apparatus to distinguish signal from background. External backgrounds in the form of rock muons and cosmic ray muons were considered through both analytical calculations and with the CRY cosmic ray generator [231] with a GEANT4 simulation. It is believed that a fiducial cut removing external events will reduce these backgrounds by a factor of 10^8 , yielding on the order of 1 muon over 5 years of exposure.

It is anticipated that the contributing uncertainties can be reduced to less than 1% for signal events and 10% for background events. The combined existing systematic uncertainties can be as much as five times these numbers. Thus an upper limit on the potential systematic uncertainties of 5% for signal and 50% for background is assumed for the sensitivity calculations.

8.4.2 ν_μ Appearance

The detector response derived from simulation is used to determine the sensitivity of the appearance experiment to the presence of sterile neutrinos. The sensitivities and optimizations were computed using GLoBES [83]. Modifications were made to simulate accelerator effects such as the integration of the decay straight as outlined in [229, 234] and to include the non-standard interactions for sterile neutrino oscillations [235]. The detector response is summarized as a “migration” matrix of the probability that a neutrino generated in a particular energy bin i is reconstructed in energy bin j . Defined in this way, the migration matrix encapsulates both the resolution of the detector and its efficiency. Samples of all neutrino interactions that could participate in the experiment are generated to determine the response for each detection channel.

The spectrum of expected signal and background for this simulation is shown in Fig. 106 assuming 1.8×10^{18} μ^+ decays and a 2 km baseline. A contour plot showing the sensitivity of the ν_μ appearance experiment to sterile neutrinos appears in Fig. 107 showing the results of the multi-variate analysis with the ideal systematics and inflated systematics as well as the results of the cuts based analysis. These contours are shown with respect to the derived variable $\sin^2 2\theta_{e\mu} = 4|U_{e4}|^2|U_{\mu4}|^2$. Systematic uncertainties are included in the contour as stated. The contours derived from the latest fits to existing appearance data and to the data showing evidence of sterile neutrino oscillations [49] are also shown. This study shows that the multi-variate analysis is sensitive to the phase space covered by the existing 99% contours well above the 10σ level, even with the systematics inflated by a factor of five.

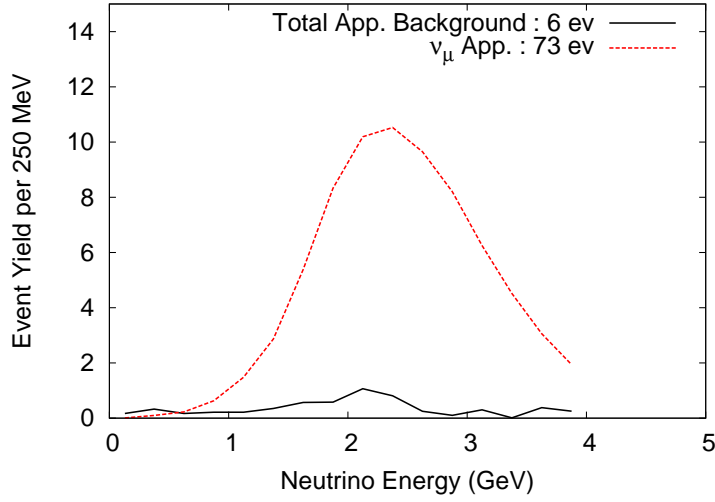


Figure 106: The neutrino spectrum of a ν_μ appearance experiment measured at the SuperBND far detector using the simulated detector response.

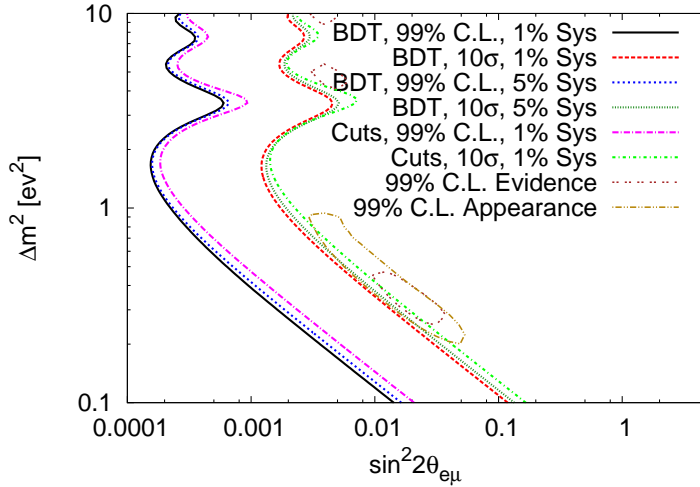


Figure 107: Contours of the χ^2 deviation from the no-sterile neutrino hypothesis corresponding to a 99% C.L. (2.575σ) and 10σ variations. Two different sets of systematic uncertainties are represented; the default systematics with 1% signal uncertainty and a 10% background uncertainty and a conservative set that is five times larger. A cuts based analysis is also shown. The 99% confidence level contours from a global fit to all experiments showing evidence for unknown signals (appear + reactor + Gallium) and the contours derived from the accumulated data from all applicable neutrino appearance experiments [49] are also shown.

8.4.3 $\bar{\nu}_\mu$ Disappearance

As noted above, a disappearance experiment is potentially more sensitive to the oscillation amplitudes than the appearance analysis. However, it is also more sensitive to the signal normalization than an appearance experiment. The neutrino flux is extremely well understood for nuSTORM, but further understanding of the measured spectrum resulting from the combination of efficiencies and cross sections is required. To control these effects, a near detector identical to the far detector is required. This is the motivation behind the 200 Ton version of SuperBIND at the near detector site. A simulation of such a near detector is in progress, so an approximation of the anticipated systematic must be made. Combined fits of near and far detector rates are standard practice in oscillation experiments [236] and an optimization for such an experiment at an early version of nuSTORM has already been done [21] for an idealized ν_e disappearance experiment assuming different beam properties. For the current discussion, the systematic uncertainties are assumed to be identical to the signal systematics described in the appearance context.

The sensitivity of the experiment is computed using GLOBES as in the appearance experiment with the only difference in the selection of the like sign muon. The signal and background spectra, after the application of detector response, with and without light sterile neutrino oscillations are shown in Fig. 108. As with the appearance analysis, sensitivity contours to short baseline oscillations were generated assuming 3.2×10^{17} μ^+ decays per year collected over 5 years in a 1.3 kTon detector. The contours with respect to the effective mixing angle $\sin^2 2\theta_{\mu\mu} = 4U_{\mu 4}^2(1 - U_{\mu 4}^2)$ are shown in Fig. 109. To improve on the phase space covered with the exclusion limits from the fits to the existing data[49], the experiment needs better than the 5% signal systematic shown as an upper limit. This figure shows the great sensitivity of the disappearance experiment to systematic effects that is not as acute in the appearance analysis. The expected sensitivity given the lower bound on the systematic uncertainties will improve on the 99% C.L. from the fits to the existing data [49].

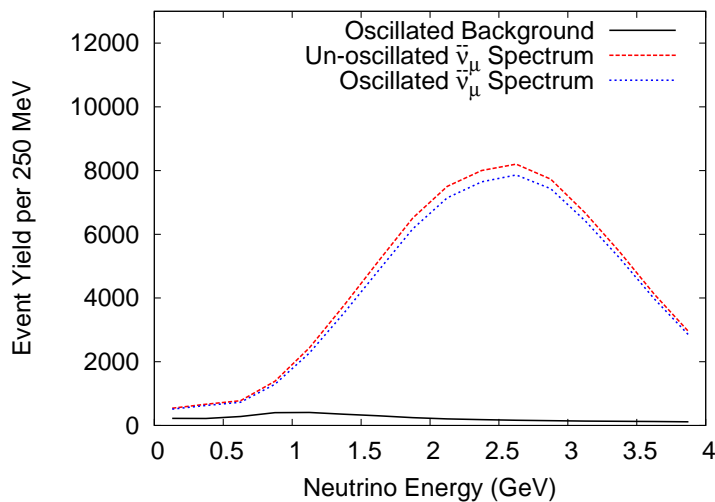


Figure 108: The expected number of events for a short baseline $\bar{\nu}_\mu$ disappearance experiment at nuSTORM assuming $\Delta m_{14}^2 = 0.89$ and $\sin^2 2\theta_{\mu\mu} = 4U_{\mu 4}^2(1 - U_{\mu 4}^2) = 0.09$.

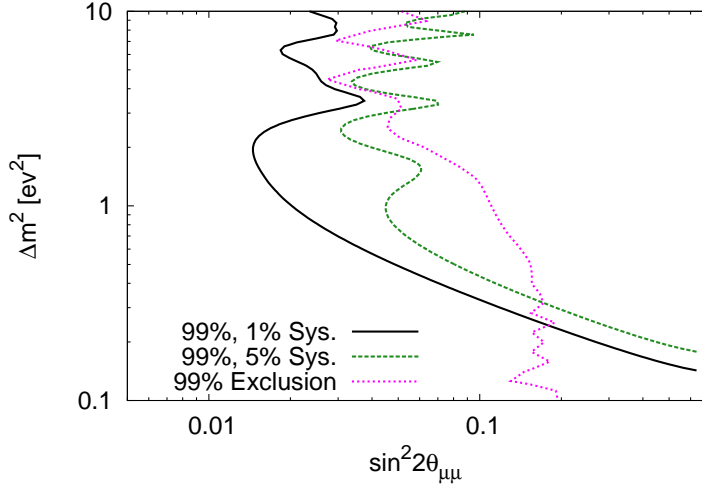


Figure 109: The sensitivity of a disappearance experiment at nuSTORM to the presence of a light sterile neutrino oscillation. Contour generated using GLOBES, assuming a 1.3 kTon far detector, 2 km away from the muon storage ring, exposed to neutrinos resulting from an exposure of 1.6×10^{18} useful muon decays. A 1% signal and 10% background systematic uncertainty is assumed by default. The 99% C.L. bound, assuming a systematic error multiplied by a factor of 5, is also shown with the existing experimental bounds [49]

8.4.4 Combined Appearance and Disappearance

Combining appearance and disappearance information from the muon neutrino channels is important because the channels provide complementary information and they will be observable in the nuSTORM beam at the same time. The migration matrices derived for the two experiments are completely uncorrelated because of the difference in the charge of the selected signal, i.e., like sign muon signal rather than opposite sign muons.

A simultaneous fit using both appearance and disappearance results will make the best use of the available data. This is accomplished for a given Δm_{14}^2 and effective mixing angle (either $\sin^2 2\theta_{e\mu}$ or $\sin^2 2\theta_{\mu\mu}$) through the use of a simple fit which finds the minimum χ^2 between the sterile hypothesis and the null hypothesis as a function of $|U_{\mu 4}|$ (for $\sin^2 2\theta_{e\mu}$) or $|U_{e 4}|$ (in the case of $\sin^2 2\theta_{\mu\mu}$).

The sensitivity contour derived from the combination of ν_μ appearance and $\bar{\nu}_\mu$ disappearance is shown with respect to $\sin^2 2\theta_{e\mu}$ is shown in Fig. 110(a) and with respect to $\sin^2 2\theta_{\mu\mu}$ in Fig. 110(b). The combined sensitivity shows an improved performance over the appearance experiment alone at $\Delta m_{14}^2 > 0.8 \text{ eV}^2$. The improvement is marginal but it does reduce the constraints on the systematic uncertainties required to achieve the 10σ benchmark for a short baseline experiment. The improvement over the disappearance experiment alone is more significant for all Δm_{14}^2 .

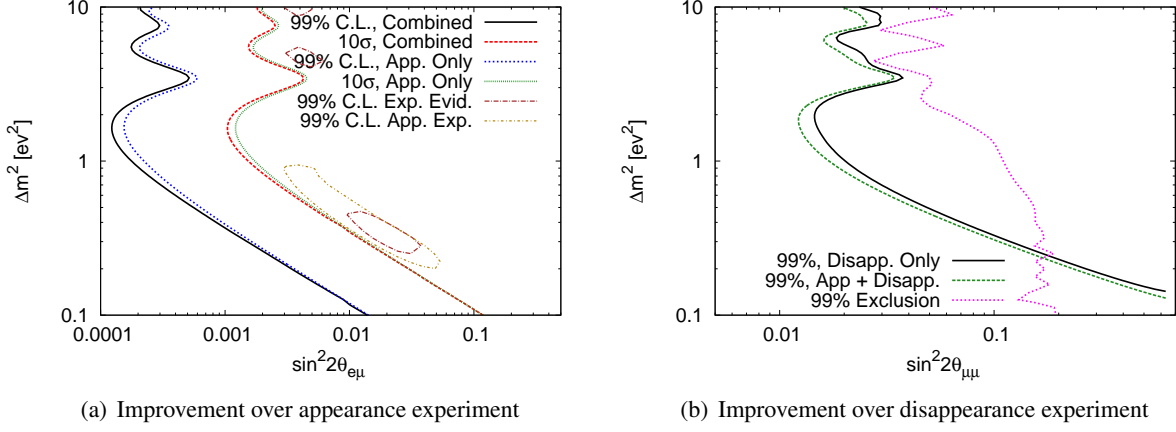


Figure 110: The sensitivity of a combined fit between ν_μ appearance experiment and a $\bar{\nu}_\mu$ disappearance experiment at nuSTORM. Contour generated using GLoBES, assuming a 1.3 kTon far detector, 2 km away from the muon storage ring, exposed to neutrinos resulting from an exposure of 1.6×10^{18} useful muon decays. A 1% signal and 10% background systematic uncertainty is assumed.

8.5 ν_e preliminaries

8.5.1 Shower reconstruction motivation

In addition to the muon appearance-disappearance channels, the flavor content of the nuSTORM beam provides an option to investigate ν_e channels. ν_e appearance from the muon decay would prove challenging given the lack of charge identification available in SuperBIND for events likely to shower, but a ν_e disappearance channel is approachable. The CC-NC distinction required for these types of events could also provide an option to study NC disappearance, which would supply an especially powerful indicator for sterile neutrinos.

8.5.1.1 Electron shower reconstruction

The primary requirement placed upon the reconstruction for a ν_e analysis is the ability to identify the electron from the charged current interaction. In SuperBIND, the electron will quickly shower generating an event topology similar to that of neutral current interactions. Distinguishing between the electromagnetic shower from the ν_e CC and all other hadronic showers (both residually from the CC interactions through resonance, deep inelastic scattering etc., and all NC interactions) becomes the foremost concern. Examples of CC and NC event types for ν_e events in SuperBIND can be seen in Fig. 111.

8.5.1.2 Direction estimation

The direction of the shower is estimated by taking the charge-weighted mean position of each plane and fitting with a straight line. In cases with little hadronic interaction this method is a reasonable approximation of the electron direction. However, any hadronic showers can interfere with the estimation of the electromagnetic shower direction, making this estimation poor. Where it is assumed the majority of the energy

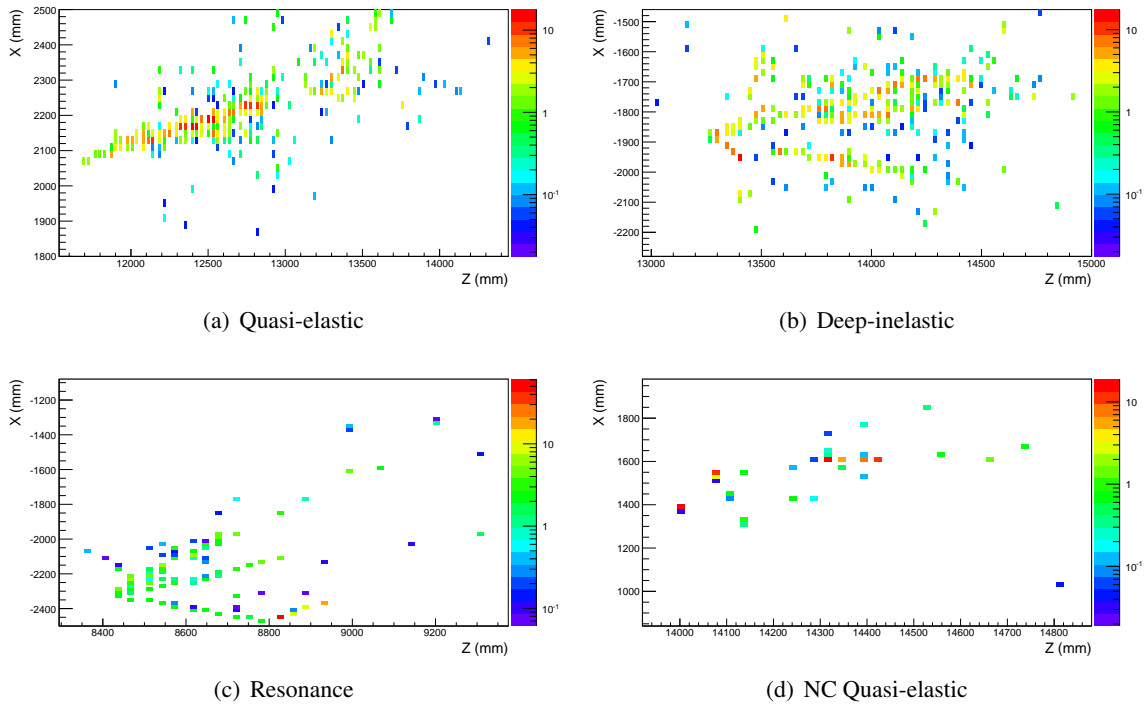


Figure 111: ν_e CC interaction examples in SuperBIND. The deposited energy in MeV is shown on the z-axis.

will be deposited within one Moliere radius, a deviation in the true shower direction of more than one radius prohibits current identification using the following method.

8.5.1.3 Current prediction

By comparing the fraction of energy deposited in the central region of the shower, it is likely some distinction between the NC and CC events can be achieved. As it is expected that 90% of the energy from an electro-magnetic shower should be contained within one Moliere radius, the volume which contains a majority of the energy deposited in the scintillator (here we have used 50%) can be utilized as a figure of merit. The density of this region, which adds the further discrimination power of total energy deposited in the scintillator, can be seen in Fig. 112. There are issues associated with successfully constraining this region, as the direction of the shower (which might need to be distinguished from multiple showers) can be difficult to reconstruct, and so is not included here. Therefore, the efficiency of this method is not currently optimal and is undergoing additional work. In any case, this shows some of the discrimination power available from a purely sampling approach in SuperBIND.

It is expected that the shower density and other variables will be used in a multi-variate approach. Additional methods are under consideration, including the Library Event Matching employed by MINOS.

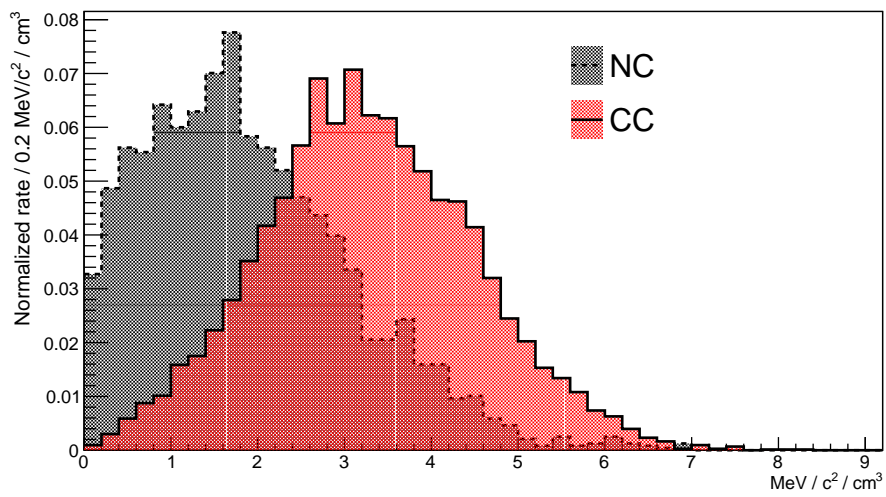


Figure 112: Density of energy deposited in the scintillator for the total volume in which 50% of the energy was found for ν_e CC and NC events.

8.6 Neutrino Interaction Study

The requirements of the neutrino-nucleus-scattering program at the nuSTORM facility were described in Section 3.2.1. Two studies have been carried out to demonstrate the potential of nuSTORM. A review of the systematic uncertainties that could be achieved at nuSTORM is compared with the precision of a selection of present and proposed experiments at conventional neutrino beams (section 8.6.1). A straw-man detector based on the MicroBooNE liquid-argon time-projection-chamber is introduced in section 8.6.2 and used to evaluate the precision with which the charged-current quasi-elastic cross section could be determined at the nuSTORM facility. The results of the studies indicate that nuSTORM will be able to provide definitive measurements of neutrino-nucleus scattering.

8.6.1 Review of systematic uncertainties in neutrino-nucleus scattering studies

The status of the data on neutrino-nucleus (νN) scattering was reviewed in Section 3.2.1 together with a discussion of the factors limiting the accuracy of the present generation of experiments. νN scattering cross sections have been determined for incident neutrino energies in the few-GeV range [237–243]. A summary of the systematic uncertainties affecting these measurements is presented in Table 28. The flux uncertainties range from $\sim 7\%$ to 20% ; in each case, the flux uncertainty makes a substantial contribution to the total systematic error while in a number of cases the flux uncertainty is the dominant source of systematic uncertainty.

At the nuSTORM facility, the flavor-composition of the neutrino beam will be known and the flux will be determined with a precision of 1% using the storage-ring instrumentation (see section 4). Inspection of Table 28 indicates that, to make best use of the excellent knowledge of the neutrino flux, a detector capable of delivering measurements at the $\%$ level will be required. The HiResM ν detector [244] would be a suitable choice. Table 29 lists the design parameters of the HiResM ν detector. The performance of such a detector exposed to the nuSTORM flux is illustrated in Fig. 113 where the charged-current quasi-elastic (CCQE) cross section is plotted as a function of neutrino energy E_ν . The figure shows the precision with which the cross section would be measured if the systematic uncertainties estimated for the HiResM ν detector are combined with the 1% flux uncertainty that nuSTORM will provide. For comparison, the performance of HiResM ν combined with a flux uncertainty of 10% is shown. Fig. 113 also shows the present measurements of the CCQE cross section; these measurements are only available for muon-neutrino (and muon-anti-neutrino) beams. The figure shows that nuSTORM has the potential to improve the systematic uncertainty on muon-neutrino (muon-anti-neutrino) CCQE cross section measurements by a factor of $\sim 5 - 6$. The electron-neutrino- (electron-anti-neutrino-) nucleus cross section measurements that can be made with nuSTORM will be a unique contribution.

8.6.2 The potential of nuSTORM: a straw-man detector

The MicroBooNE detector, an unmagnetized liquid-argon (LAr) time-projection-chamber (TPC) with a mass of 170 T [254] was used as the basis for the straw-man detector. The LArSoft package [255] was used to simulate $\bar{\nu}_\mu$ and ν_e events and the event samples were combined to simulate the flux that will be delivered by nuSTORM with a stored μ^+ beam. Studies of the performance of LAr TPCs have demonstrated

Table 28: Sources of systematic uncertainties for different experiments [237–240, 242, 243]. The column headed “Experiment” reports the experiment and the channel (neutral-current elastic, NCE; charged-current quasi-elastic, CCQE; charged-current single π^0 production $CC\pi^0$; quasi-elastic, QE; and charged-current, CC). The incident neutrino flavor is also indicated. The systematic uncertainties are classified as uncertainties related to: the performance of the detector (column headed “Detector”); the Monte Carlo simulation of the experiment (“Monte Carlo”) and “Other”. The column headed “Sub-total” reports the combination of these uncertainties combined in quadrature. The flux uncertainty is reported in the column headed “Flux” and the total systematic error in the column headed “Total”.

Experiment	Systematic uncertainty (%)					
	Detector	Monte Carlo	Other	Sub-total	Flux	Total
MiniBooNE NCE ($E_\nu \sim 1$ GeV)	15.6	6.4		16.9	6.7	18.1
MiniBooNE CCQE ν_μ ($E_\nu \in 0.2 - 3.0$ GeV)	3.2	15.7		16.1	6.9	17.5
MiniBooNE CCQE ν_e ($E_\nu \in 0.2 - 3.0$ GeV)	14.6	8.5		16.1	9.8	19.5
MiniBooNE CC π^0 ν_μ ($E_\nu \in 0.5 - 2.0$ GeV)	5.8	14.4		15.6	10.5	18.7
MiniBooNE QE $\frac{d^2\sigma}{dT_\mu d\cos\theta_\mu}$ ($E_\nu \in 0.5 - 2.0$ GeV)	4.6	4.4		6.4	8.7	10.7
T2K Inclusive ν_μ CC ($E_\nu \sim 1$ GeV)	0.7–12	0.4–9		1.3–15	10.9	10.9–18.6
Minerva $\bar{\nu}_\mu$ CCQE ($Q^2 < 1.2$ GeV ²)	8.9–15.6	2.8	2–6	9.6–17	12	15.3–20.8
LSND $\bar{\nu}_\mu p \rightarrow \mu^+ n$ 0.1GeV	5	12		13	15	20

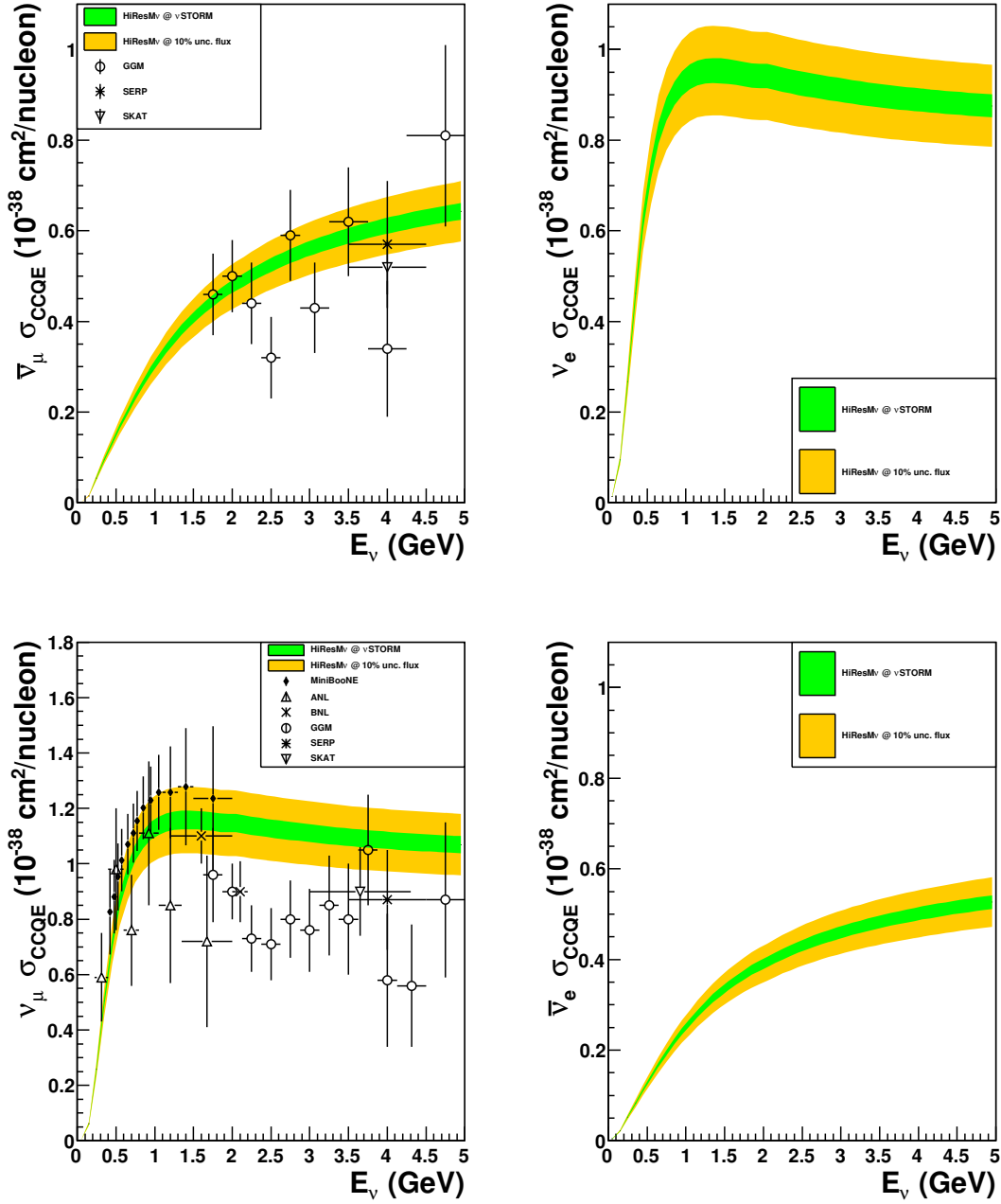


Figure 113: The CCQE cross section (σ_{CCQE}) plotted as a function of incident neutrino energy (E_ν). The cross sections that would be obtained with stored μ^+ beams are shown in the top row; the $\bar{\nu}_\mu$ CCQE cross section is shown in the top left panel while the ν_e CCQE cross section is shown in the top right panel. The cross sections that would be obtained with stored μ^- beams are shown in the bottom row; ν_μ CCQE cross section in the bottom left panel, ν_e CCQE cross section in the bottom right panel. The width of the colored bands represent the systematic uncertainty on the cross sections determined using the HiResM ν detector at the nuSTORM facility (see text for details). The green band shows the detector uncertainties combined with the 1% uncertainty on the neutrino flux at nuSTORM. The yellow band shows the detector uncertainties combined with a flux uncertainty of 10%. Measurements made by the MiniBoNE (\blacklozenge), ANL (\triangle), BNL (\times), Gargamelle (\circ), SERP ($*$) and SKAT (∇) collaborations are also shown [240, 246–252]. The data can be found at [253].

Table 29: In order to take maximal advantage of the nuSTORM accurate beam the detector errors need to be kept small. The HiresM ν small uncertainties [245] make it a suitable detector for this effect. The "Reconstruction" error refers to the track reconstruction error. It is dominated by the proton-reconstruction in the QE event. The "Background" estimate corresponds to the contamination of resonant and DIS events. Finally, the "FSI error" estimation corresponds to the impact of final state interactions on the topology of the measured tracks.

Detector	Types of Errors	Contribution (%)
HiResM ν	Reconstruction	0.8
	Background	2.1
	FSI error	1.5
	Total	2.9

Table 30: Parameters assumed in the LArSoft simulation implemented for this analysis.

Effect	Value
Momentum resolution of contained tracks	3%
Angular resolution	3%
Minimum range for track finding	2 cm

high spatial resolution [256] and excellent energy resolution [257]. The combination of particle range measurements with specific energy loss (dE/dx) allows efficient particle discrimination. The efficiencies and resolutions used in the LArSoft simulation are summarized in Table 30. Neutrino interactions were simulated within a LAr TPC enclosing a volume of $256.35 \times 233 \times 1036.8 \text{ cm}^3$. The software used to simulate the neutrino interactions was LArSoft. LArSoft uses the GENIE neutrino interaction generator [258] to produce interactions in the liquid argon volume, and stores the final-state particles for further simulation. Particles were passed to Geant4 to be tracked through the detector. Events were generated for incident neutrino energies uniformly distributed between 0.5 GeV and 4 GeV, reweighted to the nuSTORM flux and scaled to the number of interactions expected for an exposure of 10^{21} POT on a 100 T fiducial mass at a distance of 50 m from the end of the straight section (see section 3.2.1). Fig. 114 and Fig. 115 show typical CCQE in the muon and electron channels in the MicroBooNE detector. For this analysis, the parameters listed in Table 30 were used in the LArSoft package. Muon-neutrino induced CCQE events were selected by requiring a muon candidate unaccompanied by proton or pion candidates. Electron-neutrino induced CCQE events were selected by requiring a single-electron candidate accompanied by at most one proton candidate and unaccompanied by a pion candidate. The events-selection criteria are summarized in table 31.

In practice, the simple CCQE-like selection based on track finding will also select events in which any number of hadrons are produced which deposit less than ~ 40 MeV in the detector. Fig. 116 shows the cross sections for the production of CCQE-like events using the criteria described above. The event sample that can be accumulated using a detector with a fiducial mass of 100 T at nuSTORM is large enough that the statistical uncertainty is significant only in the lowest E_ν bin (~ 0.5 GeV) and becomes negligible at higher energies. The flux uncertainty of 1% also makes a relatively small contribution, leaving the detector system-

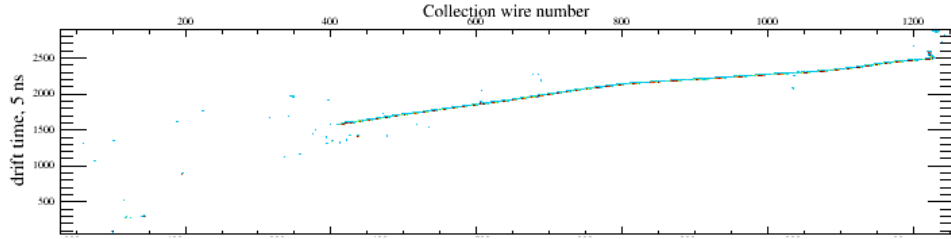


Figure 114: Example of a $\bar{\nu}_\mu$ CCQE interaction. The track in this event display belongs to a 0.9 GeV μ^+ .

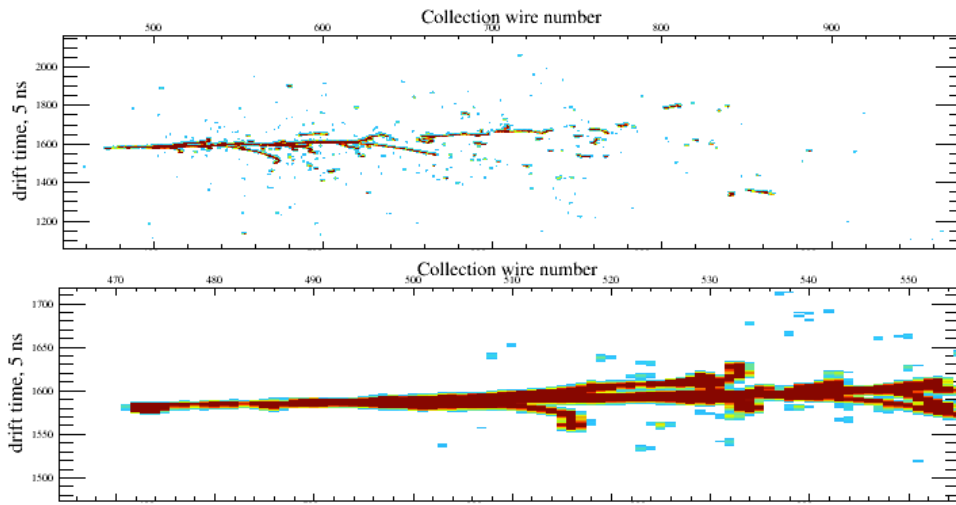


Figure 115: Selection criteria for the analysis. The CCQE-like events are defined as containing one lepton and strictly no pions. Combining this with data in Table 30, one can expect an efficiency loss for leptons with small momentum/short range. The resulting CCQE-like event count will include topologies where any given number of neutrons, and protons with less than 40 MeV are present.

Table 31: Selection criteria for the analysis. The CCQE-like events are defined as containing one lepton and no pions. Single electron candidates where the companion proton is not found are also accepted.

Interaction Category	Required Topology
$\bar{\nu}_\mu$ CCQE _{LIKE}	1 μ^+ + 0proton + 0pion
ν_e CCQE _{LIKE}	1 e^- + 0/1 proton + 0pion

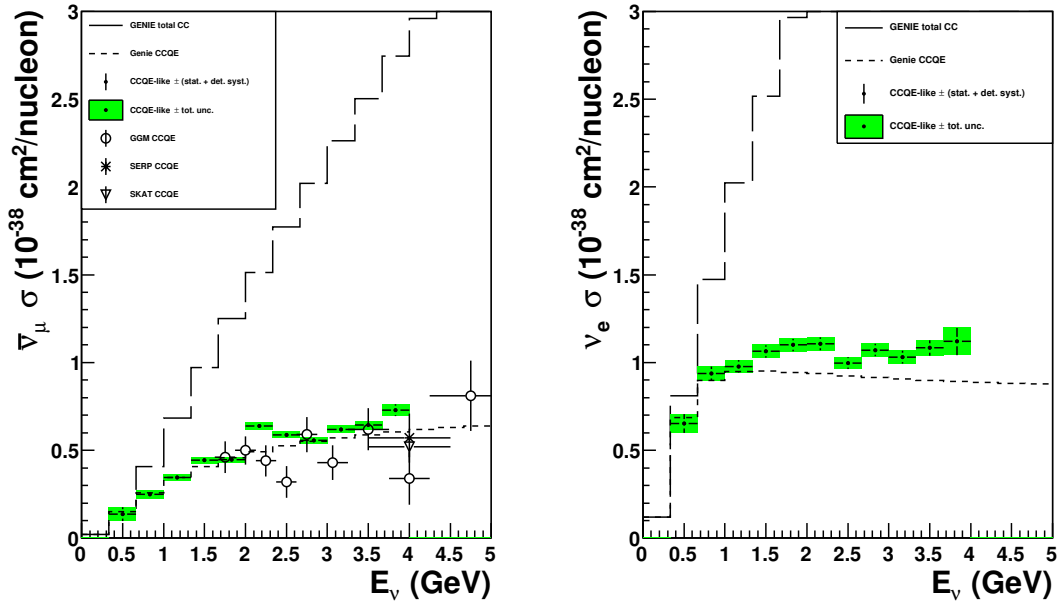


Figure 116: $\bar{\nu}_\mu$ and ν_e CCQE-like cross sections obtained using the straw-man detector analysis described in the text. The uncertainties include statistical, detector systematic (3%) uncertainties and the 1% nuSTORM flux uncertainty. The dashed lines show GENIE's total CC and Quasi-Elastic cross sections for comparison. Measurements made by the Gargamelle (\circ), SERP ($*$) and SKAT (\times) collaborations are also shown.

atic as the dominant source of uncertainty. In the muon channel, nuSTORM offers a six-fold improvement in the precision with which the CCQE cross sections can be measured. In the electron channel the measurements that nuSTORM will provide will be unique. The extension of this analysis to other channels will be the subject of future work.

9 Outlook and conclusions

In this proposal we have presented a compelling case for the nuSTORM facility. As mentioned in the introduction, nuSTORM’s motivation rests on three central themes: 1. A search for sterile neutrinos for unprecedented precision, 2. Unique opportunities in ν interaction physics and 3. Presents a powerful technology test bed for muon accelerator physics. With respect to search for sterile neutrinos, nuSTORM present the only facility that can do all of the following:

- Make a direct test of the LSND and MiniBooNE anomalies.
- Provide stringent constraints for both ν_e and ν_μ disappearance to over constrain $3 + N$ oscillation models and to test the Gallium and reactor anomalies directly.
- Test the CP- and T-conjugated channels as well, in order to obtain the relevant clues for the underlying physics model, such as CP violation in $3 + 2$ models.

With respect to ν interaction physics, nuSTORM presents the first opportunity to measure both ν_e and ν_μ cross sections at the the 1% level with a ν beam that can be characterized 5 to 10 times more precisely than conventional ν beams.

Lastly, with respect to accelerator R&D, nuSTORM can provide muon beams suitable for the next generation of studies into muon ionization cooling which are so crucial to the viability of any $\mu^+\mu^-$ collider. This can be done simultaneously while carrying out its neutrino physics program.

9.1 Moving forward

We are requesting Stage-1 approval for nuSTORM. Stage-1 approval will allow us to strengthen our collaboration and will, in particular, provide a strong foundation for our non-US collaborators to obtain support from their funding authorities to help prepare the next step for nuSTORM – the preparation of a Conceptual Design Report. Proton beams capable of serving the ν STORM facility can also be provided at CERN and with that realization, an Expression of Interest on nuSTORM has been submitted to the CERN SPSC Committee. It will come up for discussion at the next open meeting of the SPSC on June 25th of this year. The EOI to CERN has requested resources to:

- Investigate in detail how ν STORM could be implemented at CERN; and
- Develop options for decisive European contributions to the ν STORM facility and experimental program wherever the facility is sited.

The EoI defines a roughly two-year program which culminates in the delivery of a Technical Design Report which corresponds to the level of detail found in Conceptual Design Reports as produced during the DOE CD process.

With support potentially from both the Fermilab PAC and the CERN SPSC, nuSTORM can proceed within a decidedly “international-framework” with renewed vigor. This is a rare, but not unique situation, and would allow the collaboration to make significant progress refining the scientific and technical cases for nuSTORM while at the same time performing an overall optimization of the facility and its cost. This is truly a case where “The whole is greater than the sum of its parts [259]”.

9.2 Support request

Table 32 lists the support we require over the next 12-18 months in order to make further progress on the work needed to be accomplished for the CDR. S: Scientist, E: Engineer, D: Designer/drafter

Table 32: Support request

Task	Division	Effort type	FTE
π production simulations	APC	S	0.15
Inconel target studies	AD	E	1.0
Proton beamline optimization	AD	S/E	0.3
Decay ring lattice studies	AD	S	0.3
Kicker design	AD	E	0.2
Magnet design	TD	S/E/D	1.0
Decay ring instrumentation design	AD	E	0.5

A Long-Baseline Considerations

A multitude of experiments have been proposed in order to observe CP violation in the leptonic sector and determine the neutrino mass hierarchy (MH), see for instance [260]. In the U.S. context, the long baseline neutrino experiment (LBNE) is being pursued. The present design consists of a 700 kW conventional neutrino beam aimed at a 10 kt liquid argon (LAr) detector placed at $L = 1300$ km from the source [261]. Due to its long baseline and relatively large matter effects, LBNE would be able to determine the MH at 3σ for 75% of the parameter space. Its ability to measure the CP phase precisely and/or to discover CP violation is, however, limited due to a lack of statistics.

Measurement of the CP phase to a similar precision to that achieved in the quark sector is only offered by a Neutrino Factory (NF) [168, 262]. In a NF, a highly collimated beam of muon neutrinos and electron antineutrinos is produced from muon decays in a storage ring with long straight sections [23]. The present NF design parameters [24] are 10^{21} useful muon decays per 10^7 seconds, aimed at a 100 kton magnetized iron detector (MIND) placed at 2000 km from the source, with a parent muon energy of 10 GeV. In order to form an intense muon beam for acceleration and storage, muon phase space cooling is required for this default configuration. In addition, the fact that the neutrinos in a NF are a tertiary beam implies significant proton driver intensities; in this case, a 4 MW proton beam plus its associated target station.

These technical challenges are to be contrasted with the advantages of a NF – there are no intrinsic backgrounds and the absolute neutrino flux can be determined to better than 1%. Furthermore, the presence of both muon and electron neutrinos in the beam allows for a measurement of all final flavor cross sections at the near detector. A detailed analysis of the impact of systematic uncertainties in neutrino oscillation experiments has been recently performed in [168], where the key systematics affecting the different types of facilities were identified. In particular, it was shown that the main sources of systematics affecting a NF are matter density uncertainties (see also [263]). One possibility to reduce the impact of the matter uncertainty would be to combine the results from the golden ($\nu_e \rightarrow \nu_\mu$) and the so-called platinum ($\nu_\mu \rightarrow \nu_e$) channels [264]. It is well-known that this combination of channels is very effective in solving degeneracies, particularly in the case of large θ_{13} where background levels are not so relevant. However, the platinum channel is inaccessible in a MIND, because it requires the identification of the lepton charge in electron neutrino (and anti-neutrino) charged current events.

In order to be able to access the platinum oscillation channels, a totally active-scintillator detector (TASD) or a Liquid Argon (LAr) detector would be needed. In this case, the big challenge would be the magnetization of the detector. At a NF it is mandatory to distinguish the sign of the charged lepton produced at the detector, in order to disentangle the appearance and disappearance signals. In [265] the feasibility of electron charge identification was studied in the context of a low energy NF for a TASD in a 0.5 T magnetic field using a so-called magnetic cavern. It soon was speculated that a magnetized LAr detector should be suitable as well [266–269]. Note, that the detectors most likely will have to be deep underground due to the large duty factor of stored particle beams in a NF.

In [270] the physics performance of a low luminosity (10^{20} useful muon decays per year), low energy neutrino factory, using a magnetized 10 kton LAr detector placed at 1300 km from the source, was studied. This choice of detector size and baseline is obviously inspired by LBNE: it allows the reuse of the LBNE facilities to the largest extent possible and thus makes this option considerably more efficient in terms of resource usage. These parameters correspond to an overall reduction in exposure by a factor of 100, and

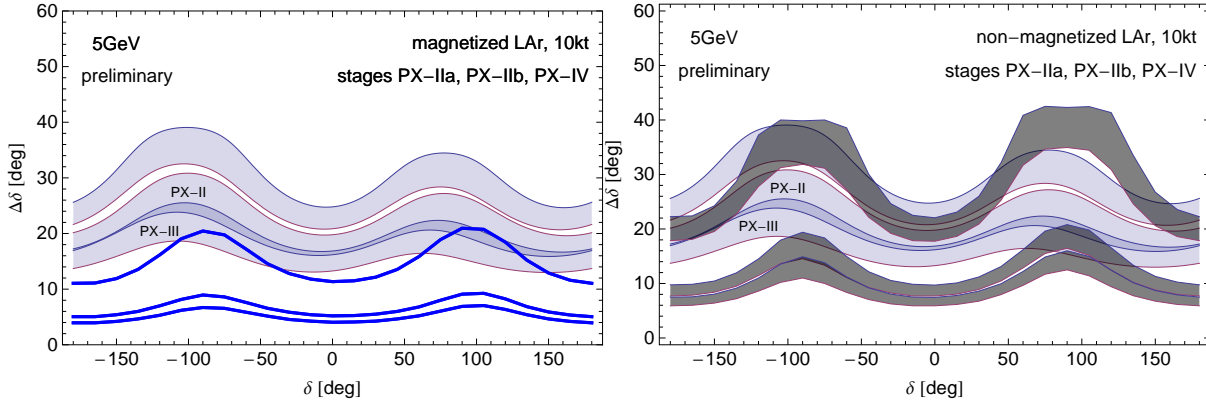


Figure 117: Expected precision for a measurement of δ at 1σ (1 d.o.f.) as a function of the true value of δ . Results are shown for the low luminosity, low energy neutrino factory (lines in the left panel, dark gray bands in the right panel) as well as for different exposures for LBNE (light bands). For LBNE the different bands correspond, from top to bottom, to 70, 110 and 230 $\text{MW}\times\text{kt}\times\text{yr}$. For the NF the different lines (bands) correspond, from top to bottom, to 1, 5.6 and 10×10^{20} useful muon decays per polarity and year, using a 10 kton LAr detector in all cases. The left panel shows the results when the detector is assumed to be magnetized; while the right panel shows the variation in the results when the charge identification efficiency is varied from 0.5 (upper edge of each band) to 0.9 (lower edge). See text for details.

would in principle allow the NF to be based on existing technology and already planned infrastructure. To give a specific example – consider phase II of Project X, where initially a 3 GeV proton beam with 1 MW of power will become available, which, according to studies performed within the Muon Accelerator Staging Study (MASS), without muon cooling could result in 10^{20} useful muon decays per year and polarity. This constitutes a reduction of luminosity by a factor 5 with respect to the default setup [24]. Then following [270] this permits the detector mass to be reduced from 100 kt to 10 kt. This is but one example of how to achieve this entry level luminosity. Obviously, as Project X matures, future proton beam facilities may have much more favorable parameters resulting in corresponding increases in luminosity. In an extended phase II of Project X, the beam power may increase to 3 MW and with the addition of cooling, 5.6×10^{20} useful muon decays can be achieved. Eventually, in phase IV, 4 MW at 8 GeV will become available, which will yield 10^{21} useful muon decays per year and polarity.

The results obtained in [270] for the precision attainable for a measurement of the CP violating phase δ are shown in the left panel of Fig. 117, at 1σ (1 d.o.f.). From top to bottom, the lines correspond to the results for a NF using 1.0, 5.6 and 10.0×10^{20} useful muon decays per polarity and year. The results are compared with the expected precision attainable at LBNE phase I ($0.7 \text{ MW}\times 10 \text{ kt}\times 10 \text{ yr.}$), at LBNE using a beam produced in the second stage of project X ($1.1 \text{ MW}\times 10 \text{ kt}\times 10 \text{ yr.}$) and at LBNE using the beam produced at the third stage of project X ($2.3 \text{ MW}\times 10 \text{ kt}\times 10 \text{ yr.}$). Since the performance of a magnetized LAr detector is indeed uncertain, in [270] the sensitivities using the performance parameters of a T ASD [265], were also presented. Even though more conservative signal and background rejection efficiencies were considered in this case, these only resulted in a slight reduction in performance with respect to the results using a LAr detector. The detector parameters are summarized in Table 1 in [270]. Systematic uncertainties have been implemented as in [168], using the default values for the systematic uncertainties listed in Table 2 therein. All correlations are taken into account, between different channels as well as between the near and far detectors. All simulations have been done using a modification of GLOBES [83, 84], and marginalization

over not-shown oscillation parameters was performed as explained in [168].

As already mentioned, one of the major technical challenges for this setup is the magnetization of a large volume LAr detector. However, even if magnetization would be the preferred option to achieve a very clean charge ID for muons and electrons, this may not be mandatory. It was already shown in [271] that, especially for large values of θ_{13} , a modest charge identification efficiency would yield good performance for a full luminosity low energy neutrino factory. Such efficiency may be attainable at a LAr non-magnetized detector combining different signatures that are different for neutrino and antineutrino events [271]: 1) in argon, the capture probability of a μ^- by an atom is about 76%, whereas this process cannot take place for μ^+ ; 2) the angular distribution of the outgoing lepton is different for ν and $\bar{\nu}$ events; 3) protons produced in QE ν events could in principle be tagged in argon. In [271] it was estimated that, combining these signatures, a charge identification efficiency between 50% and 90% could be achieved for a LAr detector. Under the same assumptions, the performance of a low luminosity low energy neutrino factory is presented in the right panel of Fig. 117, where the results are also compared to different phases of LBNE. From top to bottom, the dark gray bands show the performance for the setup described above, using the same useful muon decays as in the left panel: 1.0, 5.6 and 10×10^{20} decays per polarity and year, from top to bottom. The width of the bands shows the variation in performance when the charge separation efficiency is increased from 0.5 (upper edges) to 0.9 (lower edges). The same charge separation efficiency is assumed for muons and electrons.

The results from [270] (summarized in Fig. 117) show that a NF with 10 times fewer useful muon decays and a 10 times smaller detector mass with respect to the baseline NF scenario, would still outperform realistic super-beam setups like LBNE. This setup stands as a viable upgrade path for the nuSTORM facility, since this low luminosity can be achieved using existing proton drivers at Fermilab and without muon cooling. The reduced muon energy with respect to the NF baseline design makes it possible to use a baseline of around 1300 km, and the use of a magnetized LAr detector allows for full exploitation of the physics potential of the platinum channel, which is crucial for the overall performance of the facility. It has also been shown that, if magnetization is not viable, a modest charge separation would still allow for reasonable performance, comparable to that of LBNE. Finally, it should also be noted that, once a 4 MW lower energy proton beam becomes available from Project X, and if muon cooling is added and the detector mass is increased by a factor of 1-3, the performance of this facility would match or even exceed that of the baseline NF. Therefore, neither the initial energy of 5 GeV nor the baseline need to be changed at later stages.

B Magnetized Totally Active Detector

We have shown in Sec. 6 that a magnetized detector is required for nuSTORM if we wish to study the $\bar{\nu}_\mu^{(\pm)}$ oscillation appearance channels and that this naturally lead to the choice of magnetized iron technology. If one wanted to also look for $\bar{\nu}_e^{(\pm)}$ appearance, then magnetized totally active detector technology would be an appropriate alternative. Magnetic solutions for totally active detectors were studied within the International Scoping Study (ISS) [272] in the context of investigating how very large magnetic volumes could be produced at an acceptable cost. A liquid Argon (LAr) or a totally-active scintillator detector (TASD) could be placed inside such a volume giving a magnetized totally active detector. The following technologies were considered:

- Room Temperature Coils (Al or Cu)

- Conventional Superconducting Coils
- High Tc Superconducting Coils
- Low Temperature Non-Conventional Superconducting Coils

Within the ISS, much larger detector masses were considered than the 1 kT needed for nuSTORM. However, we can consider using one of the 10 large solenoids (each 15 m diameter \times 15 m long) studied in the ISS for use with a 1 kT LAr detector. The ISS concept of a “magnetic cavern” is shown in Fig. 118.

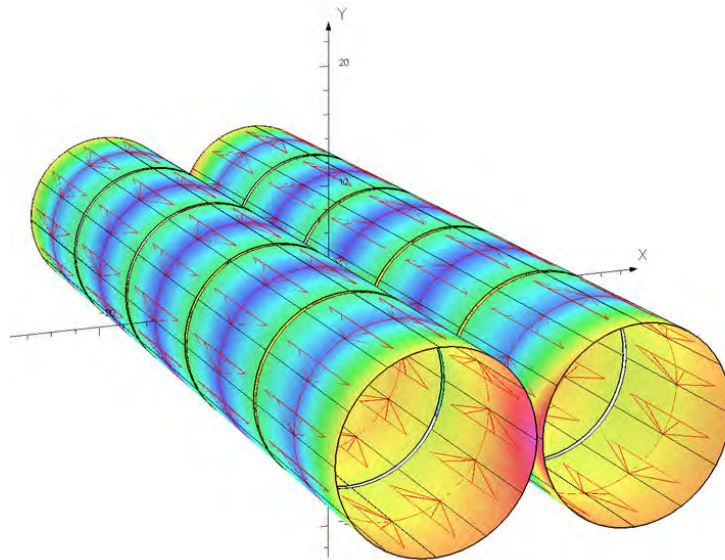


Figure 118: Magnetic Cavern Configuration

B.1 Conventional Room Temperature Magnets

In order to get adequate field strength with tolerable power dissipation, conventional room-temperature coils would have to be relatively thick. We first considered coils of Al conductor operating at 150 K. We then determined the amount of conductor necessary to produce a reference field of only 0.1 T. In order to keep the current density at approximately $100\text{A}/\text{cm}^2$, 10 layers of 1 cm^2 Al conductor would be required for our 15 m diameter \times 15 m long reference solenoid. Using a $\$20/\text{kg}$ cost for convention magnets [273], the estimated cost for 1 solenoid is $\$5\text{M}$. The power dissipation (assuming $R=1 \times 10^{-8}\text{ Ohm}\cdot\text{m}$) is approximately 1 MW. The operating costs for 1 MW of power would be $\$1.5\text{M}/\text{year}$ (based on typical US power costs). The cost of the magnet system including 10 years of operation is then $\$20\text{M}$. If one includes the cost of cooling the coils to 150 K, the costs increase substantially. Studies have shown [273] that there is little cost benefit to operating non-superconducting (Al or Cu) coils at low temperature vs. room temperature. If we consider that the power dissipation at room temperature for Al coils triples (vs. 150 K operation), then the total magnet cost increases to $\$50\text{M}$.

B.2 Conventional Superconducting Coils

Conventional superconducting solenoids are certainly an option for providing the large magnetic volumes that are needed. Indeed coils of the size we are considering were engineered (but never built) for the proposed GEM experiment at the SSC. A cylindrical geometry (solenoid) does imply that a fraction of the magnetic volume will be outside the volume of the active detector, which will likely be rectangular in cross section. This is certainly a disadvantage in terms of efficient use of the magnetic volume, but would provide personnel access paths to detector components inside the magnetic cavern. It is certainly possible to consider solenoids of rectangular cross section, and thus make more efficient use of the magnetic volume, but the engineering and manufacturing implications of this type of design have not been evaluated.

Technically, superconducting magnets of this size could be built, but the cost is not well known. There have been a number of approaches to estimating the cost of a superconducting magnet and we will mention two of those here. The first comes from Green and St. Lorant [274]. They considered all the magnets that had been built at the time of their study (1993) and developed two formulas for extrapolating the cost of a superconducting magnet: one scaling by stored energy and one scaling by magnetic volume times field. They are given below:

$$C = 0.5(E_s)^{0.662} \quad (10)$$

and

$$C = 0.4(BV)^{0.635} \quad (11)$$

where E_s is the stored energy in MJ, B is the field in Tesla, V is the volume in m^3 and C is the cost in M\$. The formulas given above give a cost for each 15 m diameter \times 15 m long, 0.5T magnet of approximately \$20M (based on E_s) and \$38M (based on magnetic volume). As another reference point, we used the CMS coil [275] (B=4T, V=340 m^3 , Stored energy = 2.7 GJ, "As built cost" = \$55M). The Green and St. Lorant formulas give costs for the CMS magnet of \$93M and \$41M based on stored energy and magnetic volume, respectively. From these data we can make "Most Optimistic" and "Most Pessimistic" cost extrapolations for our baseline NF solenoid. The most optimistic cost comes from using the formula, based on stored energy and assume that it over-estimates by a factor of 1.7 (93/55), based on the CMS as built cost. This gives a cost of \$14M for each of our NF detector solenoids. The most pessimistic cost extrapolation comes from using the formula based on magnetic volume and conclude that it under-estimates the cost by a factor of 1.3 (55/41), based on the CMS as built cost. This then gives a cost of \$60M for each of our NF detector solenoids. There is obviously a large uncertainty represented here.

Another extrapolation model was used by Balbekov *et al.* [276] based on a model developed by A. Herve. The extrapolation formulae are given below:

$$P_0 = 0.33S^{0.8} \quad (12)$$

$$P_E = 0.17E^{0.7} \quad (13)$$

and

$$P = P_0 + P_E \quad (14)$$

where P_0 is the price of the equivalent zero-energy magnet in MCHF, P_E is the price of magnetization, and P is the total price. S is the surface area (m^2) of the cryostat and E (MJ) is the stored energy. This model

includes the cost of power supplies, cryogenics and vacuum plant. From the above equations you can see that the model does take into account the difficulties in dealing with size separately from magnetic field issues. Balbekov et. al. used three “as-builts” to derive the coefficients in the above equations:

- ALEPH (R=2.65m, L=7m, B=1.5T, E=138MJ, P=\$14M)
- CMS (R=3.2m, L=14.5m, B=4T, E=3GJ, P=\$55M)
- GEM (R=9m, L=27m, B=0.8T, E=2GJ, P=\$98M)

The GEM magnet cost was an estimate based on a detailed design and engineering analysis. Using this estimating model, we have for one of the NF detector solenoids: $P_0 = 0.33(707)^{0.8} = 63\text{MCHF}$, $P_E = 0.17(265)^{0.7} = 8.5\text{MCHF}$. The magnet cost is thus approximately \$57M (which is close to our most pessimistic extrapolation given above). One thing that stands out is that the magnetization costs are small compared to the total cost. The mechanical costs involved with dealing with the large vacuum loading forces on the vacuum cryostat assumed to be used for this magnet are by far the dominant cost.

B.3 Low Temperature Non-Conventional Superconducting Coils

In this concept we solve the vacuum loading problem of the cryostat by using the superconducting transmission line (STL) that was developed for the Very Large Hadron Collider superferic magnets [207]. The solenoid windings now consist of this superconducting cable which is confined in its own cryostat. Each solenoid consists of 150 turns and requires 7500 m of cable. There is no large vacuum vessel and access to the detectors can be made through the winding support cylinder, since the STL does not need to be close-packed in order to reach an acceptable field. We have performed a simulation of the Magnetic Cavern concept using STL solenoids and the results are shown in Fig. 119. With the iron end-walls (1 m thick), the average field in the xz plane is approximately

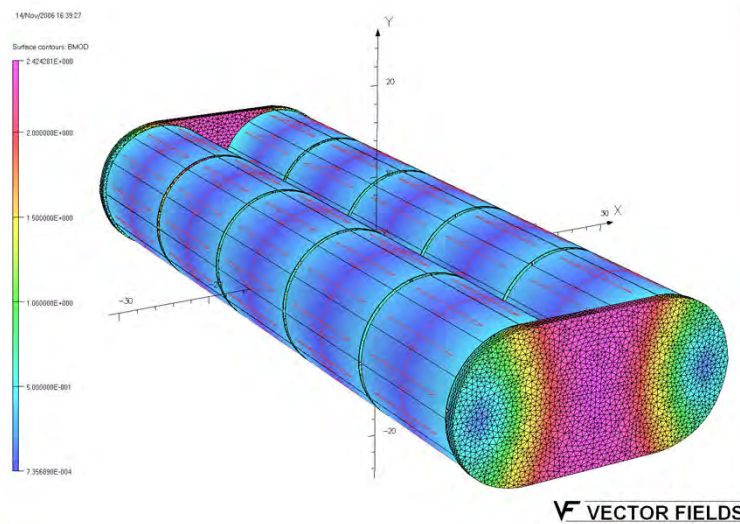


Figure 119: STL Solenoid Magnetic Cavern Simulation

0.58 T at an excitation current of 50 kA. The maximum radial force is approximately 16 kN/m and the maximum axial force approximately 40 kN/m. The field uniformity is quite good with the iron end-walls and is shown in Fig. 120.

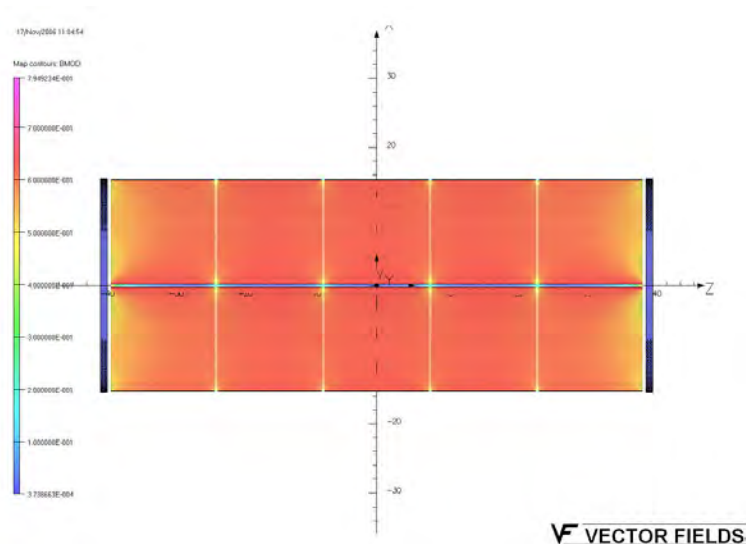


Figure 120: STL Solenoid Magnetic Cavern Field Uniformity in XZ plane

B.4 Superconducting Transmission Line

The superconducting transmission line (STL) consists of a superconducting cable inside a cryopipe cooled by supercritical liquid helium at 4.5-6.0 K placed inside a co-axial cryostat. It consists of a perforated Invar tube, a copper stabilized superconducting cable, an Invar helium pipe, the cold pipe support system, a thermal shield covered by multilayer super-insulation, and the vacuum shell. One of the possible STL designs developed for the VLHC is shown in Fig. 121.

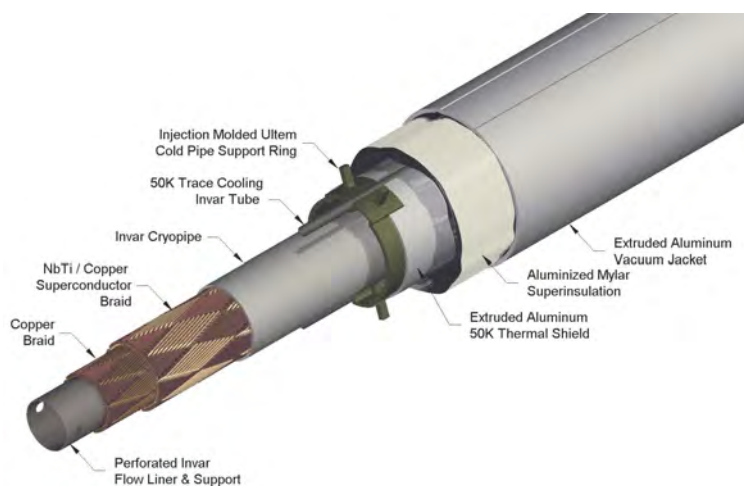


Figure 121: Superconducting transmission line

The STL is designed to carry a current of 100 kA at 6.5 K in a magnetic field up to 1 T. This provides a 50% current margin with respect to the required current in order to reach a field of 0.5T. This operating margin can compensate for temperature variations, mechanical or other perturbations in the system. The superconductor for the STL could be made in the form of braid or in the form of a two-layer spiral winding using Rutherford cable. The braid consists of 288 NbTi SSC-type strands 0.648 mm in diameter and arranged in a pattern of two sets of 24 crossing bundles with opposite pitch angle about the tube. A conductor made of Rutherford

cables consists of 9 NbTi cables that were used in the SSC dipole inner layer. A copper braid is placed inside the superconductor to provide additional current carrying capability during a quench. The conductor is sandwiched between an inner perforated Invar pipe, which serves as a liquid helium channel, and an outer Invar pressure pipe that closes the helium space. Both braided and spiral-wrapped conductors and the 10 cm long splice between them have been successfully tested with 100 kA transport current within the R&D program for the VLHC. The STL has a 2.5-cm clear bore which is sufficient for the liquid helium flow in a loop up to 10 km in length. This configuration allows for cooling each solenoid with continuous helium flow coming from a helium distribution box.

The thermal shield is made of extruded aluminum pipe segments, which slide over opposite ends of each support spider. The 6.4-mm diameter Invar pipe is used for 50 K pressurized helium. It is placed in the cavities at the top and the bottom of both the shield and the supports. The shield is wrapped with 40 layers of a dimpled super insulation. The vacuum shell is made of extruded aluminum or stainless steel. Heat load estimates for the described STL are:

- Support system: 53 mW/m at 4.5 K and 670 mW/m at 40 K
- Super insulation: 15 mW/m at 4.5 K and 864 mW/m at 40K

The estimated cost of the described STL is approximately \$500/m. Further STL design optimization will be required to adjust the structure to the fabrication and operating conditions of the desired detector solenoids and to optimize its fabrication and operational cost.

B.5 Conclusions

Magnetizing volumes large enough to contain upwards of 1kT of LAr or totally active scintillator at fields up to 0.5T with the use of the STL concept would appear to be possible, but would require dedicated R&D to extend the STL developed for the VLHC to this application. It eliminates the cost driver of large conventional superconducting coils, the vacuum-insulated cryostat, and has already been prototyped, tested, and costed during the R&D for the VLHC. A full engineering design would still need to be done, but this technique has the potential to deliver the large magnetic volume required with a field as high as 1T, with very uniform field quality and at an acceptable cost.

References

- [1] P. Kyberd et al. (nuSTORM Collaboration) (2012), 1206.0294.
- [2] A. Aguilar et al. (LSND) (????).
- [3] A. A. Aguilar-Arevalo et al. (MiniBooNE), Phys. Rev. Lett. **98**, 231801 (2007), 0704.1500.
- [4] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev.Lett. **105**, 181801 (2010), 1007.1150.
- [5] T. Mueller, D. Lhuillier, M. Fallot, A. Letourneau, S. Cormon, et al., Phys.Rev. **C83**, 054615 (2011), 1101.2663.
- [6] P. Huber, Phys.Rev. **C84**, 024617 (2011), 1106.0687.
- [7] G. Mention, M. Fechner, T. Lasserre, T. Mueller, D. Lhuillier, et al., Phys.Rev. **D83**, 073006 (2011), 1101.2755.
- [8] P. Anselmann et al. (GALLEX Collaboration.), Phys.Lett. **B342**, 440 (1995).
- [9] W. Hampel et al. (GALLEX Collaboration), Phys.Lett. **B420**, 114 (1998).
- [10] J. Abdurashitov, V. Gavrin, S. Girin, V. Gorbachev, T. V. Ibragimova, et al., Phys.Rev.Lett. **77**, 4708 (1996).
- [11] J. Abdurashitov et al. (SAGE Collaboration), Phys.Rev. **C59**, 2246 (1999), hep-ph/9803418.
- [12] J. Abdurashitov, V. Gavrin, S. Girin, V. Gorbachev, P. Gurkina, et al. (SAGE Collaboration), Phys.Rev. **C73**, 045805 (2006), nucl-ex/0512041.
- [13] K. Abazajian, M. Acero, S. Agarwalla, A. Aguilar-Arevalo, C. Albright, et al. (2012), 1204.5379.
- [14] F. An et al. (DAYA-BAY Collaboration), Phys.Rev.Lett. **108**, 171803 (2012), 1203.1669.
- [15] J. Ahn et al. (RENO collaboration), Phys.Rev.Lett. **108**, 191802 (2012), 1204.0626.
- [16] Y. Abe et al. (DOUBLE-CHOOZ Collaboration), Phys.Rev.Lett. **108**, 131801 (2012), 1112.6353.
- [17] K. Abe et al. (T2K Collaboration), Phys.Rev.Lett. **107**, 041801 (2011), 1106.2822.
- [18] P. Adamson et al. (MINOS Collaboration), Phys.Rev.Lett. **107**, 181802 (2011), 1108.0015.
- [19] D. G. Koshkarev (1974), CERN/ISR-DI/74-62.
- [20] D. Neuffer, *Design Considerations for a Muon Storage Ring* (1980), Telmark Conference on Neutrino Mass, Barger and Cline eds., Telmark, Wisconsin.
- [21] W. Winter, Phys.Rev. **D85**, 113005 (2012), 1204.2671.
- [22] H. University, *Cambridge Electron Accelerator (Cambridge, Mass.) Records of the Cambridge Electron Accelerator : an inventory* (2006), Records of the Cambridge Electron Accelerator, 1952-1974; <http://oasis.lib.harvard.edu/oasis/deliver/hua11001> .

- [23] S. Geer, Phys.Rev. **D57**, 6989 (1998), hep-ph/9712290.
- [24] S. Choubey et al. (The IDS-NF collaboration) (2011), 1112.2853.
- [25] A. Kusenko, F. Takahashi, and T. T. Yanagida, Phys.Lett. **B693**, 144 (2010), 1006.1731.
- [26] R. Mohapatra, Phys.Rev. **D64**, 091301 (2001), hep-ph/0107264.
- [27] C. Froggatt and H. B. Nielsen, Nucl.Phys. **B147**, 277 (1979).
- [28] J. Barry, W. Rodejohann, and H. Zhang, JCAP **1201**, 052 (2012), 37 pages, 1 figure/ v2: additional NLO operators considered, references added, matches version published in JCAP, 1110.6382.
- [29] R. Mohapatra, S. Nasri, and H.-B. Yu, Phys.Rev. **D72**, 033007 (2005), hep-ph/0505021.
- [30] C. S. Fong, R. N. Mohapatra, and I. Sung, Phys.Lett. **B704**, 171 (2011), 1107.4086.
- [31] H. Zhang, Phys.Lett. **B714**, 262 (2012), 1110.6838.
- [32] M. Bando and K. Yoshioka, Prog.Theor.Phys. **100**, 1239 (1998), hep-ph/9806400.
- [33] E. Ma, Phys.Lett. **B380**, 286 (1996), hep-ph/9507348.
- [34] Q. Shafi and Z. Tavartkiladze, Phys.Lett. **B451**, 129 (1999), hep-ph/9901243.
- [35] K. Babu and G. Seidl, Phys.Rev. **D70**, 113014 (2004), hep-ph/0405197.
- [36] Z. G. Berezhiani and R. N. Mohapatra, Phys.Rev. **D52**, 6607 (1995), hep-ph/9505385.
- [37] R. Foot and R. Volkas, Phys.Rev. **D52**, 6595 (1995), hep-ph/9505359.
- [38] V. Berezhinsky, M. Narayan, and F. Vissani, Nucl.Phys. **B658**, 254 (2003), hep-ph/0210204.
- [39] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration) (2012), 1207.4809.
- [40] K. Schreckenbach, G. Colvin, W. Gelletly, and F. Von Feilitzsch, Phys.Lett. **B160**, 325 (1985).
- [41] M. A. Acero, C. Giunti, and M. Laveder, Phys.Rev. **D78**, 073009 (2008), 0711.4222.
- [42] C. Giunti, M. Laveder, Y. Li, Q. Liu, and H. Long, Phys.Rev. **D86**, 113014 (2012), 1210.5715.
- [43] J. Kopp, M. Maltoni, and T. Schwetz, Phys.Rev.Lett. **107**, 091801 (2011), 1103.4570.
- [44] C. Giunti and M. Laveder, Phys.Lett. **B706**, 200 (2011), 1111.1069.
- [45] G. Karagiorgi (2011), 1110.3735.
- [46] C. Giunti and M. Laveder, Phys.Rev. **D84**, 093006 (2011), 1109.4033.
- [47] C. Giunti and M. Laveder, Phys.Rev. **D84**, 073008 (2011), 1107.1452.
- [48] M. Archidiacono, N. Fornengo, C. Giunti, S. Hannestad, and A. Melchiorri (2013), 1302.6720.
- [49] J. Kopp, P. A. N. Machado, M. Maltoni, and T. Schwetz (2013), 1303.3011.
- [50] B. Armbruster et al. (KARMEN), Phys. Rev. **D65**, 112001 (2002), hep-ex/0203021.

- [51] P. Astier et al. (NOMAD), Nucl. Phys. **B611**, 3 (2001), hep-ex/0106102.
- [52] L. Borodovsky, C. Chi, Y. Ho, N. Kondakis, W.-Y. Lee, et al., Phys.Rev.Lett. **68**, 274 (1992).
- [53] M. Antonello, B. Baibussinov, P. Benetti, E. Calligarich, N. Canci, et al. (2012), 1209.0122.
- [54] Y. Ashie et al. (Super-Kamiokande), Phys. Rev. **D71**, 112005 (2005), hep-ex/0501064.
- [55] B. T. Cleveland et al., Astrophys. J. **496**, 505 (1998).
- [56] F. Kaether, W. Hampel, G. Heusser, J. Kiko, and T. Kirsten, Phys.Lett. **B685**, 47 (2010), 1001.2731.
- [57] J. N. Abdurashitov et al. (SAGE), Phys. Rev. **C80**, 015807 (2009), 0901.2200.
- [58] J. Hosaka et al. (Super-Kamiokande), Phys. Rev. **D73**, 112001 (2006), hep-ex/0508053.
- [59] B. Aharmim et al. (SNO), Phys. Rev. **C75**, 045502 (2007), nucl-ex/0610020.
- [60] B. Aharmim et al. (SNO), Phys. Rev. **C72**, 055502 (2005), nucl-ex/0502021.
- [61] B. Aharmim et al. (SNO), Phys. Rev. Lett. **101**, 111301 (2008), 0806.0989.
- [62] B. Aharmim et al. (SNO Collaboration) (2011), 1109.0763.
- [63] G. Bellini et al. (The Borexino Collaboration), Phys.Rev.Lett. **107**, 141302 (2011), 1104.1816.
- [64] G. Bellini et al. (Borexino), Phys.Rev. **D82**, 033006 (2010), 0808.2868.
- [65] A. A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev.Lett. **103**, 061802 (2009), 0903.2465.
- [66] G. Cheng et al. (MiniBooNE Collaboration, SciBooNE Collaboration), Phys.Rev. **D86**, 052009 (2012), 1208.0322.
- [67] P. Adamson et al. (The MINOS Collaboration), Phys.Rev. **D81**, 052004 (2010), 1001.0336.
- [68] P. Adamson et al. (MINOS Collaboration), Phys.Rev.Lett. (2011), * Temporary entry *, 1104.3922.
- [69] Y. Declais, J. Favier, A. Metref, H. Pessard, B. Achkar, et al., Nucl.Phys. **B434**, 503 (1995).
- [70] Y. Declais, H. de Kerret, B. Lefievre, M. Obolensky, A. Etenko, et al., Phys.Lett. **B338**, 383 (1994).
- [71] A. Kuvshinnikov, L. Mikaelyan, S. Nikolaev, M. Skorokhvatov, and A. Etenko, JETP Lett. **54**, 253 (1991).
- [72] G. Vidyakin, V. Vyrodov, I. Gurevich, Y. Kozlov, V. Martemyanov, et al., Sov.Phys.JETP **66**, 243 (1987).
- [73] H. Kwon, F. Boehm, A. Hahn, H. Henrikson, J. Vuilleumier, et al., Phys.Rev. **D24**, 1097 (1981).
- [74] G. Zacek et al. (CALTECH-SIN-TUM), Phys. Rev. **D34**, 2621 (1986).

- [75] M. Apollonio et al. (CHOOZ), *Eur. Phys. J.* **C27**, 331 (2003), [hep-ex/0301017](#).
- [76] F. Boehm, J. Busenitz, B. Cook, G. Gratta, H. Henrikson, et al., *Phys.Rev.* **D64**, 112001 (2001), [hep-ex/0107009](#).
- [77] D. Dwyer (2012), Talk at Neutrino2012, 3–9 June 2012, Kyoto, Japan.
- [78] Y. Abe et al. (Double Chooz Collaboration), *Phys.Rev.* **D86**, 052008 (2012), [1207.6632](#).
- [79] A. Gando et al. (The KamLAND Collaboration), *Phys.Rev.* **D83**, 052002 (2011), [1009.4771](#).
- [80] F. Dydak, G. Feldman, C. Guyot, J. Merlo, H. Meyer, et al., *Phys.Lett.* **B134**, 281 (1984).
- [81] J. Reichenbacher (2005).
- [82] L. Auerbach et al. (LSND), *Phys.Rev.* **C64**, 065501 (2001), [hep-ex/0105068](#).
- [83] P. Huber, M. Lindner, and W. Winter, *Comput. Phys. Commun.* **167**, 195 (2005), [hep-ph/0407333](#), URL <http://www.mpi-hd.mpg.de/globes>.
- [84] P. Huber, J. Kopp, M. Lindner, M. Rolinec, and W. Winter, *Comput. Phys. Commun.* **177**, 432 (2007), [hep-ph/0701187](#), URL <http://www.mpi-hd.mpg.de/globes>.
- [85] M. C. Gonzalez-Garcia and M. Maltoni, *Phys. Rept.* **460**, 1 (2008), [0704.1800](#).
- [86] M. Maltoni and T. Schwetz, *Phys. Rev.* **D76**, 093005 (2007), [0705.0107](#).
- [87] E. Akhmedov and T. Schwetz, *JHEP* **1010**, 115 (2010), [1007.4171](#).
- [88] M. Maltoni and T. Schwetz, *Phys. Rev.* **D68**, 033020 (2003), [hep-ph/0304176](#).
- [89] G. Karagiorgi, M. Shaevitz, and J. Conrad (2012), [1202.1024](#).
- [90] P. Ade et al. (Planck Collaboration) (2013), [1303.5076](#).
- [91] G. Hinshaw, D. Larson, E. Komatsu, D. Spergel, C. Bennett, et al. (2012), [1212.5226](#).
- [92] S. Das, T. Louis, M. R. Nolta, G. E. Addison, E. S. Battistelli, et al. (2013), [1301.1037](#).
- [93] C. Reichardt, L. Shaw, O. Zahn, K. Aird, B. Benson, et al., *Astrophys.J.* **755**, 70 (2012), [1111.0932](#).
- [94] K. Story, C. Reichardt, Z. Hou, R. Keisler, K. Aird, et al. (2012), [1210.7231](#).
- [95] W. J. Percival et al. (SDSS Collaboration), *Mon.Not.Roy.Astron.Soc.* **401**, 2148 (2010), [0907.1660](#).
- [96] N. Padmanabhan, X. Xu, D. J. Eisenstein, R. Scalzo, A. J. Cuesta, et al. (2012), [1202.0090](#).
- [97] C. Blake, E. Kazin, F. Beutler, T. Davis, D. Parkinson, et al., *Mon.Not.Roy.Astron.Soc.* **418**, 1707 (2011), [1108.2635](#).
- [98] L. Anderson, E. Aubourg, S. Bailey, D. Bizyaev, M. Blanton, et al., *Mon.Not.Roy.Astron.Soc.* **427**, 3435 (2013), [1203.6594](#).

- [99] J. R. Kristiansen, O. y. Elgarø y, C. Giunti, and M. Laveder (2013), 1303.4654.
- [100] A. Mirizzi, N. Saviano, G. Miele, and P. D. Serpico (2012), 1206.1046.
- [101] N. Saviano, A. Mirizzi, O. Pisanti, P. D. Serpico, G. Mangano, et al. (2013), 1302.1200.
- [102] L. Bento and Z. Berezhiani, Phys.Rev. **D64**, 115015 (2001), hep-ph/0108064.
- [103] A. Dolgov and F. Takahashi, Nucl.Phys. **B688**, 189 (2004), hep-ph/0402066.
- [104] J. Hamann, S. Hannestad, G. G. Raffelt, and Y. Y. Wong, JCAP **1109**, 034 (2011), 1108.4136.
- [105] G. Gelmini, S. Palomares-Ruiz, and S. Pascoli, Phys.Rev.Lett. **93**, 081302 (2004), astro-ph/0403323.
- [106] H. Motohashi, A. A. Starobinsky, and J. Yokoyama (2012), 1203.6828.
- [107] C. M. Ho and R. J. Scherrer (2012), 1212.1689.
- [108] J. G. Morfin, J. Nieves, and J. T. Sobczyk, Adv.High Energy Phys. **2012**, 934597 (2012), 1209.6586.
- [109] B. Bhattacharya, R. J. Hill, and G. Paz, Phys.Rev. **D84**, 073006 (2011), 1108.0423.
- [110] A. Bodek, S. Avvakumov, R. Bradford, and H. S. Budd, J.Phys.Conf.Ser. **110**, 082004 (2008), 0709.3538.
- [111] V. Bernard, L. Elouadrhiri, and U. Meissner, J.Phys. **G28**, R1 (2002), hep-ph/0107088.
- [112] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev. **D81**, 092005 (2010), 1002.2680.
- [113] V. Lyubushkin et al. (NOMAD Collaboration), Eur.Phys.J. **C63**, 355 (2009), 0812.4543.
- [114] J.G.Morfin (MINER ν A Collaboration), poster presented at NEUTRINO2012 Conference, Kyoto (2012).
- [115] S. Boyd, S. Dytman, E. Hernandez, J. Sobczyk, and R. Tacik, AIP Conf.Proc. **1189**, 60 (2009).
- [116] R. Smith and E. Moniz, Nucl.Phys. **B43**, 605 (1972).
- [117] O. Benhar, A. Fabrocini, S. Fantoni, and I. Sick, Nucl.Phys. **A579**, 493 (1994).
- [118] O. Benhar and D. Meloni, Nucl.Phys. **A789**, 379 (2007), hep-ph/0610403.
- [119] A. M. Ankowski and J. T. Sobczyk, Phys.Rev. **C77**, 044311 (2008), 0711.2031.
- [120] J. Marteau, Eur.Phys.J. **A5**, 183 (1999), hep-ph/9902210.
- [121] M. Martini, M. Ericson, G. Chanfray, and J. Marteau, Phys.Rev. **C80**, 065501 (2009), 0910.2622.
- [122] M. Martini, M. Ericson, G. Chanfray, and J. Marteau, Phys.Rev. **C81**, 045502 (2010), 1002.4538.
- [123] J. Nieves, I. Ruiz Simo, and M. Vicente Vacas, Phys.Lett. **B707**, 72 (2012), 1106.5374.
- [124] J. Nieves, I. Ruiz Simo, and M. Vicente Vacas, Phys.Rev. **C83**, 045501 (2011), 1102.2777.

- [125] M. Martini, M. Ericson, and G. Chanfray, Phys.Rev. **C84**, 055502 (2011), 1110.0221.
- [126] D. Meloni and M. Martini, Phys.Lett. **B716**, 186 (2012), 1203.3335.
- [127] J. T. Sobczyk, Phys.Rev. **C86**, 015504 (2012), 1201.3673.
- [128] M. Martini, M. Ericson, and G. Chanfray, Phys.Rev. **D85**, 093012 (2012), 1202.4745.
- [129] U. Mosel and O. Lalakulich, PoS **BORMIO2012**, 034 (2012), 1204.2269.
- [130] O. Lalakulich, K. Gallmeister, and U. Mosel, Phys.Rev. **C86**, 014614 (2012), 1203.2935.
- [131] S. Nakayama et al. (K2K Collaboration), Phys.Lett. **B619**, 255 (2005), hep-ex/0408134.
- [132] A. A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev. **D81**, 013005 (2010), 0911.2063.
- [133] Y. Kurimoto et al. (SciBooNE Collaboration), Phys.Rev. **D81**, 033004 (2010), 0910.5768.
- [134] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev. **D83**, 052007 (2011), 1011.3572.
- [135] O. Lalakulich, K. Gallmeister, T. Leitner, and U. Mosel, AIP Conf.Proc. **1405**, 127 (2011), 1107.5947.
- [136] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev. **D83**, 052009 (2011), 1010.3264.
- [137] T. Golan, C. Juszczak, and J. T. Sobczyk, Phys.Rev. **C86**, 015505 (2012), 1202.4197.
- [138] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Lett. **B664**, 41 (2008), 0803.3423.
- [139] Y. Kurimoto et al. (SciBooNE Collaboration), Phys.Rev. **D81**, 111102 (2010), 1005.0059.
- [140] M. Hasegawa et al. (K2K Collaboration), Phys.Rev.Lett. **95**, 252301 (2005), hep-ex/0506008.
- [141] K. Hiraide et al. (SciBooNE Collaboration), Phys.Rev. **D78**, 112004 (2008), 0811.0369.
- [142] D. Rein and L. M. Sehgal, Nucl.Phys. **B223**, 29 (1983).
- [143] C. Berger and L. Sehgal, Phys.Rev. **D76**, 113004 (2007), 0709.4378.
- [144] C. Berger, AIP Conf.Proc. **1189**, 218 (2009), 0908.2758.
- [145] E. Paschos and D. Schalla, AIP Conf.Proc. **1189**, 213 (2009), 0910.2852.
- [146] E. Hernandez, J. Nieves, and M. Vicente-Vacas, Phys.Rev. **D80**, 013003 (2009), 0903.5285.
- [147] S. Nakamura, T. Sato, T.-S. Lee, B. Szczerbinska, and K. Kubodera, Phys.Rev. **C81**, 035502 (2010), 0910.1057.
- [148] M. Valverde, J. Amaro, E. Hernandez, and J. Nieves, Acta Phys.Polon. **B40**, 2551 (2009), 0906.1516.
- [149] E. Hernandez, J. Nieves, and M. Valverde, Phys.Rev. **D82**, 077303 (2010), 1007.3685.

- [150] L. Alvarez-Ruso, L. Geng, S. Hirenzaki, M. Vicente Vacas, T. Leitner, et al., AIP Conf.Proc. **967**, 201 (2007), 0709.3019.
- [151] D. Rein and L. M. Sehgal, Annals Phys. **133**, 79 (1981).
- [152] K. M. Graczyk and J. T. Sobczyk, Phys.Rev. **D77**, 053003 (2008), 0709.4634.
- [153] J. A. Nowak (MiniBooNE Collaboration), AIP Conf.Proc. **1189**, 243 (2009), 0909.3659.
- [154] K. M. Graczyk and J. T. Sobczyk, Phys.Rev. **D77**, 053001 (2008), 0707.3561.
- [155] A. Bodek and U.-k. Yang, AIP Conf.Proc. **1222**, 233 (2010).
- [156] M. Gluck, E. Reya, and A. Vogt, Eur.Phys.J. **C5**, 461 (1998), hep-ph/9806404.
- [157] P. Astier et al. (NOMAD Collaboration), Nucl.Instrum.Meth. **A515**, 800 (2003), hep-ex/0306022.
- [158] K. Abe et al. (T2K Collaboration), Nucl.Instrum.Meth. **A659**, 106 (2011), 1106.1238.
- [159] D. Ayres et al. (NOvA Collaboration) (2004), hep-ex/0503053.
- [160] T. Akiri et al. (LBNE Collaboration) (2011), 1110.6249.
- [161] M. Day and K. S. McFarland, Phys.Rev. **D86**, 053003 (2012), 1206.6745.
- [162] A. De Rujula, R. Petronzio, and A. Savoy-Navarro, Nucl.Phys. **B154**, 394 (1979).
- [163] A. Bodek and J. Ritchie, Phys.Rev. **D23**, 1070 (1981).
- [164] M. Martini, private communication via G. Zeller.
- [165] P. Huber, M. Mezzetto, and T. Schwetz, JHEP **0803**, 021 (2008), 0711.2950.
- [166] D. A. Dwyer (Collaboration for the Daya Bay) (2013), 1303.3863.
- [167] Y. Abe et al. (Double Chooz Collaboration) (2013), 1301.2948.
- [168] P. Coloma, P. Huber, J. Kopp, and W. Winter (2012), 1209.5973.
- [169] O. Lalakulich and U. Mosel, Phys.Rev. **C86**, 054606 (2012), 1208.3678.
- [170] J. Nieves, F. Sanchez, I. Ruiz Simo, and M. Vicente Vacas, Phys.Rev. **D85**, 113008 (2012), 1204.5404.
- [171] B. Osmanov (MINERvA Collaboration) (2011), 1109.2855.
- [172] S. Mishra (2010).
- [173] S. Mishra et al. (2008), Letter of Intent submitted to Fermilab .
- [174] T. Akesson et al. (ATLAS collaboratian), Nucl. Instrum. Meth. **A522**, 50 (2004).
- [175] T. Akesson et al. (ATLAS collaboratian), Nucl. Instrum. Meth. **A522**, 131 (2004).

- [176] T. Akesson et al. (ATLAS collaboration), *IEEE Nucl.Sci.Symp.Conf.Rec.* **2**, 1185 (2005).
- [177] V. Bychkov et al. (COMPASS collaboration), *Particles and Nuclei Letters* **2**, 111 (2002).
- [178] K. Platzer et al. (COMPASS collaboration), *IEEE Transactions on Nuclear Science* **52(3)** (2005).
- [179] A. Stahl et al., *Expression of Interest for a very long baseline neutrino oscillation experiment (LBNO)* (2012), CERN-SPSC-2012-021, SPSC-EOI-007; <http://cds.cern.ch/record/1457543>.
- [180] The MICE collaboration, mICE-TRD-2005.
- [181] E. Baussan et al. (EUROnu Super Beam Collaboration) (2012), 1212.0732.
- [182] E. Baussan, M. Dracos, T. Ekelof, E. F. Martinez, H. Ohman, et al. (2012), 1212.5048.
- [183] A. de Bellefon et al. (2006), [hep-ex/0607026](http://arxiv.org/abs/hep-ex/0607026).
- [184] L. Agostino et al. (MEMPHYS Collaboration), *JCAP* **1301**, 024 (2013), 1206.6665.
- [185] 1219664, *The Fermilab Main Injector Technical Design Handbook* (1994).
- [186] 610465, *The NuMI Technical Design Handbook* (2002).
- [187] V. Papadimitriou, *Status of the LBNE Neutrino Beamline* (2011), 1112.0720.
- [188] Fermilab, *Technical Division MI Lambertson design*, URL <http://tdserver1.fnal.gov/AcceleratorSupport/fmi-magnets/ILA>.
- [189] Fermilab, *Technical Division, MI C Magnet design*, URL <http://tdserver1.fnal.gov/AcceleratorSupport/fmi-magnets/ICA>.
- [190] Fermilab, *EDB Dipole design*, URL <http://tdserver12.fnal.gov/search?SearchableText=351156>.
- [191] FNAL, *FNAL FESS MI Radiation Safety Drawing no 9-6-6-7 C-8* (1993).
- [192] Fermilab, *NSIQ1 quadrupole design* (1993), URL <http://tdserver12.fnal.gov/search?SearchableText>.
- [193] Fermilab, *B2 Dipole design* (1993), URL <http://tdserver12.fnal.gov/search?SearchableText=351>.
- [194] J. Kyle, *Private communication*.
- [195] D. Cossairt, *Fermilab Radiological Control Manual Chapter 10 Section 3-6 A* (2010).
- [196] S. Chouhan et al., *IEEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY*, **21**, 1813 (2011).
- [197] P. Wanderer, *Private communication*.
- [198] T. Roberts, *G4beamline - A "Swiss Army Knife" for Geant4, optimized for simulating beamline* (2013), Version 2.12.
- [199] V. Lebedev, *OptiM - Computer code for linear and non-linear optics calculations* (2007).
- [200] S. Lee, *Accelerator Physics* (World Scientific, 2012), 3rd ed.

- [201] A. Liu et al. (2013), iPAC proceedings, Shanghai.
- [202] L. S by, *nuSTORM Beam instrumentation* (2013), eDMS document number: 1284677, CERN.
- [203] M. Gasior and R. Jones, *The principle and first results of betatron tune measurement by direct diode detection* (2005).
- [204] T. Lackowski et al., *nuSTORM Conventional Facilities Project Definition Report* (2013), FESS/Engineering Project No. 6-13-1.
- [205] D. G. Michael et al. (MINOS), Nucl. Instrum. Meth. **A596**, 190 (2008), 0805.3170.
- [206] A. E. I. for Detectors at Accelerators (2012), URL <http://aida.web.cern.ch/aida/index.html>.
- [207] G. Ambrosio et al. (VLHC Design Study Group) (2001).
- [208] R. Smith et al. (USCMS Collaboration), IEEE Trans.Appl.Supercond. **14**, 1830 (2004).
- [209] H. Piekarz, R. Carcagno, B. Claypool, G. W. Foster, S. L. Hays, et al., IEEE Trans.Appl.Supercond. **16**, 342 (2006).
- [210] G. Foster and V. Kashikhin, IEEE Trans.Appl.Supercond. **12**, 111 (2002).
- [211] A. Devred et al., IEEE Trans.Appl.Supercond. **22**, 4804909 (2012).
- [212] V. Vysotsky et al., IEEE Trans.Appl.Supercond. **20**, 402 (2010).
- [213] A. Foussart et al., IEEE Trans.Appl.Supercond. **22**, 42000505 (2012).
- [214] R. Wesche, M. Bagnasco, P. Bruzzone, M. Calvi, F. Cau, et al. (2009).
- [215] P. Adamson et al. (MINOS Collaboration), IEEE Trans.Nucl.Sci. **49**, 861 (2002).
- [216] H. Maesaka (K2K SciBar Collaboration), pp. 185–198 (2003).
- [217] Y. Kudenko (T2K), Nucl. Instrum. Meth. **A598**, 289 (2009), 0805.0411.
- [218] D. Greiner, T. Lachenmaier, J. Jochum, and A. Cabrera, Nucl. Instrum. Meth. **A581**, 139 (2007).
- [219] Z. Sadygov (1996), russian patent No. 2102820.
- [220] N. Bacchetta et al., Nucl. Instrum. Meth. **A383**, 263 (1996).
- [221] B. Dolgoshein (SIPM Collaboration), pp. 442–456 (2003).
- [222] S. Hansen (2012), mu2e document 2565.
- [223] R. Bayes, A. Laing, F. Soler, A. Cervera Villanueva, J. Gomez Cadenas, et al., Phys.Rev. **D86**, 093015 (2012), 1208.2735.
- [224] C. Andreopoulos et al., Nucl. Instrum. Meth. A **614**, 87 (2010), 0905.2517.
- [225] J. Apostolakis and D. H. Wright (Geant4), AIP Conf. Proc. **896**, 1 (2007).

- [226] A. Cervera-Villanueva, J. J. Gomez-Cadenas, and J. A. Hernando, Nucl. Instrum. Meth. **A534**, 180 (2004).
- [227] A. Hocker, J. Stelzer, F. Tegenfeldt, H. Voss, K. Voss, et al., PoS **ACAT**, 040 (2007), physics/0703039.
- [228] P. Adamson et al. (MINOS), Phys. Rev. D **82**, 051102 (2010), 1006.0996.
- [229] C. Tunnell, Ph.D. thesis, University of Oxford (2013).
- [230] R. J. Abrams, S. K. Agarwalla, A. Alekou, C. Andreopoulos, C. M. Ankenbrandt, S. Antusch, M. Apollonio, M. Aslaninejad, J. Back, P. Ballett, et al. (2011), 1112.2853, URL <http://arxiv.org/abs/1112.2853>.
- [231] J. V. D. W. Chris Haggmann, David Lange, Tech. Rep. UCRL-TM-229453, Lawrence Livermore National Laboratory (2013), URL <http://nuclear.llnl.gov/simulation/main.html>.
- [232] P. Adamson et al. (MINOS Collaboration), Phys.Rev. **D81**, 072002 (2010), 0910.2201.
- [233] P. Adamson et al., Nucl. Instrum. Meth. **A556**, 119 (2006).
- [234] C. Tunnell (2012), 1205.6338.
- [235] J. Kopp, M. Lindner, T. Ota, and J. Sato, Phys.Rev. **D77**, 013007 (2008), 0708.0152.
- [236] P. Adamson et al. (MINOS Collaboration), Phys.Rev. **D77**, 072002 (2008), 0711.0769.
- [237] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys. Rev. D **82**, 092005 (2010), URL <http://link.aps.org/doi/10.1103/PhysRevD.82.092005>.
- [238] P. Adamson et al., Phys. Rev. Lett. **102**, 211801 (2009), URL <http://link.aps.org/doi/10.1103/PhysRevLett.102.211801>.
- [239] A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys.Rev. **D83**, 052009 (2011), 1010.3264.
- [240] A. A. Aguilar-Arevalo et al. (MiniBooNE Collaboration), Phys. Rev. D **81**, 092005 (2010), URL <http://link.aps.org/doi/10.1103/PhysRevD.81.092005>.
- [241] C. Anderson et al. (ArgoNeuT Collaboration), Phys.Rev.Lett. **108**, 161802 (2012), 1111.0103.
- [242] K. Abe et al. (T2K Collaboration) (2013), 1302.4908.
- [243] F. Snider (MINERvA) (2012).
- [244] S. Mishra, R. Petti, and C. Rosenfeld, PoS **NUFACT08**, 069 (2008), 0812.4527.
- [245] S. Mishra (2013), private communication.
- [246] G. Fanourakis, L. Resvanis, G. Grammatikakis, P. Tsilimigras, A. Vayaki, et al., Phys.Rev. **D21**, 562 (1980).
- [247] S. Bonetti, G. Carnesecchi, D. Cavalli, P. Negri, A. Pullia, et al., Nuovo Cim. **A38**, 260 (1977).
- [248] L. Auerbach et al. (LSND Collaboration), Phys.Rev. **C66**, 015501 (2002), nucl-ex/0203011.

- [249] S. Belikov, A. Bugorsky, V. S. Epshtein, N. Kalganov, L. Klimenko, et al., *Z.Phys.* **A320**, 625 (1985).
- [250] J. Brunner et al. (SKAT Collaboration), *Z.Phys.* **C45**, 551 (1990).
- [251] W. Mann, U. Mehtani, B. Musgrave, Y. Oren, P. Schreiner, et al., *Phys.Rev.Lett.* **31**, 844 (1973).
- [252] N. Baker, A. Cnops, P. Connolly, S. Kahn, H. Kirk, et al., *Phys.Rev.* **D23**, 2499 (1981).
- [253] M. Whalley, *Nucl.Phys.Proc.Suppl.* **139**, 241 (2005), [hep-ph/0410399](http://arxiv.org/abs/hep-ph/0410399).
- [254] B. Jones, in *Proceedings of the XXIst International Europhysics Conference on High Energy Physics (EPS-HEP2011). 21-27 July 2011. Grenoble, Rhone-Alpes France.* (2011).
- [255] E. f. t. L. C. Church, To be published in *J. Phys. Conf. Ser.* (2013).
- [256] M. Antonello et al. (ICARUS Collaboration), *Advances in High Energy Physics* **2013** (2013).
- [257] C. Anderson et al., *Journal of Instrumentation* **7**, P10019 (2012), URL <http://stacks.iop.org/1748-0221/7/i=10/a=P10019>.
- [258] C. Andreopoulos et al., *Nucl. Instrum. Meth.* **A614**, 87 (2010), 0905.2517.
- [259] Aristotle, *Metaphysics* (353 BC(?)), book H 1045a 8-10:.
- [260] S. Agarwalla, E. Akhmedov, M. Blennow, P. Coloma, A. Donini, et al. (2012), 1209.2825.
- [261] LBNE Conceptual Design Report from Oct 2012, volume 1, URL <http://lbne.fnal.gov/papers.shtml>.
- [262] P. Coloma, A. Donini, E. Fernandez-Martinez, and P. Hernandez, *JHEP* **1206**, 073 (2012), 1203.5651.
- [263] P. Huber, M. Lindner, and W. Winter, *Nucl.Phys.* **B645**, 3 (2002), [hep-ph/0204352](http://arxiv.org/abs/hep-ph/0204352).
- [264] P. Huber, M. Lindner, M. Rolinec, and W. Winter, *Phys.Rev.* **D74**, 073003 (2006), [hep-ph/0606119](http://arxiv.org/abs/hep-ph/0606119).
- [265] A. D. Bross, M. Ellis, S. Geer, O. Mena, and S. Pascoli, *Phys.Rev.* **D77**, 093012 (2008), 0709.3889.
- [266] P. Kyberd, M. Ellis, A. Bross, S. Geer, O. Mena, et al. (2009).
- [267] J. Tang and W. Winter, *Phys.Rev.* **D81**, 033005 (2010), 0911.5052.
- [268] E. Fernandez Martinez, T. Li, S. Pascoli, and O. Mena, *Phys.Rev.* **D81**, 073010 (2010), 0911.3776.
- [269] P. Ballett and S. Pascoli, *Phys.Rev.* **D86**, 053002 (2012), 1201.6299.
- [270] E. Christensen, P. Coloma, and P. Huber (2013), 1301.7727.
- [271] P. Huber and T. Schwetz, *Phys.Lett.* **B669**, 294 (2008), 0805.2019.
- [272] T. Abe et al. (ISS Detector Working Group), *JINST* **4**, T05001 (2009), detector report of the International Scoping Study of a future Neutrino Factory and Super-Beam facility, 86 pages, 49 figures, 0712.4129.

[273] M. Green, *Private communication*.

[274] M. Green and S. St. Lorant, *Adv.Cryog.Eng.* **39A**, 271 (1994).

[275] A. Herve, G. Acquistapace, D. Campi, P. Cannarsa, P. Fabricatore, et al., *IEEE Trans.Appl.Supercond.* **12**, 385 (2002).

[276] V. Balbekov, *MuCool Note 216* (2001).

May | 2013

FESS/Engineering Project No. 6-13-1



nuSTORM Conventional Facilities

PDR

Project Definition Report for the conventional facilities to house the nuSTORM Facilities.

This Project Design Report (PDR) is intended to be a self-consistent basis for the development of a planning level cost estimate for the conventional facilities to support the programmatic requirements. This report has not answered every technical design question and as such, the current level of contingency is believed to be consistent with the degree of technical confidence in the design at this stage. It is recognized that some basic construction concerns will be reviewed and optimized during the remaining stages of the project.

Authors of this document:

T. Lackowski, FESS/Engineering
S. Dixon, FESS/Engineering
R. Jedziniak, LG Associates
M. Blewitt, Holabird & Root
L. Fink, Holabird & Root

SECTION I EXECUTIVE SUMMARY

SECTION II REQUIREMENTS

SECTION III DETAILED DESCRIPTION

Functional Areas

- Area 1 – Primary Beamline Enclosure
- Area 2 – Target Station
- Area 3 – Transport Line/Muon Decay Ring
- Area 4 – Near Detector
- Area 5 – Far Detector
- Area 6 – Site Work

SECTION IV SUGGESTED PROJECT BUDGET

- Part 1 – Cost Summary
- Part 2 - Methodology
- Part 3 - Cost Estimate Classification
- Part 4 - Preliminary Risk Identification

APPENDIX A COST DETAILS

APPENDIX B PRELIMINARY DRAWINGS

- PDR-01 Location Plans and List of Drawings
- PDR-02 Existing – Site Plan
- PDR-03 Underground – Site Plan
- PDR-04 Surface Buildings – Site Plan
- PDR-05 Primary Beamline
- PDR-06 Main Injector and Primary Beamline Sections
- PDR-07 Enclosure Plan at Target Hall
- PDR-08 Target Hall Building Plan Sheet 1
- PDR-09 Target Hall Building Plan Sheet 2
- PDR-10 Target Hall Building Sections Sheet 1
- PDR-11 Target Hall Building Sections Sheet 2
- PDR-12 Target Hall Building Sections Sheet 3
- PDR-13 Enlarged Plans and Sections
- PDR-14 Muon Decay Ring Plan
- PDR-15 Muon Decay Ring Section
- PDR-16 Muon Decay Ring Building Plan
- PDR-17 Cryogenic Building Plan
- PDR-18 Muon Decay Ring Building Section
- PDR-19 Near Detector Hall Floor Plan Sheet 1
- PDR-20 Near Detector Hall Floor Plan Sheet 2
- PDR-21 Near Detector Hall Floor Plan Sheet 3
- PDR-22 Building and Enclosure Section Sheet 1
- PDR-23 Building and Enclosure Section Sheet 2
- PDR-24 Far Detector Floor Plan
- PDR-25 Far Detector Floor Plan
- PDR-26 Building Section



The objective of this Project Definition Report (PDR) is to document one (1) possible solution for the conventional facilities required to house the nuSTORM experiment on the Fermilab site. It is recognized that this effort is done in support of obtaining DOE approval for Critical Decision Zero and that the programmatic requirements are still considered preliminary at this stage of the project.

The nuSTORM Conventional Facilities is anticipated to consist of six (6) functional areas consisting of the Primary Beamline, Target Station, Transport Line/Muon Decay Ring, Near Detector, Far Detector and the Site Work.

The nuSTORM Conventional Facilities will be located on the Fermilab site, south of the existing Main Injector and west of Kautz Road.

Project Costs

The Total Project Cost (TPC) for the Conventional Facilities portion of this project is estimated at \$148,350,000 for the construction and associated design services. The Other Project Costs (OPC) are estimated at \$2,526,000.

The TPC includes Construction, EDIA (Engineering, Design, Inspection and Administration), Contingency and Indirect Costs. The TPC has been estimated in FY13 dollars. The Indirect Costs associated with this project, are based on current laboratory rates, dated October 2012.

Schedule

CD-0 Approval	Month 0
CD-1 Approval	Month 12
CD-2 Approval	Month 24
CD-3 Approval	Month 36
Start Conventional Facilities Construction	Month 39
Complete Conventional Facilities Construction	Month 57

The schedule is based on technically driven parameters and does not incorporate lags for DOE approvals or funding restrictions.



REQUIREMENTS

nuSTORM Conventional Facilities

Section II

The nuSTORM Conventional Facilities design described in this Project Definition Report is based in information collected during discussions, meetings and workshops with the design leads of the functional areas. Listed below are the functional areas and the design leads for each area:

Primary Beamline	Michael Geelhoed
Target Station	Kris Anderson
Transport Line/Muon Decay Ring	Ao Liu
Near Detector	Alan Bross
Far Detector	Herman Cease
Site Work	FESS/Engineering

The following assumptions were incorporated into the development of this Project Definition Report.

- It is assumed that DOE Order 413.3A, “*Program and Project Management for the Acquisition of Capital Assets*,” will be followed during the execution of the subsequent phases of this project.
- The existing Main Injector accelerator will be reconfigured for use as an extraction beamline to support the nuSTORM facilities. This reconfiguration will result in a beamline that is extracted from the existing MI-40 absorber eastward to the nuSTORM facilities. It is assumed that the reconfiguration of the beamline and related devices is not part of the nuSTORM Conventional Facilities scope of work.
- While it is recognized that significant work associated with reconfiguring the cryogenic systems of the TeVatron is required to accommodate the nuSTORM Experiment, those costs are not included in the nuSTORM Conventional Facilities scope of work.
- For the purposes of this Project Definition Report, a shielding depth of 21 feet earth equivalent has been used for areas that contain extracted beam and twelve (12) feet for the Transport Line Enclosure, Muon Decay Ring Enclosure and those portions of the project associated with the secondary beam.
- It is assumed that the nuSTORM facilities will not be normally occupied.
- The guiding principals of high performance building design will be incorporated into the design of the nuSTORM Conventional Facilities. However, based on the type and use of the facilities, is not intended that the nuSTORM Conventional Facilities will become a LEED certified building. The project processes and each project element will be evaluated during design to reduce their impact on natural resources without sacrificing program objectives. The project design will incorporate maintainability, aesthetics,



REQUIREMENTS**nuSTORM Conventional Facilities**

environmental justice and program requirements to deliver a well-balanced project.

The drawings contained in the Appendix B contain detailed descriptions of additional requirements for the nuSTORM Conventional Facilities.

Section**II**



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

The nuSTORM Conventional Facilities will be located in an area south of the existing Main Injector accelerator and west of Kautz Road on the Fermilab site. In general terms, a proton beam will be extracted from the existing Main Injector at the MI-40 absorber, directed east towards a new below grade target station, muon decay ring. This extracted beam will be directed at a Near Detector east of the muon decay ring and towards the Far Detector located at the existing DZero Assembly Hall. Figure 1, below, shows a site photo depicting the nuSTORM Conventional Facilities.

Section III



Figure 1 – View Looking North of Fermilab with the nuSTORM Facilities



FUNCTIONAL AREAS

The nuSTORM Conventional Facilities are envisioned to include seven (7) functional areas. This is intended to provide a logical and constructible sequence to reduce the construction period to a minimum. Further design iterations will be required to determine how to optimize the construction packages based on programmatic and funding driven limitations.

Area 1 - Primary Beamline Enclosure (WBS 1.0)

The first functional area is the Primary Beamline Enclosure, consisting of the work involved with construction of a below-grade, concrete enclosure for the beamline components that will be required to transport the proton beam from the existing Main Injector enclosure into the Target Station. Figure 2, below, shows the plan view of the beamline enclosure with the nuSTORM beamline indicated in orange.

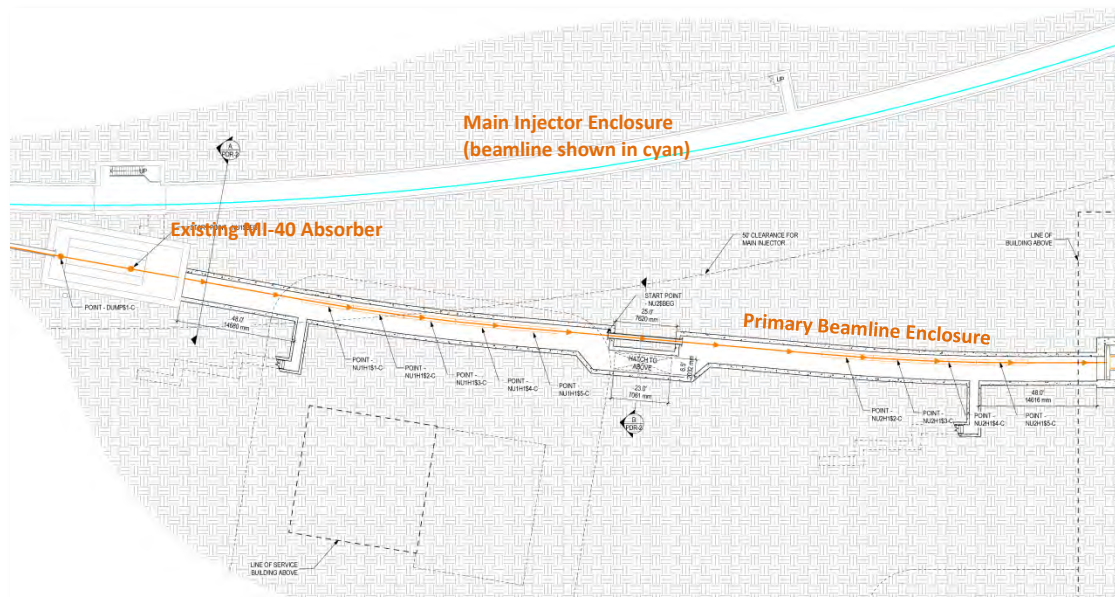


Figure 2 – Plan View of Primary Beamline Enclosure

At the upper portion of the figure is the existing Main Injector with the Main Injector beamline indicated in cyan. The nuSTORM Primary Beamline Enclosure (PBE) is shown at the lower right of the existing MI-40 Absorber in orange.

The nuSTORM PBE will begin at the existing east wall of the MI-40 Absorber and will house components similar to the conventional beamline components in the Main Injector. The PBE will include two (2) code compliance exit stairways provided at



each end of the enclosure to ensure proper exiting. These exit stairs will be similar in style and construction to stairs installed in the Main Injector Project.

In addition, the PBE will include a shielded drop hatch to accommodate installation of beamline components located at the approximate mid-point of the enclosure. This hatch is intended to remain open during installation of the beamline components. Once assembly is complete, the hatch will be filled with precast concrete shielding blocks to a depth of 21 feet in order to provide the required shielding for a primary beamline.

Portions of the PBE will be constructed during a Main Injector shutdown due to shielding requirements of the operating accelerator.

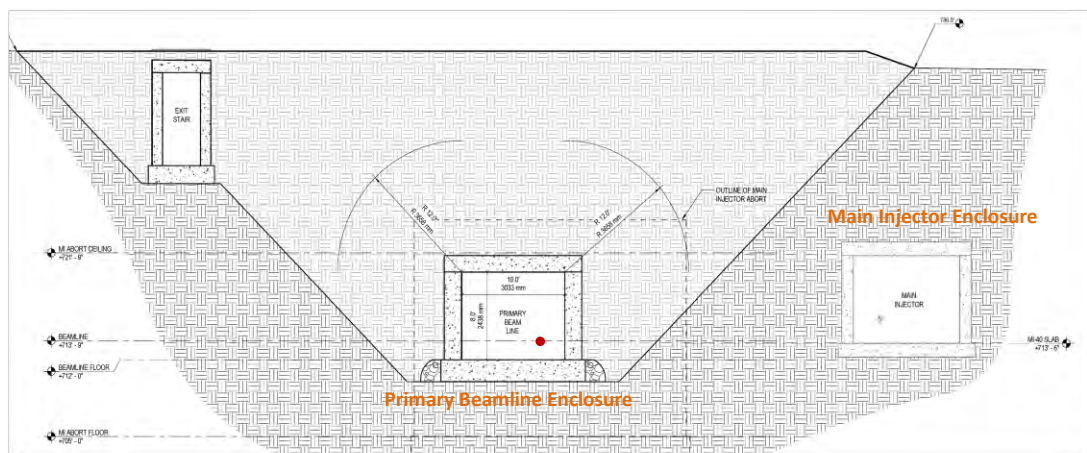


Figure 3 –Typical Section of Primary Beamline Enclosure

The PBE is based on the dimensions of a Main Injector style enclosure. These enclosures provide a ten (10) foot interior width and an eight (8) foot interior height. Figure 3, above, depicts a typical enclosure cross section. The beamline is shown as a red dot and is expected to be located three feet away from the north wall of the enclosure. The height of the beamline components will vary with the position of the beam.

Utilities and access to the PBE will be provided through a new Service Building located at grade level approximately halfway along the length of the PBE. This new 50'x50' service building will be based on a typical Main Injector style service building and associated electrical substation.



Area 2 – Target Station (WBS 2.0)

The second functional area is the nuSTORM Target Station consisting of below-grade, cast-in-place concrete enclosure for the beamline and detector components and an above grade Target Support Building.

The nuSTORM Target Station below grade detector enclosure consists of the spaces required to house the nuSTORM target and beamline components, accommodate installation and safe operation of the nuSTORM target. Technical requirements and access information for the nuSTORM Target Station are based on the nuSTORM Target Hall Preliminary Layout drawing dated 11-MAR-2013 and subsequent discussions.

Figure 4, below, is a plan view of the below grade portion of the nuSTORM Target Station at the same elevation of the Primary Beamline Enclosure. The target station will be an isolated concrete enclosure that provides a shielded environment for the target components. The shielding requirements include 3 feet of concrete on the floor and walls, a 6 inch air gap and 4 feet of steel shielding. The shielding above the target station provides space for eight feet of steel shielding and 3 feet of concrete shielding. The conventional construction work provides the concrete for the floor and walls of the target chase, but the steel shielding for the walls and floor as well as the shielding above the target is provided by the target group.

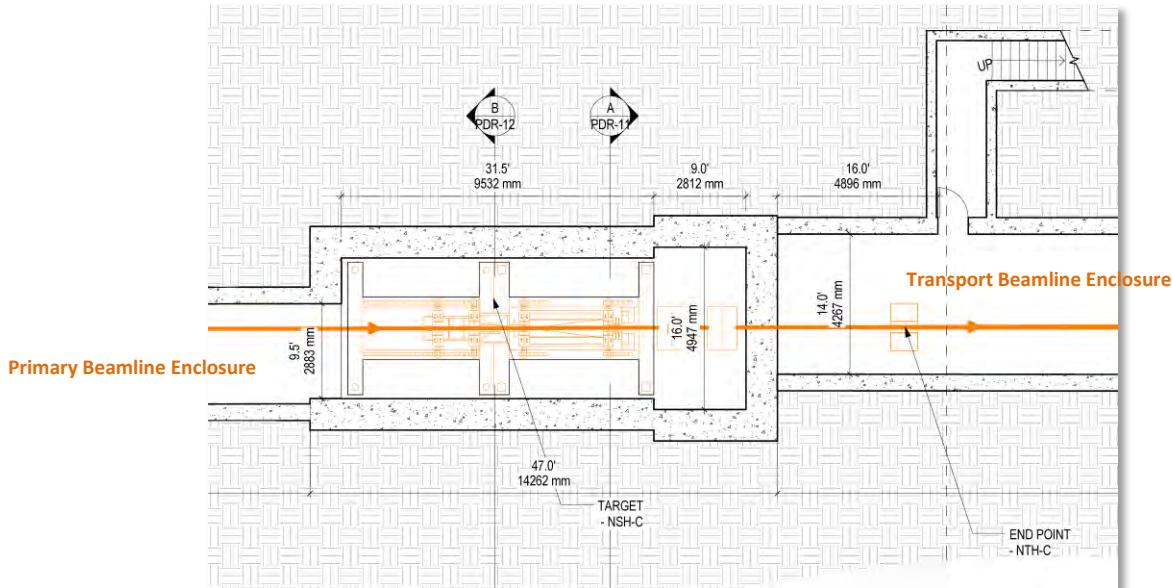


Figure 4 – Plan View of the nuSTORM Target Chase



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

Figure 5, below, provides a plan view of the lower level of the nuSTORM Target Station. This level, approximately 14 feet below existing grade, provides space for the support functions associated with the nuSTORM target including a work cell for target components, shielded storage of activated components, staging areas for shield blocks as well as the mechanical and electrical systems required to operate the nuSTORM target.

Section III

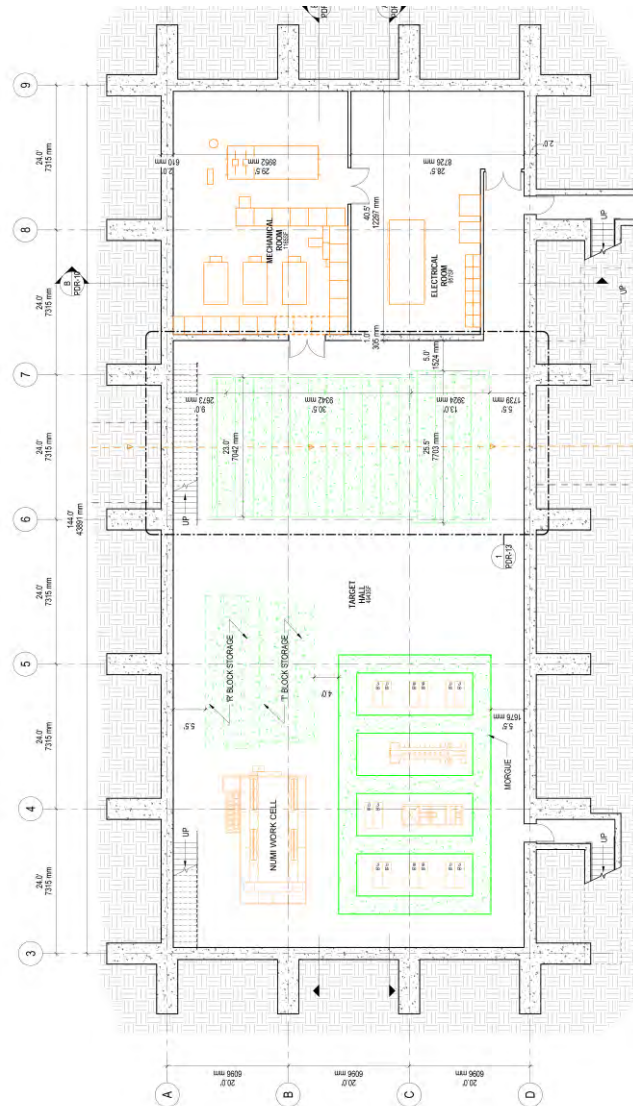


Figure 5 – Plan View of the Below Grade portion of the nuSTORM Target Station

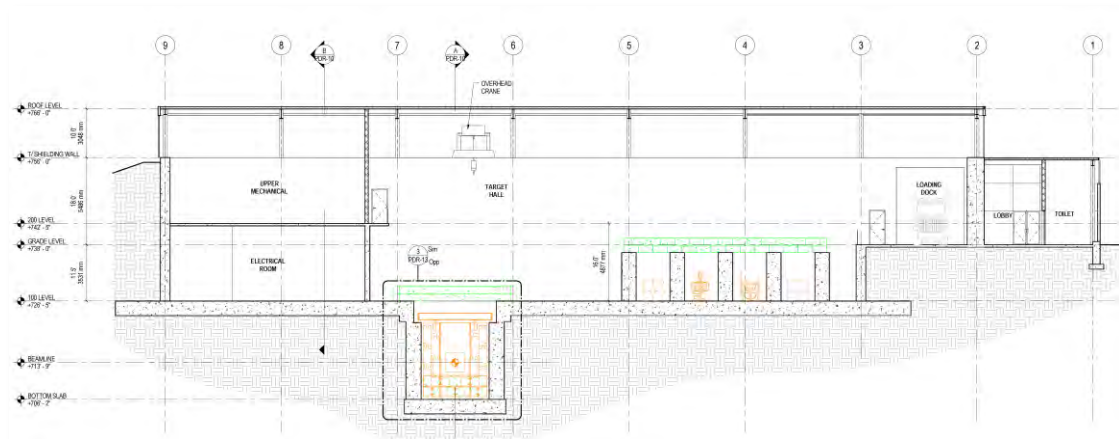


Figure 6 – Section View of the nuSTORM Target Station

Figure 6, above, depicts a section view of the nuSTORM Target Station showing the relationship of the target chase to the below grade areas and the above grade target service building. The above grade portion of the nuSTORM Target Station consists of a service building that includes a loading dock, toilet facilities, mechanical and electrical rooms to support the operation of the building. The above grade building has been designed to accommodate the movement and handling of activated target components. As a result, the walls of the above grade building provide 3 feet of shielding to a height of 10 feet above grade.

The below grade portion of the nuSTORM Target Station will be constructed of cast-in-place concrete. The above grade portion will be constructed of cast-in-place concrete walls and a structural steel frame to support the roof and the overhead bridge crane. The building will be equipped with a 50 ton capacity overhead bridge crane, similar in style and construction to cranes installed with the Main Injector project.

The arrangement of the spaces for the below grade portion of the nuSTORM Target Station include the provision for code compliant egress. This is accomplished with two (2) exit stairs and connecting smoke-proof corridors positioned to allow for two (2) means of egress for the below grade spaces.

The nuSTORM Target Service building contains the Mechanical Room, Electrical Room, toilets and janitor's closet to support the operation of the facility. These spaces have been sized based on experience with the Main Injector and NuMI projects and have not been optimized based on specific equipment or processes.



The mechanical systems for the nuSTORM Target Station include the following:

- Target Chase system to provide cooling for the target;
- Building system to condition the space and provide a pressure gradient towards the Target Chase;
- Service Building system to condition the support spaces;
- A tritium recovery system similar to the existing system used at NuMI to condense the moisture in the Target Chase, transport it to a boiler in the above grade building;
- A Target Chase underdrain system to intercept groundwater at the Target Chase. This system will include a geo-membrane system capable of isolating the Target Chase from the surrounding area with appropriate witness zones to verify the operation of the system;
- An interior water collection within the Target Chase to collect water from the interior of the chase. This water will be directed to a dedicated sump basin for testing. Contaminated water will be collected and disposed of properly utilizing standard Laboratory procedures;
- A building underdrain system to intercept ground water and pump it to the surface. This system will include redundant sump basins with duplex pumps.

Area 3 – Transport Line Enclosure (WBS 3.0)

The third functional area is the consists of the below grade beamline enclosure to house the Transport Beamline components required to transport the secondary beam from the Target Station to the Muon Decay Ring and the enclosure to house the Primary Beam Absorber.

The Transport Beamline Enclosure will begin at the east wall of the Target Station and will house both conventional and cryogenic beamline components. The Transport Beamline Enclosure will include code compliance exits that will be similar in style and construction to stairs installed in the Main Injector.

The Transport Beamline Enclosure is based on the dimensions of a Main Injector style concrete enclosure. These enclosures provide a ten (10) foot interior width and an eight (8) foot interior height.

Figure 7, below, depicts a plan view of the Transport Beamline Enclosure with the Target Station shown on the left side, the Muon Decay Ring Enclosure shown at the upper right corner and the Beam Absorber Enclosure at the lower right corner.

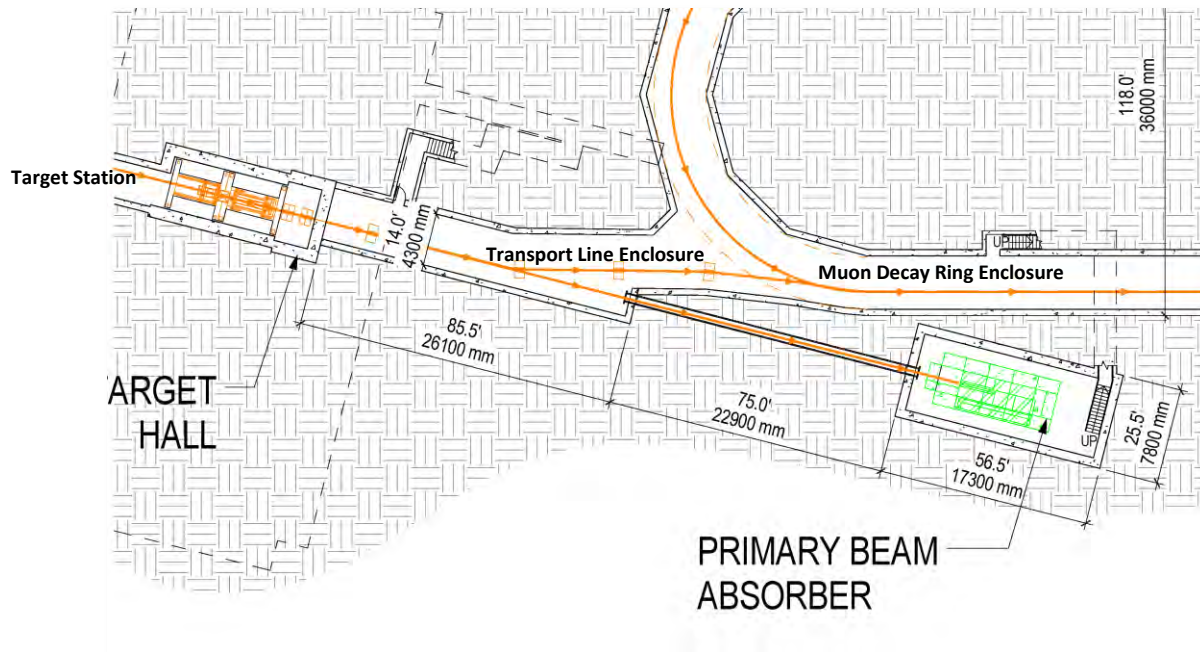


Figure 7 – Plan View of Transport Line Enclosure

The Primary Beam Absorber Enclosure has been designed to accommodate a steel and concrete beam absorber similar in size, type and construction to the existing MI-40 absorber. For the purposes of this report, the conventional construction is assumed to provide the cast-in-place concrete enclosure, code compliant exiting and the buried beam pipe that connects the Beam Absorber Enclosure to the Transport Beamline Enclosure. The shielding steel is assumed to be provided by the technical group.

Utilities and access for the Transport Beamline Enclosure will be provided through the nuSTORM Target Service Building located west of the Transport Beamline Enclosure

Area 4 – Muon Decay Ring Enclosure (WBS 4.0)

The fourth functional area consists of the enclosures, buildings and infrastructure to support the installation and operation of the Muon Decay Ring beamline components including the following:

- The nuSTORM Muon Decay Ring (MDR) Enclosure consisting of a below grade beamline enclosure to house the beamline components for the muon decay ring;
- The Pion Absorber enclosure;



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

- The above grade Muon Decay Ring Service Building;
- The above grade Cryogenic Building.

Figure 8, below, depicts the below grade portion of this functional area with the existing Main Injector Enclosure shown at the upper left corner of the figure, the nuSTORM Target Station at the left hand side, and the Muon Decay Ring Enclosure shown at the center.

Section III

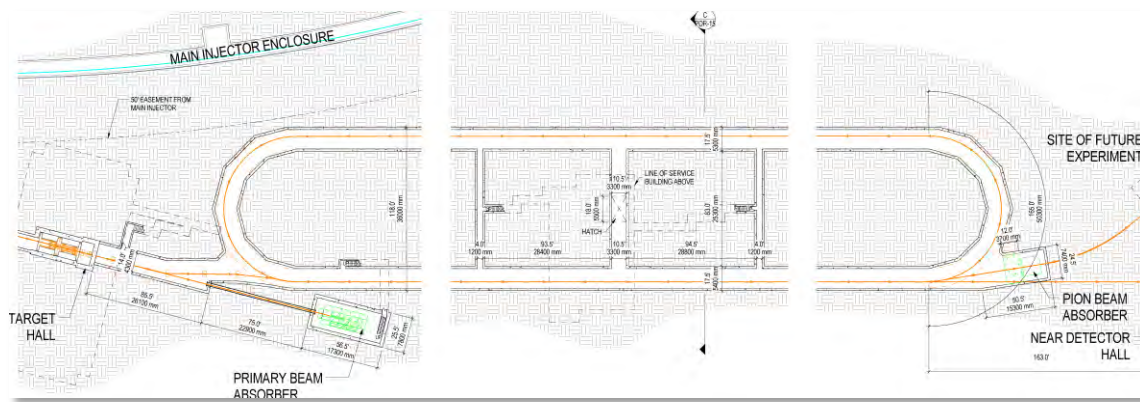


Figure 8 – Plan View of Muon Decay Ring Enclosure

The Muon Decay Ring Enclosure consists of a concrete enclosure with a 13 foot height and a 14 foot width. The enclosure is assumed to be outfitted in a similar manner as the typical Main Injector enclosure. The Muon Decay Ring Enclosure will be located approximately 27 feet below existing grade and provide more than the minimum of 12 feet of earth shielding. Figure 9, below depicts a cross section through the Muon Decay Ring Enclosure which shows the relative depth in relation to existing grade.

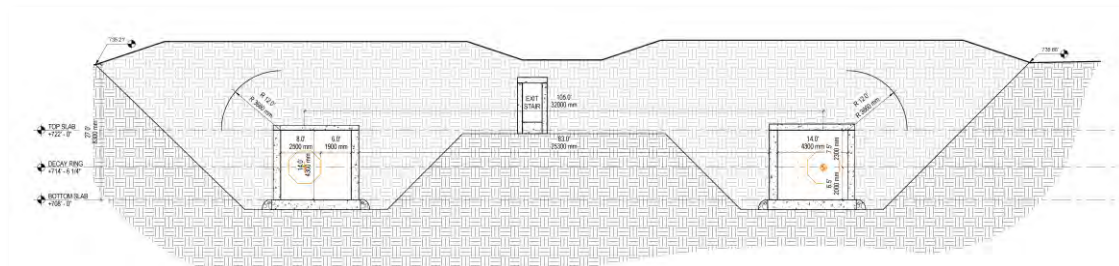


Figure 9 – Section View of Muon Decay Ring Enclosure

The Muon Decay Ring Enclosure will include code compliance exits similar in style and construction to exit stairs installed in the Main Injector.

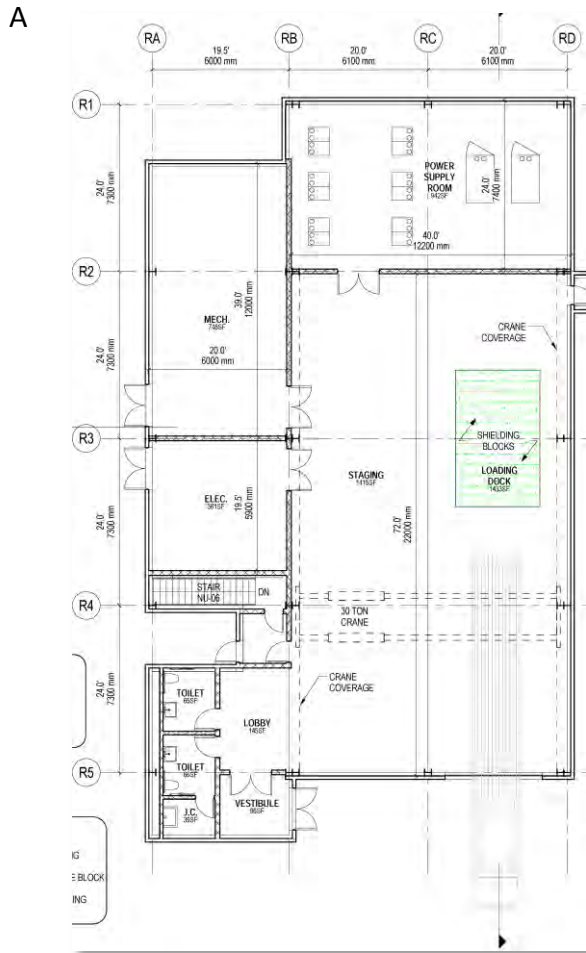


Figure 10 – Plan View of Muon Decay Ring Service Building

21 foot long by 12 foot wide shielded hatch located at the approximate center point of the Muon Decay Ring Enclosure will accommodate the vertical transport of beamline components.

The Pion Absorber Enclosure has been designed to accommodate a steel and concrete beam absorber that is 14 feet wide, by 14 feet high by 14 feet long. For the purposes of this report, the conventional construction is assumed to provide the concrete enclosure. The shielding steel and precast concrete shielding blocks are assumed to be provided by the technical group.

Utilities and access to the Muon Decay Ring Enclosure will be provided through the Muon Decay Ring Service Building located at grade at the approximate midpoint of the below grade Muon Decay Ring Enclosure.

The nuSTORM Muon Decay Ring Service Building, shown in figure 10 above, will house the functions to support the installation and operation of the Muon Decay Ring, including a loading dock, toilet facilities, janitor’s closet and Mechanical Room and Electrical Room. These spaces have been sized based on experience with the Main Injector and NuMI projects and have not been optimized based on specific equipment or processes.

The high bay of the nuSTORM Muon Decay Ring Service Building will provide space for staging and installing the nuSTORM Muon Decay Ring. The high bay includes a shield block filled hatch that allow access to the below grade Muon Decay Ring Enclosure. This hatch is intended to remain open during installation of the beamline components. Once assembly is complete, the hatch will be filled with precast



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

concrete shielding blocks to a depth of twelve (12) feet in order to provide the required shielding.

The high bay will be provided with a thirty (30) ton capacity overhead bridge crane that will be used for component staging and installations as well as shield block handling. The high bay contains space for the temporary staging of portions of the shield blocks should removal be required for maintenance and/or repair of the technical components.

The Structural Requirements for this functional area include:

- The below grade portions of the facility and building foundations will be constructed of cast-in-place concrete;
- The nuSTORM Muon Decay Ring Service Building will be metal sided, structural steel frame on a cast-in-place concrete foundation. The building will contain a 30 ton capacity overhead bridge crane to accommodate the unloading, staging and vertical transport of the beamline components;

The Mechanical Requirements for this function area include the following:

- The Mechanical Room will house the mechanical equipment that supports the assembly and operation of the nuSTORM Muon Decay Ring Service Building as well as the connection to the below grade Muon Decay Ring Enclosure;
- The HVAC systems for the nuSTORM Muon Decay Ring Service Building will conform to ASHRAE 90.1, ASHRAE 62 and applicable NFPA requirements and applicable sections of the Fermilab Engineering Standards Manual;
- Mechanical systems and Metasys controls will be further investigated during subsequent phases in accordance with ASHRAE 90.1 and Federal Life Cycle costing analysis;
- Heating, Ventilation and Air Conditioning Design Parameters:
 - Temperature: 68 degrees Fahrenheit to 78 degrees Fahrenheit
 - Humidity: 50% Maximum Relative Humidity, no minimum
- All plumbing work to be installed in accordance with Illinois Plumbing Code and Standard Specifications for Water & Sewer Main Construction in Illinois;
- The nuSTORM Muon Decay Ring Service Building will be conditioned with a roof mounted packaged HVAC system;
- A duplex sump pump system will be installed to collect subsurface water from around the nuSTORM Muon Decay Ring Service Building;

Section III



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

- Fire Alarm/Fire Suppression systems for the nuSTORM Muon Decay Ring Service Building shall be designed in accordance with the applicable sections of the Fermilab Engineering Standards Manual;
- Automatic sprinkler systems shall be designed to a minimum of an Ordinary Hazard Group 1 classification, in accordance with National Fire Protection Association (NFPA) latest edition. The most commonly used NFPA standards relative to automatic sprinkler systems are: 13, 20, 25, 231, 231C, 318, and 750;
- Fire alarm systems shall be designed with a minimum standby power (battery) capacity. These batteries shall be capable of maintaining the entire system in a non-alarm condition for 24 hours, in addition to 15 minutes in full load alarm condition. The most commonly used NFPA standards relative to fire alarm systems are: 70, 72, 90A, and 318;
- The facility will be equipped with a hard-wired, zoned, general evacuation fire alarm system consisting of:
 - Manual fire alarm stations at the building exits
 - Sprinkler system water flow and valve supervisory devices
 - Combination fire alarm horn/strobe located throughout the building
 - A 24 volt hard wire extension from the existing control panel
 - Connection to the site wide FIRUS monitoring system
 - Smoke detection as required.

The Electrical Requirements for this functional area include the following:

- The Electrical Equipment Room will house the electrical equipment that supports the assembly and operation of the nuSTORM Muon Decay Ring beamline components. This includes the incoming electrical service switchgear, panelboards, and related power supplies;
- The electrical power for the nuSTORM Muon Decay Ring Service Building will be provided by a new 1,500 kVA transformer. The transformer has been sized to accommodate the anticipated electrical power for both the conventional facilities and the programmatic equipment;
- The electrical substation will be located adjacent to the nuSTORM Muon Decay Ring Service Building. The substation will be designed to accommodate both the new transformer and associated 4-way air switch;
- The new electrical substation will be connected to the nuSTORM Muon Decay Ring Service Building via a new concrete encased duct bank and will be routed to new electrical service switchgear inside the Muon Decay Ring Service Building. The switchgear will be sized to accommodate the entire 1,500 kVA power from the new transformer;

Section III



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

- From the switchgear the electrical power will serve conventional facilities equipment and programmatic equipment for the nuSTORM components;
- The power for the conventional HVAC equipment will be provided from the new electrical switchgear, utilizing 480v power;
- New electrical panels serving the lights, outlets and general house power will be included in the electrical power distribution system.

Section III

Adjacent to the Muon Decay Ring Service Building will be the nuSTORM Cryogenic Building. This building will consist of the work involved with construction of an at-grade building and related facilities required to house cryogenic equipment for the nuSTORM Experiment.

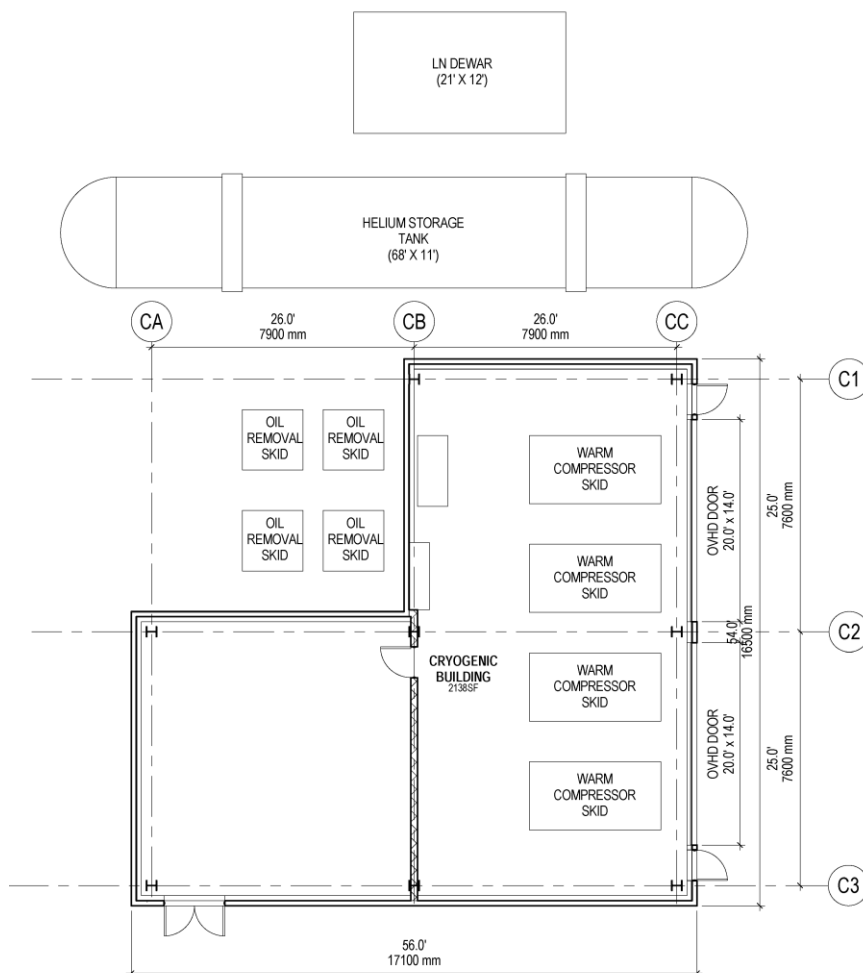


Figure 11 – Plan View of Cryogenic Building



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

The Cryogenic Building, shown in figure 11 above, is sized based on existing buildings in the Main Ring that serves a similar function. Adjacent to the Cryogenic Building is a 60 foot wide by 100 foot long hardstand area intended for trailer parking to support the cryogenic operations.

The Cryogenic Building will be connected to the nuSTORM Muon Decay Ring Service Building via a below grade trench to house the refrigerant piping and associated control equipment to support operations. The trench will terminate in the drop shaft to the below grade Muon Decay Ring Enclosure.

Section III

Area 5 – Near Detector (WBS 5.0)

The fifth functional area is the nuSTORM Near Detector Hall consisting of a below grade enclosure to house the nuSTORM Near Detectors and the above grade nuSTORM Near Detector Service Building.

Figure 12, below, depicts the below grade portion of the Near Detector Service Building. This space has been designed to accommodate the nuSTORM Near Detector as well as space for future experiments.

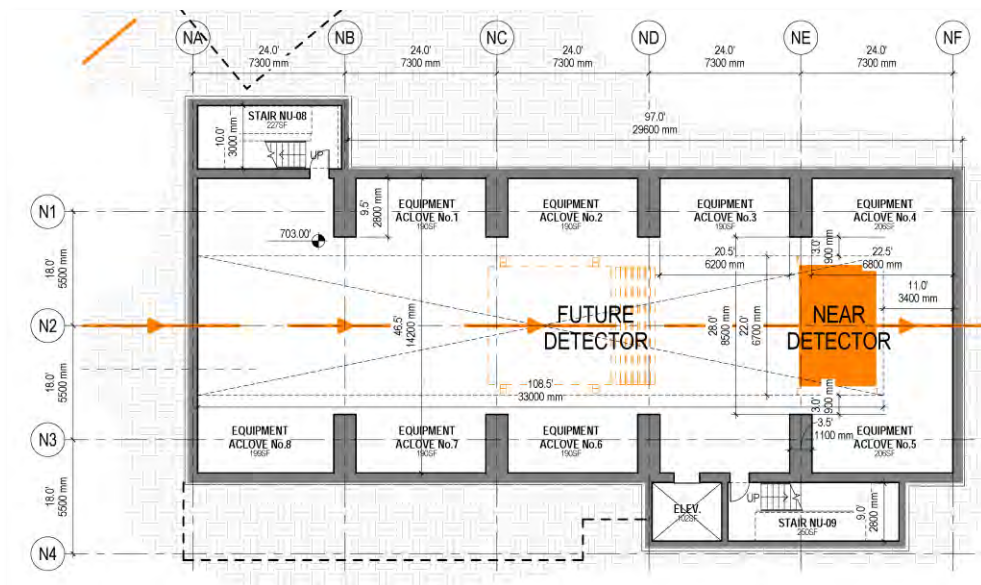


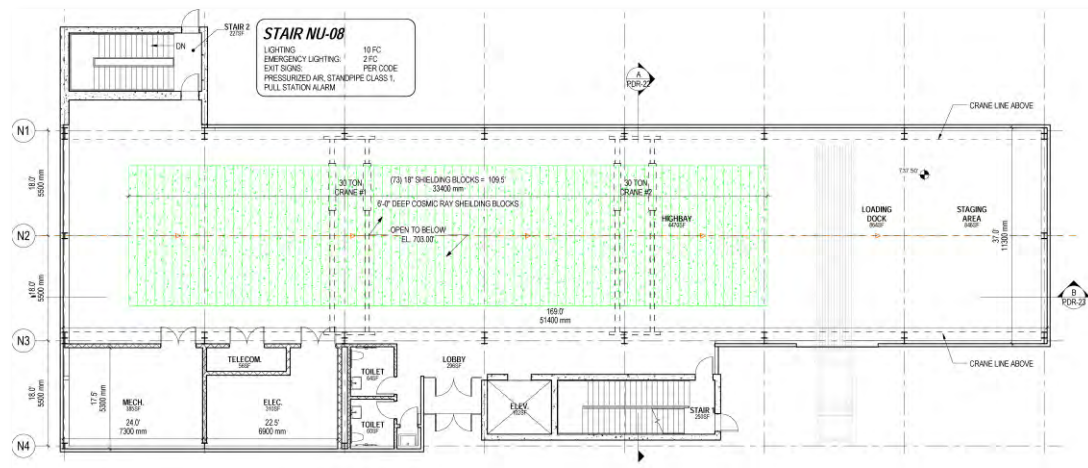
Figure 12 – Plan View of the Near Detector Enclosure.



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

The below grade portions of the facility and building foundations will be constructed of cast-in-place concrete and has been designed to accommodate six (6) feet of precast concrete shielding blocks over the detector.



Section III

Figure 13 – Plan View of the Near Detector Service Building

The above grade portion, shown in Figure 13 above, of the nuSTORM Near Detector Service Building will be a braced steel frame with pre-finished metal siding. The high bay will provide space for staging and assembling the detectors.

The space is dominated by a shield block filled hatch that allow access to the below grade detector enclosure. This hatch is intended to remain open during assembly of the detector. Once assembly is complete, the hatch will be filled with precast concrete shielding blocks to a depth of six (6) feet in order to provide the required shielding.

The high bay will be provided with two (2) thirty (30) ton capacity overhead bridge cranes that will be used for detector assembly as well as shield block handling. The high bay contains space for the temporary staging of portions of the shield blocks should removal be required for maintenance and/or repair of the detector components.

The design provides space adjacent to the nuSTORM Near Detector for the operation of the nuSTORM Near Detector including the associated computer hardware. It is recognized that this space will be minimally occupied as the day to day operation of the detector will likely occur at a central facilities located elsewhere. As such, this space will serve as the front end to remote systems and will be used mainly during



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

assembly, initial startup and maintenance/repair activities. This space will be designed in a similar manner to existing control rooms found on the Fermilab site.

The Structural Requirements for this functional area include:

- The below grade portions of the facility and building foundations will be constructed of cast-in-place concrete and has been designed to accommodate six (6) feet of precast concrete shielding blocks over the detector;
- The Muon Decay Ring Service Building will be metal sided, structural steel frame on a cast-in-place concrete foundation. The building will contain a 30 ton capacity overhead bridge crane to accommodate the unloading, staging and vertical transport of the beamline components;
- The above grade portion, nuSTORM Near Detector Service Building will be a braced steel frame with pre-finished metal siding;

The Mechanical Requirements for this functional area include the following:

- The Mechanical Room will house the mechanical equipment that supports the assembly and operation of the nuSTORM Near Detector Service Building as well as the connection to the below grade portion of the building;
- The HVAC systems for the nuSTORM Near Detector Ring Service Building will conform to ASHRAE 90.1, ASHRAE 62 and applicable NFPA requirements and applicable sections of the Fermilab Engineering Standards Manual
- Mechanical systems and Metasys controls will be further investigated during subsequent phases in accordance with ASHRAE 90.1 and Federal Life Cycle costing analysis;
- Heating, Ventilation and Air Conditioning Design Parameters:
 - Temperature: 68 degrees Fahrenheit to 78 degrees Fahrenheit
 - Humidity: 50% Maximum Relative Humidity, no minimum
- All plumbing work will be installed in accordance with Illinois Plumbing Code and Standard Specifications for Water & Sewer Main Construction in Illinois.
- The nuSTORM Near Detector Service Building will be conditioned with a roof mounted packaged HVAC system.
- A duplex sump pump system will be installed to collect subsurface water from around the below grade portion of the nuSTORM Near Detector Service Building.
- Fire Alarm/Fire Suppression systems for the nuSTORM Near Detector Service Building shall be designed in accordance with the applicable sections of the Fermilab Engineering Standards Manual.
- Automatic sprinkler systems shall be designed to a minimum of an Ordinary Hazard Group 1 classification, in accordance with National Fire Protection Association (NFPA) latest edition. The most commonly used NFPA standards

Section III



DETAILED DESCRIPTION

nuSTORM Conventional Facilities

- relative to automatic sprinkler systems are: 13, 20, 25, 231, 231C, 318, and 750.
- Fire alarm systems shall be designed with a minimum standby power (battery) capacity. These batteries shall be capable of maintaining the entire system in a non-alarm condition for 24 hours, in addition to 15 minutes in full load alarm condition. The most commonly used NFPA standards relative to fire alarm systems are: 70, 72, 90A, and 318.
 - The facility will be equipped with a hard-wired, zoned, general evacuation fire alarm system consisting of:
 - Manual fire alarm stations at the building exits
 - Sprinkler system water flow and valve supervisory devices
 - Combination fire alarm horn/strobe located throughout the building
 - A 24 volt hard wire extension from the existing control panel
 - Connection to the site wide FIRUS monitoring system
 - Smoke detection as required.

Section III

The Electrical Requirements for this functional area include the following:

- The Electrical Equipment Room will house the electrical equipment that supports the assembly and operation of the technical components. This includes the incoming electrical service switchgear, panelboards, and related power supplies;
- The electrical power for the nuSTORM Near Detector Service Building will be provided by a new 1,500 kVA transformer. The transformer has been sized to accommodate the anticipated electrical power for both the conventional facilities and the programmatic equipment;
- The electrical substation will be located adjacent to the nuSTORM Near Detector Service Building. The substation will be designed to accommodate both the new transformer and associated 4-way air switch;
- The new electrical substation will be connected to the nuSTORM Near Detector Service Building via a new concrete encased duct bank and will be routed to new electrical service switchgear inside the Near Detector Service Building. The switchgear will be sized to accommodate the entire 1,500 kVA power from the new transformer;
- From the switchgear the electrical power will serve conventional facilities equipment and programmatic equipment for the nuSTORM components;
- The power for the conventional HVAC equipment will be provided from the new electrical switchgear, utilizing 480v power;
- New electrical panels serving the lights, outlets and general house power will be included in the electrical power distribution system.



Area 6 – Far Detector (WBS 6.0)

The sixth functional area is the nuSTORM Far Detector that will be housed in the existing DZero Assembly Hall. The existing DZero facilities will be repurposed to provide the space and infrastructure to accommodate the nuSTORM Far Detector. Figure 14, below, depicts the nuSTORM Far Detector located in the existing DZero Assembly Hall.

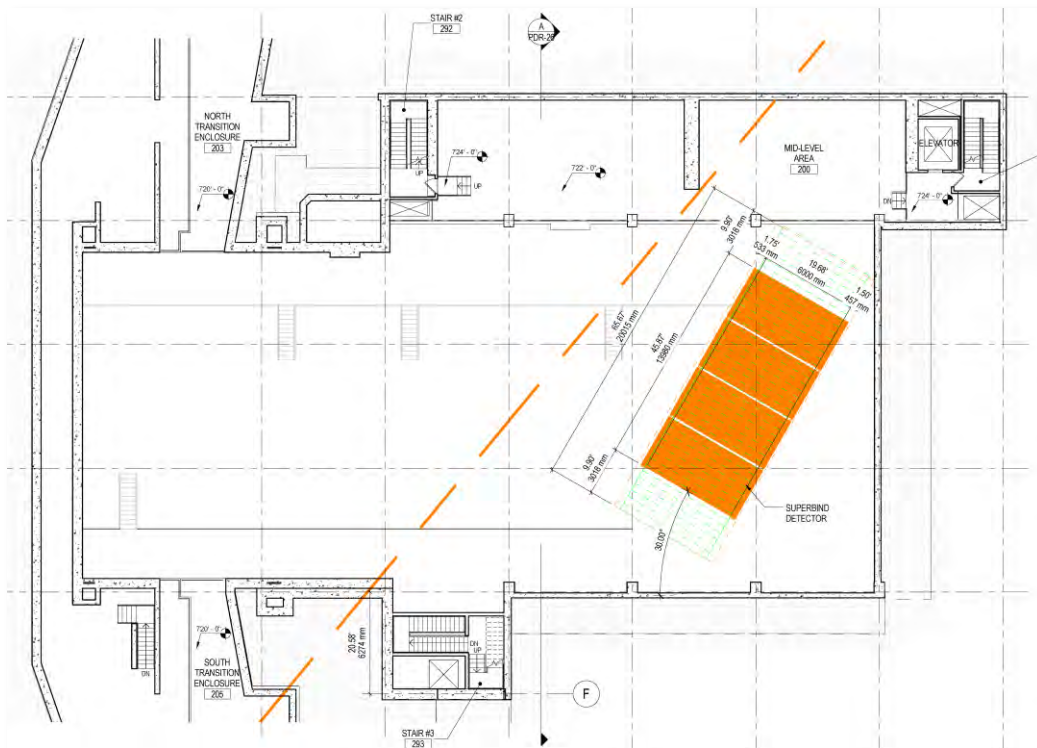


Figure 14 – Plan View of the nuSTORM Far Detector in the DZero Assembly Hall

For the purposes of this project definition report there is assumed to be minimal conventional facilities work required for the functional area. This includes the removal of existing Counting House and Control Room within the building. The technical components currently housed in these spaces are assumed to be removed by others prior to the start of the demolition work. Also included in this work scope is minor electrical rework associated with the demolition activities.



Area 7 – Site Work (WBS 8.0)

The seventh functional area is the site work and utilities required to support the nuSTORM project.

The location for the nuSTORM Conventional Facilities was selected based on the programmatic requirement for extraction of a proton beam from the existing Main Injector at the MI-40 Absorber. The location is adjacent to existing utilities serving the Main Injector including Industrial Cooling Water (ICW), Domestic Water Service (DWS), Low Conductivity Water (LCW), and electrical will be extended to serve the nuSTORM facilities.

Figure 15, below, depicts the overall site work required for the nuSTORM facilities. The existing Main Injector is at the upper portion of the figure (north is towards the top of the page), and the nuSTORM beamline is shown in orange.

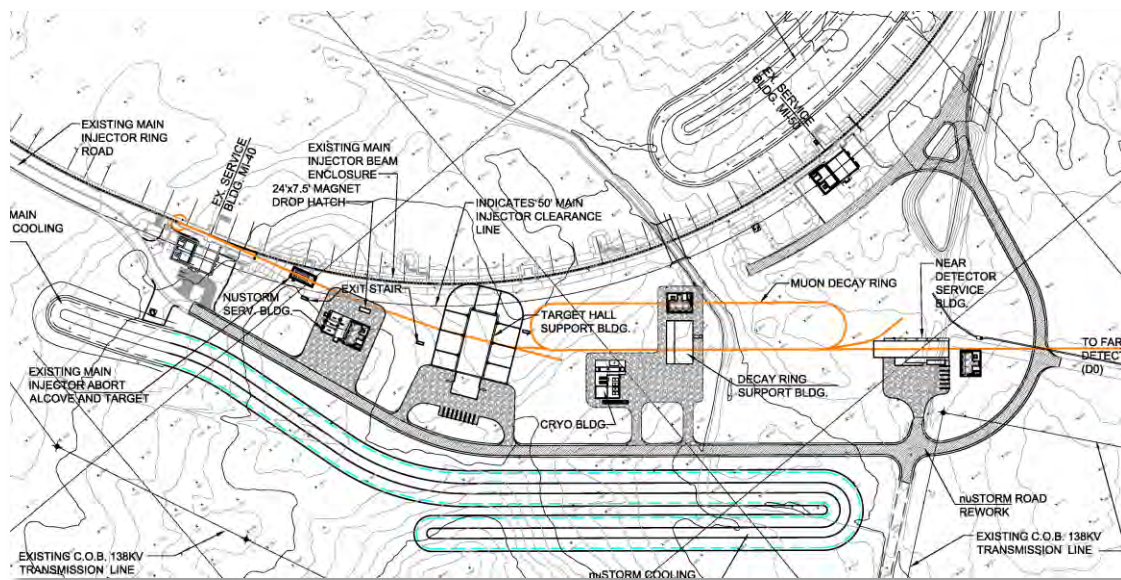


Figure 15 – Site Plan for nuSTORM Far Detector

The ICW, DWS and sanitary sewer services for the project will be extended from existing services originating at the MI-60 Service Building. Additionally, data and communication services will be extended from sources at the Main Injector. These services will be routed via a new utility corridor to the nuSTORM project site.

A new access road will provide access to the nuSTORM Conventional Facilities from existing Fermilab road network. This road will be constructed in a similar manner to



DETAILED DESCRIPTION**nuSTORM Conventional Facilities**

existing Fermilab roads and will be suitable for all weather access for assembly of the detector and normal operations.

Paved parking will be provided for five (5) vehicles at the each of the nuSTORM Service Buildings along with an unpaved gravel hardstand to provide a staging area during detector assembly and tanker trailer parking for liquid helium trailers during operation. A paved approach to the at-grade loading dock with suitable truck maneuvering space will be provided.

Earth shielding will be provided at below grade beamline enclosures in order to provide the equivalent of 21 feet of shielding for the Primary Beamline Enclosure and 12 feet at enclosures with secondary beams. The earthen berm with maintainable side slopes will be used where possible.

A new concrete encased power duct bank will be installed to connect the nuSTORM facilities to the existing Fermilab 13.8 kV electrical infrastructure system. This connection extends the existing electrical infrastructure from the Kautz Road Substation to the nuSTORM facilities.

The existing Pond C will be impacted by the construction of the nuSTORM facilities. A new pond will be constructed that restores the capacity of Pond C as well as increases the cooling capacity to accommodate the expected heat loads from the nuSTORM facility. This pond will be constructed in a similar style and manner to existing Main Injector ponds.

**Section
III**



SUGGESTED PROJECT BUDGET

nuSTORM Conventional Facilities

The nuSTORM Conventional Facilities project team developed a suggested project budget based on the preliminary design described in the drawings and Section III. The design drawings, detailed descriptions and resulting suggested project budget should be considered preliminary and based on the assumptions and requirements contained in Section II. As the programmatic requirements are refined the cost and schedule implications will also require refinement and adjustment.

Section IV

PART 1 COST SUMMARY

Listed below is a summary table of the costs associated with the scope of work described in this project definition report.

Base Cost	\$68,594,000
Engineering Design Inspection and Administration	\$20,579,000
Contingency/Management Reserve	\$47,200,000
Indirect Costs	\$11,977,000
TOTAL PROJECT COST \$148,350,000	

Demolition/Space Bank Offset	\$1,250,000
Engineering Design Inspection and Administration	\$375,000
Contingency/Management Reserve	\$486,000
Indirect Costs	\$415,000
OTHER PROJECT COSTS \$2,526,000	

The identified Other Project Costs include the costs associated with the space management costs required to demolish an equal amount of space to balance the new space created.

A further breakdown of the costs by the functional areas is listed below:

WBS	Functional Area	Base Cost	EDIA		Contingency		Indirects	Totals
			30%	%	\$			
1.0	Primary Beamline Enclosure	\$7,013,000	\$2,104,000	40%	\$3,647,000	\$1,266,000	\$14,030,000	
2.0	Target Station	\$8,993,000	\$2,698,000	55%	\$6,430,000	\$1,662,000	\$19,783,000	
3.0	Transport Line Enclosure	\$1,883,000	\$565,000	60%	\$1,469,000	\$504,000	\$4,421,000	
4.0	Muon Decay Ring Enclosure	\$26,002,000	\$7,801,000	60%	\$20,282,000	\$4,215,000	\$58,300,000	
5.0	Near Detector	\$11,750,000	\$3,525,000	40%	\$6,110,000	\$1,882,000	\$23,267,000	
6.0	Far Detector	\$720,000	\$216,000	55%	\$515,000	\$333,000	\$1,784,000	
8.0	Site Work	\$12,233,000	\$3,670,000	55%	\$8,747,000	\$2,115,000	\$26,765,000	
TOTALS		\$68,594,000	\$20,579,000		\$47,200,000	\$11,977,000	\$148,350,000	



Listed below are descriptions of the basic components used to develop the suggested project budget.

PART 2 METHODOLOGY

DOE Order 413.3-21 - DOE Guide 430.1-1X, DOE Cost Estimating Guide for Program and Project Management” was used as the basis for the development of the ICS.

Fiscal Year Dollars - The costs contained in this Project Definition Report are based on FY2013 dollars. Escalation adjustment to the above costs will need to be applied once a funding profile has been determined.

Cost Estimate Basis - The suggested project budget is based on cost data taken from Means Cost Estimating Guides, historical data and recent construction history at Fermilab. While the suggested project budget can provide input for the feasibility of the project, further design refinement will affect the final cost of the project.

High Performance Sustainable Building - Fermilab incorporates sustainable design principals into the planning, design and construction of projects. This direction is taken from the Fermilab Director’s Policy 3. The suggested project costs include the compliance with the DOE order of high performance (sustainable) building. In some instances, new facilities within the DOE complex achieve a “gold” level certification from the United States Green Building Council (USGBC) under the Leadership in Energy and Environmental Design (LEED) standards. It is recognized that the nuSTORM Conventional Facilities do not fall within the LEED criteria. While this project is not intended to become a certified building, the project processes and each project element will be evaluated during design to reduce their impact on natural resources without sacrificing program objectives. The project design will incorporate maintainability, aesthetics, environmental justice and program requirements to deliver a well-balanced project.

Space Management Requirements - Beginning in FY 2003, all new DOE Office of Science funded construction projects, including line items, GPP and IGPP, which provide new space, must have an equivalent amount of excess space allocated from the DOE Office of Science Space Bank. The identified Other Project Costs include the costs associated with the space management costs required to demolish an equal amount of space to balance the new space created.

Engineering, Design, Inspection and Administration - Project management, design, construction management, cost and schedule for the conventional construction portion of projects are typically the responsibility of the Facilities Engineering



SUGGESTED PROJECT BUDGET

nuSTORM Conventional Facilities

Services Section (FESS). This effort will be accomplished using the resources of the FESS Engineering Department supplemented with appropriate consultant resources.

Engineering Design and Inspection (ED&I) activities are included in the suggested project budgets. ED&I activities include the engineering and design activities in Preliminary and Final Design, the inspection activities associated with Construction Phase Support. The descriptions are based on DOE Directive G413.3-21, Chapter 6. Past historical data and DOE Directive G413.3-21, Section 5.4.3 indicates that 15%-25% of the construction cost is an appropriate range. Non-traditional, first of a kind projects may be higher, while simple construction such as buildings will be lower than this range. Generally, the more safety and regulatory intervention is involved, the higher the percentage.

Administration (A) activities includes those defined by DOE Directive G413.3-21, Section 5.4.3 as Project Management (PM) and Construction Management (CM). These costs range from 5%-15% of the other estimated project costs for most DOE projects, depending on the nature of the project and the scope of what is covered under project management.

For the purposes of this project definition report, the EDI and A functions have been combined. Listed below is a range of EDIA estimates for the life of the project:

6%-8%	Preliminary Design
8%-10%	Final Design
10%-12%	Construction Phase
2%-3%	Close Out Phase
=====	
26%-33%	Total Engineering, Design, Inspection and Administration

For the nuSTORM Conventional Facilities, a value of 30% was used in the suggested project budget calculations.

Management Reserve/Contingency - The application of risk-based contingency has been considered in the development of this project definition report. The contingency has been derived from a preliminary risk analysis of various aspects of the scope being estimated. This analysis takes into consideration budget, schedule, and technical risks as they apply to the project effort, underscoring the uncertainties that exist in each of the elements. The magnitude of the contingency estimate will depend on the status of planning, design, procurement, and construction, and the complexities and uncertainties of the operation or component parts of the project element. Part 4 below contains the preliminary risks identified with the conventional facilities at this stage of the project.



Indirect Costs - Indirect Costs rates are defined by DOE Order 4700.1 that states indirect costs are "...costs incurred by an organization for common or joint objectives and which cannot be identified specifically with a particular activity or project. ". The suggested costs above include Indirect Costs calculated at the current rate for projects as of October 30, 2012. As the project progresses, the Directorate Budget Office should be consulted for updated rates and procedures.

PART 3 COST ESTIMATE CLASSIFICATION

DOE Guide 430.1-1X, DOE Cost Estimating Guide for Program and Project Management" classifies cost estimates into one (1) of five (5) categories. These classifications are listed below:

Cost Estimate Classification	Primary Characteristics	
	Level of Definition (% of Complete Definition)	Cost Estimating Description (Techniques)
Class 5, Order of Magnitude	0% to 2%	Stochastic, most parametric, judgment (parametric, specific analogy, expert opinion, trend analysis)
Class 4, Intermediate	1% to 15%	Various, more parametric (parametric, specific analogy, expert opinion, trend analysis)
Class 3, Preliminary	10% to 40%	Various, including combinations (detailed, unit-cost, or activity-based; parametric; specific analogy; expert opinion; trend analysis)
Class 2, Intermediate	30% to 70%	Various, more definitive (detailed, unit-cost, or activity-based; expert opinion; learning curve)
Class 1, Definitive	50% to 100%	Deterministic, most definitive (detailed, unit-cost, or activity-based; expert opinion; learning curve)

These classifications are based on the Association for the Advanced of Cost Engineering (AACE) Recommended Practice No. 18R-97. These classifications help ensure that the quality of the cost estimate is appropriately considered when applying escalation and contingency.

The level of detail and accuracy of the budget becomes more definitive as the project's scope is refined. In a project's earliest phases, the Initiation, or Pre-Conceptual Phase (before Critical Decision [CD] -0, an Order-of-Magnitude (or Parametric) Estimate is usually required. When a capital asset acquisition project has completed the Conceptual Design Phase, a Preliminary Budget Range is required to



SUGGESTED PROJECT BUDGET

nuSTORM Conventional Facilities

establish the Budget Baseline at CD-1. Budget refinements shall be based on a Definitive Estimate for every element in the WBS and is required for CD-2.

The classification for the nuSTORM Conventional Facilities PDR is considered a Class 4 (Intermediate) based on the preliminary nature and level of definition of the programmatic requirements.

PART 4 **PRELIMINARY RISK IDENTIFICATION**

Contingency estimates are generally applied as a percentage of a particular cost or category of work. The PDR cost estimate is based on using the best available information to develop the expected cost, and then a risk analysis is performed to develop the required contingency budget based on risk probability and consequence. It is recognized that higher or lower contingency amounts are appropriate throughout the project based on an analysis of project complexity, technical characteristics, and associated risks. As part of the development of the suggested project budget, the project team has developed a preliminary list of high impact risks for the nuSTORM Conventional Facilities.

Risk #1 – Programmatic Requirements

The early stage of the project and the likely evolution of the programmatic requirements have the ability to significantly impact the cost and schedule for the conventional facilities.

Risk #2 – Subsurface Characteristics

The nuSTORM Conventional Facilities project is intended to be located on a portion of the Fermilab site with limited historic subsurface data. Experience at similar adjacent projects has been used as a basis of assumption for the development of this PDR. However, unknown subsurface conditions have the ability to impact the cost and schedule for the conventional facilities.

Section IV



Cost Details

- **Functional Area 1 – Primary Beamline Enclosure Cost Estimate**
- **Functional Area 2 – Target Station Cost Estimate**
- **Functional Area 3 – Transport Beamline Enclosure Cost Estimate**
- **Functional Area 4 – Muon Decay Ring Cost Estimate**
- **Functional Area 5 – Near Detector Cost Estimate**
- **Functional Area 6 – Far Detector Cost Estimate**
- **Functional Area 7 – Site Work Cost Estimate**
- **FY13 Provisional Labor, Indirect and Shop Rates**
- **Indirect Burden Allocation Policy and Methodology**

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT							\$7,013,000
Escalation							\$0
Subcontractor's Overhead and Profit		20.0%					\$1,169,000
Difficult Conditions (Construction at Main Injector)		10.0%					\$531,000
Subcontract Base Estimate							\$5,313,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:	Rev Date
<i>Fixed Priced Construction - Primary Beamline Enclosure</i>				6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT	
00	General				\$10,000		
01	Mobilize		1	lot	\$10,000.00	\$10,000	
02	Site Construction				\$1,695,000		
01	Silt Fence and Erosion control		1	Lot	\$50,000	\$50,000	
02	Strip Topsoil		1630	CY	\$6	\$9,778	
03	Haul Topsoil		2119	CY	\$7	\$14,830	
04	Excavate clays for Base Slab		32725	CY	\$15	\$490,875	
05	Haul Clays		42543	CY	\$7	\$297,798	
06	Stone Backfill		640	CY	\$32	\$20,480	
07	Haul and Backfill Clays		30918	CY	\$25	\$772,940	
08	Haul and spread topsoil		1630	CY	\$13	\$21,185	
09	Final Grading and seeding		1	Acre	\$23,800	\$17,484	
10	Support MI Duct Bank across excavation		0	Lot	\$45,000	\$0	
11	Support ICW piping across excavation		0	Lot	\$7,500	\$0	
03	Concrete				\$1,971,000		
01	Mud slab	<i>Enclosure</i>	71	CY	\$250	\$17,824.07	
02	Base Slab	<i>Enclosure</i>	570	CY	\$600	\$342,222.22	
03	Walls	<i>Enclosure</i>	596	CY	\$850	\$506,977.78	
04	Top Slab	<i>Enclosure</i>	463	CY	\$900	\$417,083.33	
05	Hatch Walls (7.5 x 24)	<i>Enclosure</i>	145	CY	\$900	\$130,784.00	
06	Hatch Shielding blocks	<i>Enclosure</i>	160	CY	\$1,100	\$176,000.00	
07	Stairs	<i>Enclosure</i>	2	Each	\$175,000	\$350,000.00	
08	FBP Footings						
	<i>Foundation - Walls</i>	<i>Service Bldg</i>	16	CY	\$325	\$5,200	
	<i>Column Pier - 24" - T/Pier 12" below grade</i>	<i>Service Bldg</i>	3	CY	\$325	\$975	
	<i>Footing - Continuous Wall - 12" x 2'-6"</i>	<i>Service Bldg</i>	16	CY	\$300	\$4,800	
	<i>Footing - Column Pier - 12" x 4'-0"</i>	<i>Service Bldg</i>	5	CY	\$300	\$1,500	
09	FBP Slab						
	<i>Granular Fill at Slab on Grade - 4"</i>	<i>Service Bldg</i>	24	CY	\$28	\$672	
	<i>2" Extruded Polystyrene Insulation Under Slab</i>	<i>Service Bldg</i>	1945	SF	\$1	\$2,334	
	<i>15 Mil Vapor Barrier Under Slab</i>	<i>Service Bldg</i>	1945	SF	\$0	\$584	
	<i>6" Concrete Slab w 6x6 WWF</i>	<i>Service Bldg</i>	1945	SF	\$5	\$9,628	
	<i>8" Concrete Housekeeping Slabs</i>	<i>Service Bldg</i>	1	LS	\$4,500	\$4,500	
04	Masonry				\$6,000		
01	Exterior Masonry Walls		450	SF	\$13	\$5,850	
05	Metals				\$72,000		
01	Misc. Metals						
	<i>Steel Girt Channels at Building Mid-Height</i>		4560	lbs.	\$3	\$11,400	
	<i>Metal Panel Support Angles</i>		2692	lbs.	\$3	\$6,730	
	<i>Steel Channel Opening Framing</i>		1560	lbs.	\$3	\$3,900	
02	Erect Structural Steel						
	<i>W12 Columns - Wide Flange</i>		6240	lbs.	\$3	\$15,600	
	<i>Beams and Girts- Wide Flange</i>		11258	lbs.	\$3	\$28,145	
05	Erect Roof Deck - 1 1/2" , 20 ga		2050	SF	\$3	\$6,458	

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT				\$7,013,000	
Escalation				\$0	
Subcontractor's Overhead and Profit	20.0%			\$1,169,000	
Difficult Conditions (Construction at Main Injector)	10.0%			\$531,000	
Subcontract Base Estimate				\$5,313,000	
nuSTORM Conventional Facilities					
<i>Fixed Priced Construction - Primary Beamline Enclosure</i>					
		Project No.	Status:	Date:	
		6-13-1	PDR	13-May-13	
				Rev Date	
				28-May-13	
ITEM NO.	DESCRIPTION OF WORK:	QUANTITY	UNITS	UNIT COST	AMOUNT
16	Electrical	\$720,000			
01	Cable Tray	1650	LF	\$74	\$122,100
02	Ground Wire	550	LF	\$18	\$9,900
03	Ground Rods	8	ea.	\$690	\$5,520
04	Unit heaters	2	ea.	\$870	\$1,740
05	Panels	1	lot	\$40,000	\$40,000
06	Fire Detection	5500	SF	\$6	\$33,000
07	Lighting	1	Lot	\$40,000	\$40,000
08	Electrical Distribution	1	Lot	\$100,000	\$100,000
09	Exterior Lighting	1	Lot	\$25,000	\$25,000
10	Install Switchboard	1	EA	\$62,500	\$62,500
11	Install 480 V Ductbank	60	LF	\$563	\$33,750
12	Install Transformers	1	EA	\$14,375	\$14,375
13	Install Ground Grid Wire	550	LF	\$18	\$9,625
14	Install Ground Rods	10	EA	\$690	\$6,900
15	Install Building Bond Connections	140	LF	\$179	\$25,069
16	Install Panel Feeders	1	LS	\$12,769	\$12,769
17	Install Distribution Circuits	1	LS	\$4,460	\$4,460
18	Install PP-208Y/120 VAC	1	EA	\$5,750	\$5,750
19	Install LP - 480Y/277 VAC	1	EA	\$10,844	\$10,844
20	Install 45 kVA, 480 - 208Y/277 VAC	1	EA	\$13,375	\$13,375
21	Install Welding Receptacles	6	EA	\$955	\$5,730
22	Install 120/208 VAC Receptacles	16	EA	\$239	\$3,820
23	Install Disconnect Switches	6	EA	\$540	\$3,240
24	Install Unit Heaters	4	EA	\$2,000	\$8,000
25	Connect Other mechanical Equipment	4	EA	\$2,000	\$8,000
26	Install Flour. Lighting	2200	SF	\$13	\$28,215
27	Install Emergency Lighting (UPS)	1	LS	\$13,875	\$13,875

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT							\$8,993,000
Escalation							\$0
Subcontractor's Overhead and Profit		20.0%					\$1,499,000
Difficult Conditions							\$0
Subcontract Base Estimate							\$7,494,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:	Rev Date
<i>Fixed Priced Construction - Target Station</i>				6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT	
00	General		\$10,000				
01	Mobilize		1	lot	\$10,000.00		\$10,000
02	Site Construction		\$760,000				
01	Silt Fence and Erosion control		1	Lot	\$50,000		\$50,000
02	Strip Topsoil		89	CY	\$6		\$534
03	Haul Topsoil		124	CY	\$7		\$868
04	Excavate clays for Base Slab		6098	CY	\$15		\$91,470
05	Excavate clays for Building		8958	CY	\$15		\$134,370
05	Haul Clays		21079	CY	\$7		\$147,553
06	Stone Backfill		201	CY	\$32		\$6,432
07	Haul and Backfill Clays		3500	CY	\$25		\$87,500
08	Haul and spread topsoil		50	CY	\$13		\$650
09	Final Grading and seeding		2	Acre	\$23,800		\$47,600
10	Backfill Along Building		7704	CY	\$25		\$192,600
03	Concrete		\$2,032,000				
01	Target Pile Mud Slab		9	CY	\$250		\$2,250
02	Target Pile Base Slab		111	CY	\$600		\$66,600
03	Target Pile Walls		302	CY	\$850		\$256,700
04	Lower Level Slabs		933	CY	\$850		\$793,050
05	Lower Level Walls		581	CY	\$600		\$348,600
06	Loading Dock Granular Base		56	CY	\$35		\$1,960
07	Loading Dock Slab		56	CY	\$500		\$28,000
08	Target Pile Shielding Blocks		100	CY	\$1,100		\$110,000
07	Stairs		2	Each	\$175,000		\$350,000
08	Foundations for At-Grade Building		100	CY	\$500		\$50,000
09	Slab for At-Grade Building		80	CY	\$250		\$20,000
10	8" Concrete Housekeeping Slabs		1	LS	\$4,500		\$4,500
04	Masonry		\$13,000				
01	Masonry Walls		1000	SF	\$13		\$13,000
05	Metals		\$564,000				
01	Mezzanine Columns		2400	lbs	3		\$7,200
02	Mezzanine beams		20400	lbs	3		\$61,200
03	Mezzanine metal deck		3000	SF	5		\$15,000
04	Crane Columns		10880	lbs	3		\$32,640
05	High Bay girders		64800	lbs	3		\$194,400
06	High Bay Roof beams		46080	lbs	3		\$138,240
07	Roof Deck		11520	SF	5		\$57,600
08	Crane Girders		44160	lbs	5		\$57,600
06	Wood and Plastic						\$0
							\$0
07	Thermal and Moisture Protection		\$1,401,000				
01	Damp Proof enclosure		15000	SF	\$8		\$120,000
02	Geo-Membrane at Target Chase		1	Lot	\$100,000		\$100,000

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT				\$8,993,000			
Escalation							\$0
Subcontractor's Overhead and Profit		20.0%					\$1,499,000
Difficult Conditions							\$0
Subcontract Base Estimate							\$7,494,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:	Rev Date
Fixed Priced Construction - Target Station				6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT	
02	Install Metal Siding <i>3" Centrica Formawall</i>		15120	SF	\$46	\$695,520	
03	Install Built-Up Roofing <i>2 Layers 1 1/2" Insulation, 1/2" Fiberboard, Ply Felt, White Marble Ballast</i>		9000	SF	\$18	\$162,000	
	4	<i>Tapered Insulation</i>	9000	SF	\$3	\$22,500	
04	Install Aluminum Coping		420	LF	\$15	\$6,300	
05	Architectural Treatment (10%)		1	Lot	\$110,000	\$110,000	
06	Guiding Principals Compliance (15%)		1	Lot	\$185,000	\$185,000	
08	Doors and Windows					\$51,000	
01	Enclosure Man doors 3 x 7		4	Each	\$1,400	\$5,600	
02	Install Exterior Man Doors <i>Single Insulated Hollow Metal Door and Frame</i>		2	Each	\$1,400	\$2,800	
	<i>Double Insulated Hollow Metal Door and Frame (6'x7')</i>		2	Each	\$1,800	\$3,600	
03	Install Interior Man Doors <i>Hollow Metal Door and Frame (3'x7')</i>		4	Each	\$1,200	\$4,800	
04	Install Overhead Door <i>Insulated Coil Door - 18'X14'</i>		2	Each	\$13,000	\$26,000	
05	Install Skylight/ daylighting		6	Each	\$1,400	\$8,400	
						\$0	
09	Finishes					\$108,000	
01	Painting		12000	SF	\$3	\$36,000	
02	Paint Exposed Ceiling		9000	SF	\$3	\$27,000	
03	Paint Structural Steel		1	Lot	\$20,000	\$20,000	
04	Paint Interior Walls		1	Lot	\$25,000	\$25,000	
						\$0	
10	Specialties					\$0	
						\$0	
14	Conveying Equipment					\$440,000	
01	40 Ton Overhead Bridge Crane <i>Standard Industrial Crane</i>		2	Each	\$180,000	\$360,000	
02	Install Bridge Crane		2	Lot	\$25,000	\$50,000	
03	Load Test Bridge Crane		2	Lot	\$15,000	\$30,000	

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT				\$8,993,000			
Escalation							\$0
Subcontractor's Overhead and Profit				20.0%			\$1,499,000
Difficult Conditions							\$0
Subcontract Base Estimate							\$7,494,000
nuSTORM Conventional Facilities <i>Fixed Priced Construction - Target Station</i>				Project No.	Status:	Date:	Rev Date
				6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:			QUANTITY	UNITS	UNIT COST	AMOUNT
15	Mechanical						\$0
01	Domestic Water			1	Lot	\$29,171	\$29,171
02	Plumbing Fixtures & Setting			1	Lot	\$7,452	\$7,452
03	Sanitary Waste & Vent						
	<i>Underground</i>			1	lot	\$21,238	\$21,238
	<i>Aboveground</i>			1	lot	\$25,143	\$25,143
06	Domestic Hot & Cold Water Insulation			1	lot	\$5,038	\$5,038
07	Outside Air Units Air Handling Units,			1	lot	\$212,845	\$212,845
08	Fans			1	lot	\$60,803	\$60,803
09	Chilled Water Piping			1	lot	\$95,493	\$95,493
10	Chilled Water Accessories			1	lot	\$28,720	\$28,720
11	Process Cooling Water Piping (ICW)			1	lot	\$34,203	\$34,203
12	Sheet Metal Ductwork			1	lot	\$100,200	\$100,200
13	Duct Accessories			1	lot	\$1,667	\$1,667
14	Supply, Return, Exhaust Registers			1	lot	\$2,227	\$2,227
15	Insulation			1	lot	\$77,639	\$77,639
16	Controls			1	lot	\$185,000	\$185,000
17	Install Fire Riser			1	lot	\$25,000	\$25,000
18	Install Pre Action Valve			1	lot	\$15,000	\$15,000
19	Install High Bay Sprinklers			9000	SF	\$8	\$72,000
20	Install Low Bay Sprinklers			4000	SF	\$8	\$32,000
20	Test Sprinklers			1	lot	\$5,000	\$5,000
16	Electrical						\$1,079,000
01	Cable Tray			1500	LF	\$74	\$111,000
02	Ground Wire			400	LF	\$18	\$7,200
03	Ground Rods			8	ea.	\$690	\$5,520
04	Unit heaters			2	ea.	\$870	\$1,740
05	Panels			1	lot	\$40,000	\$40,000
06	Fire Detection			9000	SF	\$6	\$54,000
07	Lighting			1	Lot	\$40,000	\$40,000
08	Electrical Distribution			9000	Lot	\$30	\$270,000
09	Exterior Lighting			1	Lot	\$50,000	\$50,000
10	Install Switchboard			2	EA	\$62,500	\$125,000
11	Install 480 V Ductbank			100	LF	\$563	\$56,250
12	Install Transformers			2	EA	\$14,375	\$28,750
13	Install Ground Grid Wire			400	LF	\$18	\$7,000
14	Install Ground Rods			8	EA	\$690	\$5,520
15	Install Building Bond Connections			250	LF	\$179	\$44,766
16	Install Panel Feeders			2	LS	\$12,769	\$25,538
17	Install Distribution Circuits			2	LS	\$4,460	\$8,920
18	Install PP-208Y/120 VAC			1	EA	\$5,750	\$5,750
19	Install LP - 480Y/277 VAC			1	EA	\$10,844	\$10,844
20	Install 45 kVA, 480 - 208Y/277 VAC			2	EA	\$13,375	\$26,750
21	Install Welding Receptacles			6	EA	\$955	\$5,730
22	Install 120/208 VAC Receptacles			16	EA	\$239	\$3,820
23	Install Disconnect Switches			6	EA	\$540	\$3,240
24	Install Unit Heaters			4	EA	\$2,000	\$8,000
25	Connect Other mechanical Equipment			4	EA	\$2,000	\$8,000
26	Install Flour. Lighting			2200	SF	\$13	\$28,215
27	Install Emergency Lighting (UPS)			1	LS	\$25,000	\$25,000

FERMILAB FESS COST ESTIMATE

		ESTIMATED SUBCONTRACT AWARD AMOUNT			\$1,883,000	
Escalation					\$0	
Subcontractor's Overhead and Profit		20.0%			\$314,000	
Difficult Conditions					\$0	
Subcontract Base Estimate					\$1,569,000	
nuSTORM Conventional Facilities			Project No.	Status:	Date:	Rev Date
<i>Fixed Priced Construction - Transport Line Enclosure</i>			6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT
00	General				\$9,000	
01	Mobilize		1	lot	\$9,000.00	\$9,000
02	Site Construction				\$272,000	
01	Silt Fence and Erosion control		1	Lot	\$10,000	\$10,000
02	Strip Topsoil		404	CY	\$6	\$2,422
03	Haul Topsoil		565	CY	\$7	\$3,956
04	Excavate clays for Base Slab		4998	CY	\$15	\$74,967
05	Haul Clays		6997	CY	\$7	\$48,978
06	Stone Backfill		179	CY	\$32	\$5,741
07	Haul and Backfill Clays		3768	CY	\$25	\$94,189
08	Haul and spread topsoil		135	CY	\$13	\$1,749
09	Final Grading and seeding		1	Acre	\$23,800	\$23,800
10	8' Topsoil Haul and Spread		100	CY	\$13	\$1,300
11	Seed and Landscaping		1	LS	\$5,000	\$5,000
03	Concrete				\$944,000	
01	Target to Ring Base Slab		174	CY	\$600	\$104,444
02	Target to Ring Walls		202	CY	\$850	\$171,889
03	Target to Ring top Slab		174	CY	\$900	\$156,667
04	Primary Abort Base Slab		111	CY	\$600	\$66,667
05	Primary Abort Walls		220	CY	\$850	\$187,000
06	Primary Abort Top Slab		105	CY	\$900	\$94,500
07	Primary Absorber Base Slab		90	CY	\$600	\$53,778
08	Primary Absorber walls		38	CY	\$850	\$32,262
09	Primary Absorber top Slab		85	CY	\$900	\$76,500
04	Masonry				\$0	
05	Metals				\$0	
06	Wood and Plastic				\$0	
07	Thermal and Moisture Protection				\$83,000	
01	Damp Proof enclosure		4152	SF	\$8	\$33,216
02	Geo-Membrane at Absorbers		1	Lot	\$50,000	\$50,000
08	Doors and Windows				\$3,000	
01	Enclosure Man doors 3 x 7		2	Each	\$1,400	\$2,800
						\$0
09	Finishes				\$11,000	
01	Painting		3633	SF	\$3	\$10,899
						\$0

FERMILAB FESS COST ESTIMATE

		ESTIMATED SUBCONTRACT AWARD AMOUNT				\$1,883,000
Escalation						\$0
Subcontractor's Overhead and Profit		20.0%				\$314,000
Difficult Conditions						\$0
Subcontract Base Estimate						\$1,569,000
nuSTORM Conventional Facilities			Project No.	Status:	Date:	Rev Date
<i>Fixed Priced Construction - Transport Line Enclosure</i>			6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT
10	Specialties					\$0
						\$0
14	Conveying Equipment		\$0			\$0
15	Mechanical		\$44,000			\$0
	01	Fans	1	Each	\$13,988	\$13,988
	06	Dehumidifiers	1	Each	\$30,000	\$30,000
16	Electrical		\$203,000			
	01	Cable Tray	519	LF	\$74	\$38,406
	02	Unit heaters	1	Each	\$870	\$870
	03	Panels	1	Each	\$40,000	\$40,000
	04	Fire Detection	1557	SF	\$6	\$9,342
	05	Lighting - Enclosure	1557	SF	\$13	\$20,241
	06	Lighting - Surface Building	425	SF	\$13	\$5,525
	07	Electrical Distribution - Enclosure	1557	Lot	\$10	\$15,570

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT				\$26,002,000			
Escalation							\$0
Subcontractor's Overhead and Profit				20.0%			\$4,334,000
Difficult Conditions							\$0
Subcontract Base Estimate							\$21,668,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:	Rev Date
<i>Fixed Priced Construction - Muon Decay Ring Enclosure</i>				6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:			QUANTITY	UNITS	UNIT COST	AMOUNT
00	General			\$10,000			
01	Mobilize			1	Lot	\$10,000.00	\$10,000
02	Site Construction			\$4,968,000			
01	Silt Fence and Erosion control	<i>Enclosure</i>		1	Lot	\$90,000	\$90,000
02	Strip Topsoil	<i>Enclosure</i>		7669	CY	\$6	\$46,016
03	Haul Topsoil	<i>Enclosure</i>		10738	CY	\$7	\$75,165
04	Excavate clays for Base Slab	<i>Enclosure</i>		94958	CY	\$15	\$1,424,373
05	Haul Clays	<i>Enclosure</i>		132941	CY	\$7	\$930,588
06	Stone Backfill	<i>Enclosure</i>		3409	CY	\$32	\$109,075
07	Haul and Backfill Clays	<i>Enclosure</i>		71583	CY	\$25	\$1,789,586
08	Haul and spread topsoil	<i>Enclosure</i>		2556	CY	\$13	\$33,234
09	Final Grading and seeding	<i>Enclosure</i>		8	Acre	\$23,800	\$180,880
10	Backfill Along Building	<i>Enclosure</i>		2500	CY	\$25	\$62,500
11	Transport Line Enclosure Excavation	<i>Enclosure</i>		1	Lot	\$30,000	\$30,000
12	Primary Absorber Enclosure Excavation	<i>Enclosure</i>		1	Lot	\$50,000	\$50,000
13	Pion Absorber Enclosure Excavation	<i>Enclosure</i>		1	Lot	\$30,000	\$30,000
14	Soil and Erosion Control	<i>Cyro Bldg</i>		1	LS	\$800	\$800
15	Paving, incl. stone base	<i>Cyro Bldg</i>		1588	SY	\$40	\$63,520
16	Dewar Tank Foundations	<i>Cyro Bldg</i>		1	LS	\$22,000	\$22,000
17	Pads for tanks	<i>Cyro Bldg</i>		1	LS	\$7,500	\$7,500
18	Clear and Grub	<i>Cyro Bldg</i>		1	LS	\$200	\$200
19	Excavate Topsoil	<i>Cyro Bldg</i>		220	CY	\$6	\$1,320
20	Haul and Stockpile Topsoil	<i>Cyro Bldg</i>		277	CY	\$7	\$1,939
21	Excavate for Footings	<i>Cyro Bldg</i>		350	CY	\$22	\$7,700
22	Haul and Stockpile	<i>Cyro Bldg</i>		438	CY	\$7	\$3,066
23	8' Topsoil Haul and Spread	<i>Cyro Bldg</i>		100	CY	\$13	\$1,300
24	Seed and Landscaping	<i>Cyro Bldg</i>		1	LS	\$7,500	\$7,500
03	Concrete			\$7,952,000			
01	Mud Slab	<i>Enclosure</i>		352	CY	\$250	\$88,000
02	Base Slab	<i>Enclosure</i>		2819	CY	\$600	\$1,691,400
03	Walls	<i>Enclosure</i>		3283	CY	\$850	\$2,790,550
04	Top Slab	<i>Enclosure</i>		2462	CY	\$900	\$2,215,800
05	Hatch Walls	<i>Enclosure</i>		61	CY	\$850	\$51,850
06	Hatch Shielding Blocks (1.5'x12'x15')	<i>Enclosure</i>		120	CY	\$1,100	\$132,000
07	side passageways 86' lg x 2	<i>Enclosure</i>		239	CY	\$750	\$179,167
08	center passageway	<i>Enclosure</i>		268	CY	\$750	\$200,667
18	Pion Absorber Base Slab	<i>Enclosure</i>		45	CY	\$600	\$27,000
19	Pion Absorber walls	<i>Enclosure</i>		20	CY	\$850	\$17,000
20	Pion Absorber top Slab	<i>Enclosure</i>		40	CY	\$900	\$36,000
21	Stairs	<i>Enclosure</i>		2	Each	\$175,000	\$350,000
22	Foundations for At-Grade Building	<i>Service Bldg</i>		200	CY	\$500	\$100,000
23	Slab for At-Grade Building	<i>Service Bldg</i>		150	CY	\$250	\$37,500
24	8" Concrete Housekeeping Slabs	<i>Service Bldg</i>		1	LS	\$4,500	\$4,500
25	FBP Footings						\$0
	<i>Foundation - Walls</i>	<i>Cyro Bldg</i>		16	cy	\$325	\$5,200
	<i>Column Pier - 24" - T/Pier 12" below grade</i>	<i>Cyro Bldg</i>		3	cy	\$325	\$975
	<i>Footing - Continuous Wall - 12" x 2'-6"</i>	<i>Cyro Bldg</i>		16	cy	\$300	\$4,800
	<i>Footing - Column Pier - 12" x 4'-0"</i>	<i>Cyro Bldg</i>		5	cy	\$300	\$1,500
26	FBP Slab						\$0
	<i>Granular Fill at Slab on Grade - 4"</i>	<i>Cyro Bldg</i>		24	cy	\$28	\$672
	<i>2" Extruded Polystyrene Insulation Under Slab</i>	<i>Cyro Bldg</i>		1945	sf	\$1	\$2,334

FERMILAB FESS COST ESTIMATE

				ESTIMATED SUBCONTRACT AWARD AMOUNT		\$26,002,000
Escalation						\$0
Subcontractor's Overhead and Profit				20.0%		\$4,334,000
Difficult Conditions						\$0
Subcontract Base Estimate						\$21,668,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:
<i>Fixed Priced Construction - Muon Decay Ring Enclosure</i>				6-13-1	PDR	13-May-13
ITEM NO.	DESCRIPTION OF WORK:			QUANTITY	UNITS	UNIT COST
		<i>15 Mil Vapor Barrier Under Slab</i>	<i>Cyro Bldg</i>	1945	sf	\$0
		<i>6" Concrete Slab w 6x6 WWF</i>	<i>Cyro Bldg</i>	1945	sf	\$5
		<i>8" Concrete Housekeeping Slabs</i>	<i>Cyro Bldg</i>	1	LS	\$4,500
04	Masonry			\$32,000		
	01	Masonry Walls	<i>Service Bldg</i>	2000	SF	\$13
	02	Masonry Walls	<i>Cyro Bldg</i>	450	SF	\$13
05	Metals			\$3,643,000		
	01	High Bay Building (SF Cost)	<i>Service Bldg</i>	7500	SF	400
	02	Low Bay Building (SF Cost)	<i>Service Bldg</i>	1000	SF	350
	03	Crane Girders	<i>Service Bldg</i>	44160	lbs	5
	04	Misc. Metals				
		<i>Steel Girt Channels at Building Mid-Height</i>	<i>Cyro Bldg</i>	4560	lbs.	\$3
		<i>Metal Panel Support Angles</i>	<i>Cyro Bldg</i>	2692	lbs.	\$3
		<i>Steel Channel Opening Framing</i>	<i>Cyro Bldg</i>	1560	lbs.	\$3
	05	Erect Structural Steel				
		<i>W12 Columns - Wide Flange</i>	<i>Cyro Bldg</i>	6240	lbs.	\$3
		<i>Beams and Girts- Wide Flange</i>	<i>Cyro Bldg</i>	11258	lbs.	\$3
	06	Erect Roof Deck	<i>Cyro Bldg</i>	2050	sf	\$3
06	Wood and Plastic					\$0
						\$0
07	Thermal and Moisture Protection			\$1,218,000		
	01	Damp Proof enclosure	<i>Enclosure</i>	78888	SF	\$8
	02	Geo-Membrane at Absorbers	<i>Enclosure</i>	1	Lot	\$50,000
	03	Install Metal Siding				
		<i>3" Centrica Formawall</i>	<i>Cyro Bldg</i>	3180	sf	\$46
	04	Install Built-Up Roofing				\$0
		<i>2 Layers 1 1/2" Insulation, 1/2" Fiberboard, Ply Felt, White Marble Ballast</i>	<i>Cyro Bldg</i>	2050	sf	\$18
		<i>Tapered Insulation</i>	<i>Cyro Bldg</i>	240	sf	\$3
	05	Install Aluminum Coping	<i>Cyro Bldg</i>	220	lf	\$15
	06	Architectural Treatment (10%)	<i>Service Bldg</i>	1	Lot	\$150,000
	07	Guiding Principals Compliance (15%)	<i>Service Bldg</i>	1	Lot	\$200,000
08	Doors and Windows			\$96,000		
	01	Enclosure Man doors 3 x 7	<i>Enclosure</i>	7	Each	\$1,400
	02	Install Exterior Man Doors	<i>Service Bldg</i>			
		<i>Single Insulated Hollow Metal Door and Frame</i>		2	Each	\$1,400
		<i>Double Insulated Hollow Metal Door and Frame (6'x7')</i>		2	Each	\$1,800
	03	Install Interior Man Doors	<i>Service Bldg</i>			
		<i>Hollow Metal Door and Frame (3'x7')</i>		4	Each	\$1,200
	04	Install Overhead Door	<i>Service Bldg</i>			
		<i>Insulated Coil Door - 18'X14'</i>		2	Each	\$13,000
	05	Install Skylight/ daylighting	<i>Service Bldg</i>	6	Each	\$1,400
	06	Install Exterior Man Doors				\$0
		<i>Single Insulated Hollow Metal Door and Frame</i>	<i>Cyro Bldg</i>	2	Each	\$1,400
		<i>Double Insulated Hollow Metal Door and Frame (6'x7')</i>	<i>Cyro Bldg</i>	1	Each	\$1,800
	07	Install Interior Man Doors		1	Each	\$1,200
		<i>Hollow Metal Door and Frame (3'x7')</i>	<i>Cyro Bldg</i>			\$0
	08	Install Overhead Door		2	Each	\$13,000
		<i>Insulated Coil Door - 18'X14'</i>	<i>Cyro Bldg</i>			\$0
	09	Install Skylight/ daylighting	<i>Cyro Bldg</i>	6	Each	\$1,400
						\$0

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT				\$26,002,000			
Escalation						\$0	
Subcontractor's Overhead and Profit				20.0%		\$4,334,000	
Difficult Conditions						\$0	
Subcontract Base Estimate						\$21,668,000	
nuSTORM Conventional Facilities				Project No.	Status:	Date:	Rev Date
				<i>Fixed Priced Construction - Muon Decay Ring Enclosure</i>			
ITEM NO.	DESCRIPTION OF WORK:			QUANTITY	UNITS	UNIT COST	AMOUNT
16	Electrical			\$2,137,000			
01	Cable Tray	Enclosure	4931	LF	\$74	\$364,857	
02	Unit heaters	Enclosure	9	Each	\$870	\$7,830	
03	Panels	Enclosure	2	Each	\$40,000	\$80,000	
04	Fire Detection - Surface Building	Service Bldg	9000	SF	\$6	\$54,000	
05	Lighting - Enclosure	Enclosure	31140	SF	\$13	\$404,820	
06	Lighting - Surface Building	Service Bldg	8500	SF	\$13	\$110,500	
07	Electrical Distribution - Enclosure	Enclosure	29583	Lot	\$10	\$295,830	
08	Exterior Lighting	Service Bldg	1	Lot	\$50,000	\$50,000	
09	Install Switchboard	Service Bldg	2	EA	\$62,500	\$125,000	
10	Install 480 V Ductbank	Service Bldg	100	LF	\$563	\$56,250	
11	Install Transformers	Service Bldg	2	EA	\$14,375	\$28,750	
12	Install Generator	Service Bldg	1	Each	\$20,000	\$20,000	
13	Install Ground Grid Wire	Service Bldg	400	LF	\$18	\$7,000	
14	Install Ground Rods	Service Bldg	8	Each	\$690	\$5,520	
15	Install Building Bond Connections	Service Bldg	250	LF	\$179	\$44,766	
16	Install Panel Feeders	Service Bldg	2	LS	\$12,769	\$25,538	
17	Install Distribution Circuits	Service Bldg	2	LS	\$4,460	\$8,920	
18	Install PP-208Y/120 VAC	Service Bldg	1	Each	\$5,750	\$5,750	
19	Install LP - 480Y/277 VAC	Service Bldg	1	Each	\$10,844	\$10,844	
20	Install 45 kVA, 480 - 208Y/277 VAC	Service Bldg	2	Each	\$13,375	\$26,750	
21	Install Welding Receptacles	Service Bldg	6	Each	\$955	\$5,730	
22	Install 120/208 VAC Receptacles	Service Bldg	16	Each	\$239	\$3,820	
23	Install Disconnect Switches	Service Bldg	6	Each	\$540	\$3,240	
24	Install Unit Heaters	Service Bldg	4	Each	\$2,000	\$8,000	
25	Connect Other mechanical Equipment	Service Bldg	4	Each	\$2,000	\$8,000	
26	Install Emergency Lighting (UPS)	Service Bldg	1	LS	\$25,000	\$25,000	
27	Install Switchboard	Cyro Bldg	1	Each	\$62,500	\$62,500	
28	Install 480 V Ductbank	Cyro Bldg	60	LF	\$563	\$33,750	
29	Install Transformers	Cyro Bldg	1	Each	\$14,375	\$14,375	
30	Install Ground Grid Wire	Cyro Bldg	400	LF	\$18	\$7,000	
31	Install Ground Rods	Cyro Bldg	8	Each	\$690	\$5,520	
32	Install Building Bond Connections	Cyro Bldg	140	LF	\$179	\$25,069	
33	Install Panel Feeders	Cyro Bldg	1	LS	\$12,769	\$12,769	
34	Install Distribution Circuits	Cyro Bldg	1	LS	\$4,460	\$4,460	
35	Install PP-208Y/120 VAC	Cyro Bldg	1	Each	\$5,750	\$5,750	
36	Install LP - 480Y/277 VAC	Cyro Bldg	1	Each	\$10,844	\$10,844	
37	Install 45 kVA, 480 - 208Y/277 VAC	Cyro Bldg	1	Each	\$13,375	\$13,375	
38	Install Welding Receptacles	Cyro Bldg	4	Each	\$955	\$3,820	
39	Install 120/208 VAC Receptacles	Cyro Bldg	16	Each	\$239	\$3,820	
40	Install Disconnect Switches	Cyro Bldg	6	Each	\$540	\$3,240	
41	Install Unit Heaters	Cyro Bldg	4	Each	\$863	\$3,450	
42	Connect Other mechanical Equipment	Cyro Bldg	4	Each	\$863	\$3,450	
43	Install Flour. Lighting	Cyro Bldg	1950	SF	\$13	\$25,009	
44	Install Emergency Lighting (UPS)	Cyro Bldg	1	LS	\$13,875	\$13,875	
45	Install Exterior Lighting	Cyro Bldg	4	Each	\$656	\$2,625	
46	Install Fire Detection	Cyro Bldg	1950	SF	\$12	\$23,400	

FERMILAB FESS COST ESTIMATE

			ESTIMATED SUBCONTRACT AWARD AMOUNT	\$11,750,000			
Escalation							\$0
Subcontractor's Overhead and Profit			20.0%				\$1,958,000
Difficult Conditions							\$0
Subcontract Base Estimate							\$9,792,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:	Rev Date
<i>Fixed Priced Construction - Near Detector</i>				6-13-1	PDR	13-May-13	28-May-13
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT	
00	General						\$10,000
01	Mobilize		1	lot	\$10,000.00		\$10,000
02	Site Construction						\$885,000
01	Silt Fence and Erosion control		1	Lot	\$50,000		\$50,000
02	Strip Topsoil		556	CY	\$6		\$3,336
03	Haul Topsoil		778	CY	\$7		\$5,446
04	Excavate clays for Below Grade Enclosure		17630	CY	\$15		\$264,450
05	Haul Clays		24681	CY	\$7		\$172,767
06	Stone Backfill		3111	CY	\$32		\$99,552
07	Haul and Backfill Clays		9528	CY	\$25		\$238,200
08	Haul and spread topsoil		300	CY	\$13		\$3,900
09	Final Grading and seeding		2	Acre	\$23,800		\$47,600
03	Concrete						\$3,246,000
01	Mud Slab		58	CY	\$250		\$14,500
02	Base Slab		810	CY	\$600		\$486,000
03	Lower Walls		718	CY	\$850		\$610,300
04	Upper Walls		227	CY	\$850		\$226,667
05	Counterfort		267	CY	\$900		\$240,000
06	Top Slab between counterforts		267	CY	\$900		\$240,000
07	Hatch Shielding blocks		584	CY	\$1,100		\$642,400
08	Stairs		2	Each	\$175,000		\$350,000
09	Elevator Wall and pit		57	CY	\$900		\$51,200
10	Slab on grade Loading dock						
	<i>Granular Fill at Slab on Grade - 4"</i>		64	cy	\$28		\$1,792
	<i>2" Extruded Polystyrene Insulation Under Slab</i>		1728	sf	\$1		\$2,074
	<i>15 Mil Vapor Barrier Under Slab</i>		1728	sf	\$0		\$518
	<i>5" Concrete Slab w 6x6 WWF</i>		1728	sf	\$12		\$20,736
16	Slab on grade side bay						
	<i>Granular Fill at Slab on Grade - 4"</i>		2	cy	\$28		\$47
	<i>2" Extruded Polystyrene Insulation Under Slab</i>		90	sf	\$1		\$108
	<i>15 Mil Vapor Barrier Under Slab</i>		90	sf	\$0		\$27
	<i>5" Concrete Slab w 6x6 WWF</i>		90	sf	\$12		\$1,080
21	Top Level Substructure						
	<i>Spread Footings</i>		21	cy	\$700		\$14,933
	<i>Drilled Piers</i>		7	Ea	\$1,800		\$12,600
	<i>Strip Footings/Foundation Walls</i>		414	cy	\$800		\$331,200
04	Masonry						\$23,000
01	Masonry Walls		1800	SF	\$13		\$23,400
05	Metals						\$1,121,000
01	Crane Columns		40960	Lbs	\$3		\$122,880
02	Side Columns		140000	Lbs	\$3		\$420,000
03	Girts		1	Lot	\$40,000		\$40,000
04	Second Floor Structure		5000	SF	\$40		\$200,000
05	Premium girts for CA siding		1	Lot	\$30,000		\$30,000
06	Roof Girders High Bay		30400	Lbs	\$3		\$91,200

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT							\$11,750,000	
Escalation							\$0	
Subcontractor's Overhead and Profit							20.0%	
Difficult Conditions							\$0	
Subcontract Base Estimate							\$9,792,000	
nuSTORM Conventional Facilities					Project No.	Status:	Date:	
<i>Fixed Priced Construction - Near Detector</i>					6-13-1	PDR	13-May-13	
							Rev Date	
							28-May-13	
ITEM NO.	DESCRIPTION OF WORK:				QUANTITY	UNITS	UNIT COST	AMOUNT
07	Roof Beam High Bay				23520	Lbs	\$3	\$70,560
08	Crane Beam				38304	Lbs	\$3	\$114,912
09	Erect Roof Deck				8664	SF	\$3	\$25,992
10	Guardrails				268	LF	\$21	\$5,628
06	Wood and Plastic							\$0
								\$0
07	Thermal and Moisture Protection							\$1,687,000
01	Damp Proof enclosure				20000	SF	\$8	\$160,000
03	Install Metal Siding							
	3" Centrica Formawall				13696	sf	\$79	\$1,081,984
04	Install Built-Up Roofing							\$0
	2 Layers 1 1/2" Insulation, 1/2" Fiberboard, Ply Felt, White Marble Ballast				8664	sf	\$18	\$155,952
	Tapered Insulation				2166	sf	\$3	\$5,415
05	Install Aluminum Coping				548	lf	\$15	\$8,220
06	Architectural Treatment (10%)				1	Lot	\$125,000	\$125,000
07	Guiding Principals Compliance (15%)				1	Lot	\$150,000	\$150,000
08	Doors and Windows							\$51,000
01	Enclosure Man doors 3 x 7				4	Each	\$1,400	\$5,600
02	Install Exterior Man Doors							
	Single Insulated Hollow Metal Door and Frame				5	Each	\$1,400	\$7,000
	Double Insulated Hollow Metal Door and Frame (6'x7')				3	Each	\$1,800	\$5,400
03	Install Interior Man Doors							
	Hollow Metal Door and Frame (3'x7')				10	Each	\$1,200	\$12,000
04	Install Overhead Door							
	Insulated Coil Door - 18'X14'				1	Each	\$13,000	\$13,000
05	Install Skylight/ daylighting				6	Each	\$1,400	\$8,400
								\$0
09	Finishes							\$0
01	Painting				20000	SF	\$3	\$60,000
02	Paint Exposed Ceiling				10000	SF	\$3	\$30,000
03	Paint Structural Steel				1	Lot	\$20,000	\$20,000
04	Paint Interior Walls				1	Lot	\$25,000	\$25,000
								\$0
10	Specialties							\$0
								\$0
14	Conveying Equipment							\$0
01	30 Ton Overhead Bridge Crane				2	Each	\$140,000	\$280,000
	Standard Industrial Crane							
02	Install Bridge Crane				2	Lot	\$25,000	\$50,000
03	Load Test Bridge Crane				2	Lot	\$15,000	\$30,000
04	Elevator				1	Each	\$165,000	\$165,000

FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT				\$11,750,000			
Escalation						\$0	
Subcontractor's Overhead and Profit				20.0%		\$1,958,000	
Difficult Conditions						\$0	
Subcontract Base Estimate						\$9,792,000	
nuSTORM Conventional Facilities				Project No.	Status:	Date:	
<i>Fixed Priced Construction - Near Detector</i>				6-13-1	PDR	13-May-13	
Rev Date							
28-May-13							
ITEM NO.	DESCRIPTION OF WORK:			QUANTITY	UNITS	UNIT COST	AMOUNT
15	Mechanical			\$1,143,000			\$0
01	Domestic Water			1	Lot	\$30,000	\$30,000
02	Plumbing Fixtures & Setting			1	Lot	\$10,000	\$10,000
03	Sanitary Waste & Vent						
	<i>Underground</i>			1	lot	\$21,238	\$21,238
	<i>Aboveground</i>			1	lot	\$25,143	\$25,143
04	Domestic Hot & Cold Water Insulation			1	lot	\$5,038	\$5,038
05	Outside Air Units Air Handling Units,			1	lot	\$212,845	\$212,845
06	Fans			4	Each	\$13,988	\$55,952
07	Chilled Water Piping			1	lot	\$95,493	\$95,493
08	Chilled Water Accessories			1	lot	\$28,720	\$28,720
09	Process Cooling Water Piping (ICW)			1	lot	\$34,203	\$34,203
10	Sheet Metal Ductwork			1	lot	\$100,200	\$100,200
11	Duct Accessories			1	lot	\$1,667	\$1,667
12	Supply, Return, Exhaust Registers			1	lot	\$2,227	\$2,227
13	Insulation			1	lot	\$77,639	\$77,639
14	Controls			1	lot	\$185,000	\$185,000
15	Install Fire Riser			1	lot	\$50,000	\$50,000
16	Install Pre Action Valve			1	lot	\$15,000	\$15,000
17	Install High Bay Sprinklers			7500	SF	\$8	\$60,000
18	Install Low Bay Sprinklers			1000	SF	\$8	\$8,000
19	Test Sprinklers			1	lot	\$5,000	\$5,000
20	Dehumidifiers			4	Each	\$30,000	\$120,000
16	Electrical			\$966,000			
02	Unit heaters			10	Each	\$870	\$8,700
03	Panels			2	Each	\$40,000	\$80,000
04	Fire Detection - Surface Building			8000	SF	\$6	\$48,000
05	Lighting - Below Grade			8000	SF	\$13	\$104,000
06	Lighting - Surface Building			8000	SF	\$13	\$104,000
07	Electrical Distribution - Below Grade			8000	Lot	\$10	\$80,000
08	Exterior Lighting			1	Lot	\$50,000	\$50,000
09	Install Switchboard			2	EA	\$62,500	\$125,000
10	Install 480 V Ductbank			100	LF	\$563	\$56,250
11	Install Transformers			2	EA	\$14,375	\$28,750
12	Install Generator			1	Each	\$20,000	\$20,000
13	Install Ground Grid Wire			400	LF	\$18	\$7,000
14	Install Ground Rods			8	Each	\$690	\$5,520
15	Install Building Bond Connections			250	LF	\$179	\$44,766
16	Install Panel Feeders			2	LS	\$12,769	\$25,538
17	Install Distribution Circuits			2	LS	\$4,460	\$8,920
18	Install PP-208Y/120 VAC			1	Each	\$5,750	\$5,750
19	Install LP - 480Y/277 VAC			1	Each	\$10,844	\$10,844
20	Install 45 kVA, 480 - 208Y/277 VAC			2	Each	\$13,375	\$26,750
21	Install Welding Receptacles			6	Each	\$955	\$5,730
22	Install 120/208 VAC Receptacles			16	Each	\$239	\$3,820
23	Install Disconnect Switches			6	Each	\$540	\$3,240
24	Install Unit Heaters			4	Each	\$2,000	\$8,000
25	Connect Other mechanical Equipment			4	Each	\$2,000	\$8,000
26	Install Emergency Lighting (UPS)			1	LS	\$25,000	\$25,000

FERMILAB FESS COST ESTIMATE

			ESTIMATED SUBCONTRACT AWARD AMOUNT		\$720,000	
Escalation						\$0
Subcontractor's Overhead and Profit			20.0%			\$120,000
Difficult Conditions			10.0%			\$55,000
Subcontract Base Estimate						\$545,000
nuSTORM Conventional Facilities			Project No.	Status:	Date:	Rev Date
			<i>Fixed Priced Construction - Far Detector</i>			6-13-1
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT
00	General					\$120,000
01	Mobilize		1	Lot	\$5,000	\$5,000
02	Demolish/Remove Existing Counting House		1	Lot	\$65,000	\$65,000
03	Demolish/Remove Existing Clean Room		1	Lot	\$50,000	\$50,000
						\$0
02	Civil					\$0
03	Concrete					\$0
						\$0
04	Masonry					\$0
						\$0
05	Metals					\$0
						\$0
06	Wood and Plastic					\$0
						\$0
07	Thermal and Moisture Protection					\$0
08	Doors and Windows					\$0
						\$0
09	Finishes					\$0
						\$0
10	Specialties					\$0
						\$0
14	Conveying Equipment					\$0
						\$0
15	Mechanical					\$350,000
01	Cooling Tower System		1	Lot	\$350,000	\$350,000
	<i>Sized for two cyro compressors</i>					\$0
	<i>Based on AZero System for mu2e</i>					\$0
	<i>Includes water treatment system</i>					
16	Electrical					\$75,000
01	Electrical Service Extension to Detector		1	Lot	\$75,000	\$75,000
						\$0

FERMILAB FESS COST ESTIMATE

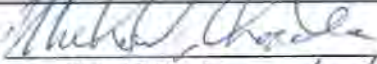
ESTIMATED SUBCONTRACT AWARD AMOUNT						\$12,233,000
Escalation						\$0
Subcontractor's Overhead and Profit		20.0%				\$2,039,000
Difficult Conditions						\$0
Subcontract Base Estimate						\$10,194,000
nuSTORM Conventional Facilities				Project No.	Status:	Date:
<i>Fixed Priced Construction - Site Work</i>				6-13-1	PDR	13-May-13
Rev Date	28-May-13					
ITEM NO.	DESCRIPTION OF WORK:		QUANTITY	UNITS	UNIT COST	AMOUNT
00	General		\$260,000			
01	Mobilize		1	Lot	\$10,000	\$10,000
02	Wetland Permits		1	Lot	\$100,000	\$100,000
03	Wetland Mitigation		1	Lot	\$150,000	\$150,000
						\$0
02	Civil		\$6,778,000			
01	Silt Fence and Erosion Control Measures		9,750	LF	\$8	\$78,000
02	Roads					
	<i>Strip and haul soils</i>		5,556	CY	\$12	\$66,667
	<i>Aggregate Base</i>		5000	SF	\$3	\$15,000
	<i>Binder and surface course</i>		60000	SF	\$2	\$120,000
03	Drives and parking					
	<i>Strip and haul soils</i>		9,574	SF	\$2	\$517,000
	<i>Aggregate Base</i>		258500	SF	\$3	\$775,500
	<i>Binder and surface course</i>		258500	SF	\$2	\$517,000
04	Hardstands		1667	CY	\$30	\$50,000
05	Ponds					
	<i>Excavate for ponds</i>		39000	CY	\$15	\$585,000
	<i>Liner</i>		198900	SF	\$8	\$1,591,200
	<i>12" clay over liner</i>		7540	CY	\$25	\$188,500
	<i>Stone banks</i>		867	CY	\$85	\$73,667
	<i>Pumps and pump station</i>		2	Each	\$400,000	\$800,000
	<i>Intake and discharge structures</i>		4	Each	\$40,000	\$160,000
	<i>Pressure Piping 12' HDPE</i>		1200	LF	\$140	\$168,000
	<i>Gravity Piping</i>		750	LF	\$110	\$82,500
06	Creek Diversion		1	Lot	\$50,000	\$50,000
07	Piped utilities					
	<i>ICW 10" Main</i>		2700	LF	\$60	\$162,000
	<i>ICW 6" Laterals</i>		240	LF	\$45	\$10,800
	<i>DWS</i>		2700	LF	\$45	\$121,500
	<i>Sanitary Sewer</i>		4600	LF	\$35	\$161,000
	<i>Sanitary Lift Stations</i>		2	Each	\$40,000	\$80,000
	<i>Hydrants</i>		10	Each	\$2,500	\$25,000
	<i>Valves and fittings</i>		45	Each	\$1,000	\$45,000
08	Storm Drainage Structures		1	Lot	\$100,000	\$100,000
09	Seeding and Landscaping		23.5	Acres	\$10,000	\$235,000
03	Concrete		\$350,000			
01	Substation Pads with Containment		5	Each	\$50,000	\$250,000
02	Walks and Aprons		200	CY	\$500	\$100,000
						\$0


FERMILAB FESS COST ESTIMATE

ESTIMATED SUBCONTRACT AWARD AMOUNT							\$12,233,000
Escalation							\$0
Subcontractor's Overhead and Profit		20.0%					\$2,039,000
Difficult Conditions							\$0
Subcontract Base Estimate							\$10,194,000
nuSTORM Conventional Facilities			Project No.	Status:	Date:	Rev Date	
<i>Fixed Priced Construction - Site Work</i>			6-13-1	PDR	13-May-13	28-May-13	
04	Masonry	\$0					
							\$0
05	Metals						
							\$0
06	Wood and Plastic						
							\$0
07	Thermal and Moisture Protection						
							\$0
09	Finishes						
							\$0
10	Specialties						
							\$0
14	Conveying Equipment						
							\$0
15	Mechanical	\$0					
16	Electrical	\$2,806,000					
	01 Temp. Power Pole Line		1	Lot	\$75,000		\$75,000
	02 Electrical Duct Banks		2200	LF	\$250		\$550,000
	03 15kv feeder cable		4400	LF	\$32		\$140,800
	04 Termination and splices		25	Each	\$250		\$6,250
	05 Transformers 750 KVA		4	Each	\$85,000		\$340,000
	06 Transformers 1500 KVA		4	Each	\$130,000		\$520,000
	07 Secondary ducts and wires		280	LF	\$600		\$168,000
	08 15 KV Switchgear		5	Each	\$22,000		\$110,000
	09 Generators		4	Each	\$60,000		\$240,000
	10 Kautz Rd Substation Upgrade		1	Lot	\$300,000		\$300,000
	11 Comm Duct Bank		2200	LF	\$100		\$220,000
	12 Electrical Manholes		4	Each	\$25,000		\$100,000
	13 Exterior road lighting		20	Each	\$1,800		\$36,000
							\$0

**Fermi National Accelerator Laboratory
FY13 Provisional Labor, Indirect and Shop Rates**

Consult your Division/Section/Project Field Financial Manager for the proper application of these rates to costs.			
Labor Burdens			
Labor Burden Rate is applied to:			
Vacation	<u>Monthly</u> Time Worked	10.25%	
Vacation	<u>Weekly</u> Time Worked	11.50%	
OPTO (Other Paid Time Off)	<u>Monthly</u> Time Worked	6.50%	
OPTO (Other Paid Time Off)	<u>Weekly</u> Time Worked	9.00%	
Fringe	Time Worked + Vacation + OPTO	32.75%	
Effective Labor (Vacation, OPTO, Fringe)	<u>Monthly</u> Time Worked	54.99%	(1)
Effective Labor (Vacation, OPTO, Fringe)	<u>Weekly</u> Time Worked	59.96%	(1)
Summer/Temp Fringe		8.00%	
Indirect Rates			Non HEP & Users Excludes TSCS
PS (Program Support)	Accelerator Division	27.5%	
PS (Program Support)	Accelerator Division - Effective Rate (PS, CSS, TSCS & G&A)	99.29%	(2) 94.05%
PS (Program Support)	Computing Division	10.2%	
PS (Program Support)	Computing Division - Effective Rate (PS, CSS, TSCS & G&A)	72.25%	(2) 67.72%
PS (Program Support)	Particle Physics Division	13.0%	
PS (Program Support)	Particle Physics Division - Effective Rate (PS, CSS, TSCS & G&A)	76.63%	(2) 71.98%
PS (Program Support)	Technical Division	20.2%	
PS (Program Support)	Technical Division - Effective Rate (PS, CSS, TSCS & G&A)	87.88%	(2) 82.94%
PS (Program Support)	Fully Loaded <u>Monthly</u> Time Worked - Accelerator Division	208.87%	(3) 200.75%
PS (Program Support)	Fully Loaded <u>Weekly</u> Time Worked - Accelerator Division	218.79%	(3) 210.41%
PS (Program Support)	Fully Loaded <u>Monthly</u> Time Worked - Computing Division	166.96%	(3) 159.94%
PS (Program Support)	Fully Loaded <u>Weekly</u> Time Worked - Computing Division	175.54%	(3) 168.29%
PS (Program Support)	Fully Loaded <u>Monthly</u> Time Worked - Particle Physics Division	173.75%	(3) 166.55%
PS (Program Support)	Fully Loaded <u>Weekly</u> Time Worked - Particle Physics Division	182.54%	(3) 175.11%
PS (Program Support)	Fully Loaded <u>Monthly</u> Time Worked - Technical Division	191.19%	(3) 183.53%
PS (Program Support)	Fully Loaded <u>Weekly</u> Time Worked - Technical Division	200.54%	(3) 192.64%
MSA (Material/Services Acquisition)		5.2%	
MSA (Material/Services Acquisition)	Effective Rate (MSA, TSCS & G&A)	22.90%	(4) 19.67%
CSS (Common Site Support)		33.80%	
CSS (Common Site Support)	Effective Rate - Non-Divisional (CSS, TSCS & G&A)	56.31%	(5) 52.20%
CSS (Common Site Support)	Fully Loaded <u>Monthly</u> Time Worked - Non-Divisional	142.25%	(6) 135.88%
CSS (Common Site Support)	Fully Loaded <u>Weekly</u> Time Worked - Non-Divisional	150.03%	(6) 143.46%
TSCS (Technical and Scientific Common Support)	(applied to HEP funded accounts only, excludes Users)	2.7%	
	Effective Rate - Non-Divisional (TSCS & G&A)	16.82%	
G&A (General and Administrative)		13.75%	
Pass-Through		1.5%	
The above rates have been submitted to the U. S. Department of Energy (DOE) and have been neither approved nor disapproved. The Laboratory's current Cost Accounting Standards Disclosure Statement has been approved by DOE. All the above rates are subject to adjustment to actual at least once per year in September. History of adjustments available on Accounting website.			
Shop Chargeback Rates *			
	Machine Shop	\$75	
	FESS Construction Engineering	\$96	
* The chargeback rates are subject to the CSS, TSCS and G&A indirect rates. Machine Shop is also subject to the TD PS rate.			

Approved: 
Michael F. Rhoades
Chief Accounting Officer

Approved: 
Cynthia S. Conger
Chief Financial Officer

- (1) - Effective rate on Time Worked after fringe rate applied to time worked + vacation + OPTO.
- (2) - Effective rate on total labor cost (see (1) above) after PS, CSS, TSCS & G&A rate applied. Shop charges are also subject to this effective rate.
- (3) - Effective rate on Time Worked after PS, CSS, TSCS & G&A rate applied to total labor cost (see (1) above).
- (4) - Effective rate on M&S costs after MSA, TSCS & G&A rate applied.
- (5) - Effective rate on total labor cost (see (1) above) after CSS, TSCS & G&A rate applied. Shop charges are also subject to this effective rate.
- (6) - Effective rate on Time Worked after CSS, TSCS & G&A rate applied to total labor cost (see (1) above).



Fermi National Accelerator Laboratory Indirect Burden Allocation Policy and Methodology

I. General Policy

It is the policy of the Laboratory to allocate indirect expenses to all final cost objectives. The types of indirect expenses allocated are Program Support (PS), Material/Service Acquisition (MSA), Common Site Support (CSS), Technical and Scientific Common Support (TSCS), and General and Administrative Expenses (G&A). All costs incurred are subject to the indirect burden allocation (as defined in Section III of this document) including the total cost of goods and services procured through Fermilab by user institutions or other external entities. This policy is consistent with the requirements of our Prime Contract with DOE to comply with Cost Accounting Standards (CAS), as well as the requirements of DOE Order 522.1, "Pricing of Departmental Materials and Services".

The Budget Office and the Accounting Department develop provisional indirect burden rates jointly. Normally provisional rates are based upon the Laboratory's current year budget of direct and indirect costs. However, in the case where the approved budget for the upcoming year has not been finalized, or in the case of a new methodology with which the Lab has little or no experience, the rates may be based on prior year(s) actual rates or projections.

The provisional rates will go into effect on the first day of the fiscal year, with a retroactive adjustment to actual (variance distribution) at least annually at year end. Major changes in funding, budgetary allocations, or the Lab's indirect burden allocation methodology could necessitate a rate change (increase or decrease) and/or a variance distribution during the year; such rate changes and variance distributions are subject to CFO approval. CAS requires rate changes to be retroactive to the beginning of the fiscal year.

The Accounting Department performs a monthly analysis of indirect allocations and monitors the rates and accumulated variances.

II. Exceptions

The indirect burden allocation rates are generally applied to all final cost objectives with the following exceptions as stated below:

A. When Laboratory personnel provide a service (labor cost) while away from the Laboratory for a period of more than 180 days, the Common Site Support rate will not be charged upon request of applicable Division/Section management. The labor must be segregated into a task to be established, not subject to CSS.

B. When special conditions or extenuating circumstances exist, the amount or applicability of the indirect charge to a collaborating institution may be negotiated with the Laboratory, with approval of the CFO. When an adjustment is granted, said adjustment should be included in the "Agreement for an Experiment", Memorandum of Understanding, or other formal document as appropriate, and such document should be provided to the Accounting Department before charges are incurred. If costs billed to a user institution will not include indirect charges, those charges must be transferred to the benefiting Laboratory B&R code, which can be determined by the purpose stated in the Agreement. The transfer is completed as part of the month-end burdening process where indirect costs are mirrored to the appropriate lab B&R. It should be noted that the use of this exception may cause difficulty in explaining the nature of these charges to DOE program managers and/or other reviewers of the benefiting B&R.

C. Large Cap Purchase Order Indirect Cost Limitation:

Purchase orders with a single procurement action of greater than \$500,000 will have indirect costs capped on \$500,000 of costs. This exception recognizes that the causal-beneficial relationship between the procurement effort and procurement output is not linear (i.e. a typical \$2 million order does not require four times the effort to place as a typical

\$500,000 order).

All purchase orders entitled to the Indirect Cost Cap should be written against an exempt expenditure type as shown below.

Exempt – Civil Construction
Exempt – Equipment Rental
Exempt – Equipment
Exempt – Fabrication Procurement

Exempt – Material Purchases
Exempt – Subcontract Services Pass Thru
Exempt – Subcontract Services
Exempt – Temporary Help

The exempt expenditure types are excluded from the Indirect Burden Allocation process that is run at month-end; they do not receive a system generated indirect charge. Instead, the indirect charge for a purchase order written against any of these expenditure types is manually computed on the first \$500,000 and recorded in Oracle Projects during the month that the first vendor invoice against the order is processed. Allocation of the indirect cost across Project/Task, in the case of split-coded orders, is based upon the P.O. distribution reported in Oracle eBS at the time of receipt of the first invoice.

The following table summarizes conditions under which a procurement action may or may not qualify for treatment under the Large Cap exception.

1.	Initial P.O.'s > \$500K qualify.
2.	Change orders > \$500K qualify. Total order amount is subject to the cap.
3.	Change orders < \$500K qualify if the original P.O. is > \$500K. Total order amount is subject to the cap.
4.	Total orders that are over \$500K as a result of original P.O. and subsequent change orders under \$500K do not qualify. Orders approved as Pass-Through orders (see below) are not subject to this requirement.
5.	Original total orders that are over \$500K as a result of multiple requisitions < \$500K placed on one purchase order qualify.
6.	Master Contract releases > \$500K qualify but releases < \$500K do not qualify.

D. Pass Through Orders:

Purchase orders that meet the definition of a Pass-Through purchase order are eligible for a reduced indirect rate of 1.5%. Pass-through orders are agreements that transfer funds to a program's/project's collaborating institution to carry out agreed-upon work. The reduced rate reflects the reduced indirect effort associated with such a procurement action. The reduced effort is primarily due to the preexisting documented agreement between the institutions, including deliverables, milestones, and due dates, most commonly through a Memorandum of Understanding.

A request for pass-through action must have CFO approval. All purchase requisitions representing approved pass-through actions must be recorded against expenditure type Subcontract Services Pass-Thru or Exempt - Subcontract Services Pass-Thru (further discussed below). Requisitions requesting pass-through treatment must include evidence of the collaborative character of the work with respect to the program/project and must generally meet the condition of requiring reduced indirect effort.

Application of the pass-through rate is subject to the \$500,000 ceiling like any other large cap order. Purchase requisitions representing a pass-through action in excess of \$500,000 should be recorded against the exempt expenditure type, Exempt - Subcontract Services Pass-Thru, instead of expenditure type Subcontract Services Pass-Thru.

E. Restricted/Exempt Burden Schedules:

There are tasks that fall under specific Service Types that use a restricted or exempt burden schedule due to special circumstances. Examples include Inventory and certain costs unallowable on the contract.

III. Indirect Burden Rate Calculation

The rates for the provisional PS, MSA, CSS, TSCS, and G&A burden allocations will be based on the following formulas, where the numerator is the pool, and the denominator is the distribution base of the pool:

A. Program Support Burden Allocation

Each of our four Divisions (Accelerator, Computing, Particle Physics, and Technical) has a Program Support allocation to cover the costs associated with central division administration, departmental management, central computing support, certain travel and training, and related costs, as well as similar costs that exist in the Centers that are associated with those Divisions.

1. **Accelerator Division – (Includes APC)**
B&R Code: EC0101070 – AD Program Support
Service Type: OP-BURDEN-PS AD
Expenditure Type: AD Program Support Allocation
2. **Computing Division**
B&R Code: EC0101080 – CD Program Support
Service Type: OP-BURDEN-PS CD
Expenditure Type: CD Program Support Allocation
3. **Particle Physics Division – (Includes FCPA & CMS Center)**
B&R Code: EC0101090 – PPD Program Support
Service Type: OP-BURDEN-PS PPD
Expenditure Type: PPD Program Support Allocation
4. **Technical Division**
B&R Code: EC0101010 – TD Program Support
Service Type: OP-BURDEN-PS TD
Expenditure Type: TD Program Support Allocation

Pool – Each Division’s Pool contains costs from the following activities as applicable:

D/S/C Administration	Project Oversight
Document Workflow & Information Systems	Transportation, Distribution, Fleet
Financial Management	Quality Assurance
Human Resources	Safety Services
IT Governance and Oversight	

The Centers have pool costs that are primarily D/S/C Administration.

Base – The Program Support burden allocation will be applied to the following expenditure types of the respective division:

Accounting Transfers – Labor	Overtime
Construction Engineering	Service Organization Distribution
EOM Wage Accrual – Monthly	Special Compensation
EOM Wage Accrual – Summer/Temp	Summer/Temp Emp. Monthly
EOM Wage Accrual – Weekly	Summer/Temp Emp. Weekly
Fringe – Special	Time Worked – Monthly
Machine Shop	Time Worked – Weekly

Vacation, OPTO, and Fringe allocations are also included in the base.

The base excludes costs charged to the PS burden pools themselves (i.e. to tasks with the service types of OP-BURDEN-PS AD, OP-BURDEN-PS CD, OP-BURDEN-PS PPD, or OP-BURDEN-PS TD.)

B. MSA Burden Allocation

The Material/Service Acquisition (MSA) burden pool represents the cost of purchasing services and materials. This includes a range of costs, from the cost of negotiation and execution of a contract to the cost of processing an invoice.

B&R Code: EC0101040 – Materials/Service and Acquisition

Service Type: OP-BURDEN-MSA

Expenditure Type: MSA Allocation

Pool – The MSA pool consists of all the costs from the following activities:

Purchasing	Stock Room
Accounts Payable	Inventory Variances
Shipping/Receiving	

Base –The MSA burden allocation will be applied to the following expenditure types:

Civil Construction	Material Purchases
Computer Maintenance	Office Machine Maintenance
Computers, Desktop	ProCard Purchases
Computers, Hardware Maintenance	Professional Services
Computers, Software Licenses	Purchased Services
Computers, Software Maintenance	Spare parts/Other Issues
Computer Services Distribution	Special Process Spares Issues
Demurrage/Container Rental	Stores Issues
Equipment	Sub Contract Services
Equipment Rental	T&M Construction Services
Fabrication Procurement	T&M Electrical Services
Facility Rental	T&M Pipe Fitters
Freight	T&M Rigging Services

Gases/ Cryogenic Fluids	Telephone Expense
Honoraria	Telephone Expense Distribution
Insurance Premium	Temporary Help

The base excludes costs charged to the MSA pool and burden pools previously allocated (i.e. to tasks with the service types of OP-BURDEN-PS AD, OP-BURDEN-PS CD, OP-BURDEN-PS PPD, or OP-BURDEN-PS TD, or OP-BURDEN-MSA.)

C. CSS Burden Allocation

The Common Site Support (CSS) burden represents the cost of running the physical facility and infrastructure (power, facility maintenance and management, computing infrastructure, telecommunications, mail service, etc.).

B&R Code: EC0101050 – Common Site Support
 Service Type: OP-BURDEN-CSS
 Expenditure Type: CSS Allocation

Pool – The CSS pool consists of costs from the following activities:

- | | |
|---|---|
| Building Maintenance and Management Facilities | Non-programmatic Power |
| Engineering Services Section | Property Management |
| ES&H Section | Telecommunications |
| Accommodations | Transportation |
| Computing Support | Travel Office |
| Farm Income | Vehicle Maintenance |
| Food Service | Audio-Visual/Duplicating/Photo Services |
| Information Resources | Variances from the Service Centers |
| Mail Operations | PS and MSA allocations on the costs in the CSS pool |
| Non-programmatic building maintenance and utilities | |

Cyber Security other than:
 Assignment of an Information Systems Security Manager
 Assignment of a Certification Agent(s) – includes forensics analyst
 Assignment of a full time Information System Security Officer (s)
 SC HQ-mandated Security Implementations

Base – The CSS burden allocation will be applied to the expenditure types listed within the PS section of this document.

Vacation, OPTO, and Fringe labor burdens, as well as PS burden allocations, are also included in the base.

The base excludes costs charged to the CSS pool and pools previously allocated (i.e. to tasks with the service types of OP-BURDEN-PS AD, OP-BURDEN-PS CD, OP-BURDEN-PS PPD, or OP-BURDEN-PS TD, OP-BURDEN-MSA, or OP-BURDEN-CSS).

D. Technical and Scientific Common Support Allocation

The Technical and Scientific Common Support (TSCS) burden represents costs incurred by the Accelerator, Particle Physics and Technical Divisions associated with providing technical and scientific services necessary to support the

high energy physics program at the laboratory. These include costs for Engineering Support, Vacuum and Fluids, the Silicon Detector, Carbon Fiber, Extrusion and Cryogenics facilities, Magnet Systems and Magnet Test facilities, and Meson Detector Building Test Facility.

B&R Code: EC-01-01-020
 Service Type – OP-BURDEN TSCS
 Expenditure Type: TSCS Burden Allocation

Pool – Each division above has pool costs from the following activities when associated with the support of technical and scientific needs:

Accelerator Controls & Instrumentation	Technical Facilities Operations/Improvements
Accelerator Operations	PS, MSA and CSS allocations on the costs in the
Technical Centers Management	TSCS pool

Base – The TSCS burden allocation will be applied to the expenditure types listed within the PS and MSA sections of this document.

Vacation, OPTO, and Fringe labor burdens, as well as PS, MSA and CSS burden allocations, are also included in the base.

Additionally, the base includes the following expenditure types:

Accounting Transfers	Relocation
Donated Funds	Relocation – Temporary
Duplicating Services	Special Events
Educational Expense	Stipend Education
Fees	Stores & Spares loss / OBS
Housing Costs	Training
On-Site Travel Reimbursement	Travel, Domestic, Lab Employee
Other Costs and Credits	Travel, Domestic, Non Employee
Other Utilities	Travel, Foreign, Lab Employee
Photo/Graphic Services	Travel, Foreign, Non Employee
Physical Inventory Adj	Vehicle Maintenance
Postage and Related Costs	Video/Streaming
Proceeds from Personal Property Sales	Visitor Subsistence over 1 year
Recruitment	Visitor Subsistence < 1 year

The base excludes costs charged to the TSCS pool and pools previously allocated (i.e. to tasks with the service types of OP-BURDEN-PS AD, OP-BURDEN-PS CD, OP-BURDEN-PS PPD, or OP-BURDEN-PS TD, OP-BURDEN-MSA, OP-BURDEN-CSS, or OP-BURDEN-TSCS). Additionally, costs charged to tasks in Non-HEP B&R's and in service type OP-R&D-USERS are also excluded.

Costs on project construction funds are not included in the base.

E. G & A Burden Allocation

The General and Administrative (G & A) burden pool represents the costs of the management and administration of the laboratory as a whole.

B&R Code: EC0101060 – General and Administrative

Service Type: OP-BURDEN-G&A

Expenditure Type: G&A Allocation

Pool – The G & A pool consists of all the costs from the following activities.

Business Services Section Office (the portion not included within the MSA or CSS pools)	Human Resources
Computing Division Information Systems	Institutional General Plant Projects (IGPP)
Conference Office	Legal Office
Contractor Fee	Miscellaneous revenues
Directorate	Offset from Pass-through Rate
Education Office	Office of Communications
Finance Section Office (the portion not included within the MSA pool)	Payroll
Service on reviews of projects/programs/activities, and on lab wide committees not specific to mission work.	
PS, MSA and CSS allocations on the costs in the G&A pool	

Base – The G&A burden allocation will be applied to all expenditure types listed within the PS, MSA & TSCS sections of this document.

Vacation, OPTO, and Fringe labor burdens, as well as PS, MSA, CSS and TSCS burden allocations, are also included in the base.

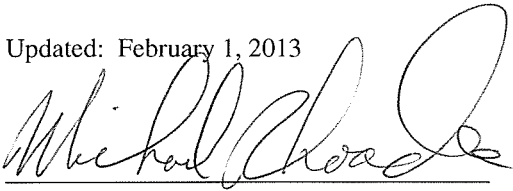
The base excludes costs charged to the G&A pool and pools previously allocated (i.e. to tasks with the service types of OP-BURDEN-PS AD, OP-BURDEN-PS CD, OP-BURDEN-PS PPD, or OP-BURDEN-PS TD, OP-BURDEN-MSA, OP-BURDEN-CSS, OP-BURDEN-TSCS or OP-BURDEN-G&A).

IV. Current Year Rates

The following link will advise the current year's rates.

[Provisional Labor, Indirect, and Shop Rates](#)

Updated: February 1, 2013



Michael Rhoades – Chief Accounting Officer

2/8/13
Date



Cynthia Conger – Chief Financial Officer



APPENDIX B

nuSTORM Conventional Facilities

Preliminary Drawings

- PDR-01 Location Plans and List of Drawings
- PDR-02 Existing – Site Plan
- PDR-03 Underground – Site Plan
- PDR-04 Surface Buildings – Site Plan
- PDR-05 Primary Beamline
- PDR-06 Main Injector and Primary Beamline Sections
- PDR-07 Enclosure Plan at Target Hall
- PDR-08 Target Hall Building Plan Sheet 1
- PDR-09 Target Hall Building Plan Sheet 2
- PDR-10 Target Hall Building Sections Sheet 1
- PDR-11 Target Hall Building Sections Sheet 2
- PDR-12 Target Hall Building Sections Sheet 3
- PDR-13 Enlarged Plans and Sections
- PDR-14 Muon Decay Ring Plan
- PDR-15 Muon Decay Ring Section
- PDR-16 Muon Decay Ring Building Plan
- PDR-17 Cryogenic Building Plan
- PDR-18 Muon Decay Ring Building Section
- PDR-19 Near Detector Hall Floor Plan Sheet 1
- PDR-20 Near Detector Hall Floor Plan Sheet 2
- PDR-21 Near Detector Hall Floor Plan Sheet 3
- PDR-22 Building and Enclosure Section Sheet 1
- PDR-23 Building and Enclosure Section Sheet 2
- PDR-24 Far Detector Floor Plan
- PDR-25 Far Detector Floor Plan
- PDR-26 Building Section

APPENDIX
B

APPENDIX B

nuSTORM

PROJECT NUMBER 6-13-1



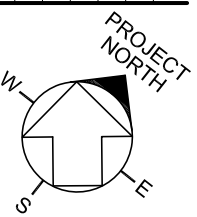
VICINITY PLAN

SCALE: N.T.S.

LIST OF DRAWINGS

PDR-01	LOCATION PLANS AND LIST OF DRAWINGS
PDR-02	EXISTING - SITE PLAN
PDR-03	UNDERGROUND - SITE PLAN
PDR-04	SURFACE BUILDINGS - SITE PLAN
PDR-05	PRIMARY BEAMLINE
PDR-06	MAIN INJECTOR AND PRIMARY BEAMLINE SECTIONS
PDR-07	ENCLOSURE PLAN AT TARGET HALL
PDR-08	TARGET HALL BUILDING PLAN SHEET 1
PDR-09	TARGET HALL BUILDING PLAN SHEET 2
PDR-10	TARGET HALL BUILDING SECTIONS SHEET 1
PDR-11	TARGET HALL BUILDING SECTIONS SHEET 2
PDR-12	TARGET HALL BUILDING SECTIONS SHEET 3
PDR-13	ENLARGED PLANS AND SECTIONS
PDR-14	MUON DECAY RING PLAN
PDR-15	MUON DECAY RING SECTION
PDR-16	MUON DECAY RING BUILDING PLAN
PDR-17	CRYOGENIC BUILDING PLAN
PDR-18	MUON DECAY RING BUILDING SECTIONS
PDR-19	NEAR DETECTOR HALL FLOOR PLAN SHEET 1
PDR-20	NEAR DETECTOR HALL FLOOR PLAN SHEET 2
PDR-21	NEAR DETECTOR HALL FLOOR PLAN SHEET 3
PDR-22	BUILDING AND ENCLOSURE SECTION SHEET 1
PDR-23	BUILDING AND ENCLOSURE SECTION SHEET 2
PDR-24	FAR DETECTOR FLOOR PLAN
PDR-25	FAR DETECTOR FLOOR PLAN
PDR-26	BUILDING SECTION

SCALE:



nuSTORM
LOCATION PLANS AND LIST OF DRAWINGS



LOCATION PLAN

SCALE: N.T.S.

PDR



DATE

08 MAY, 2013

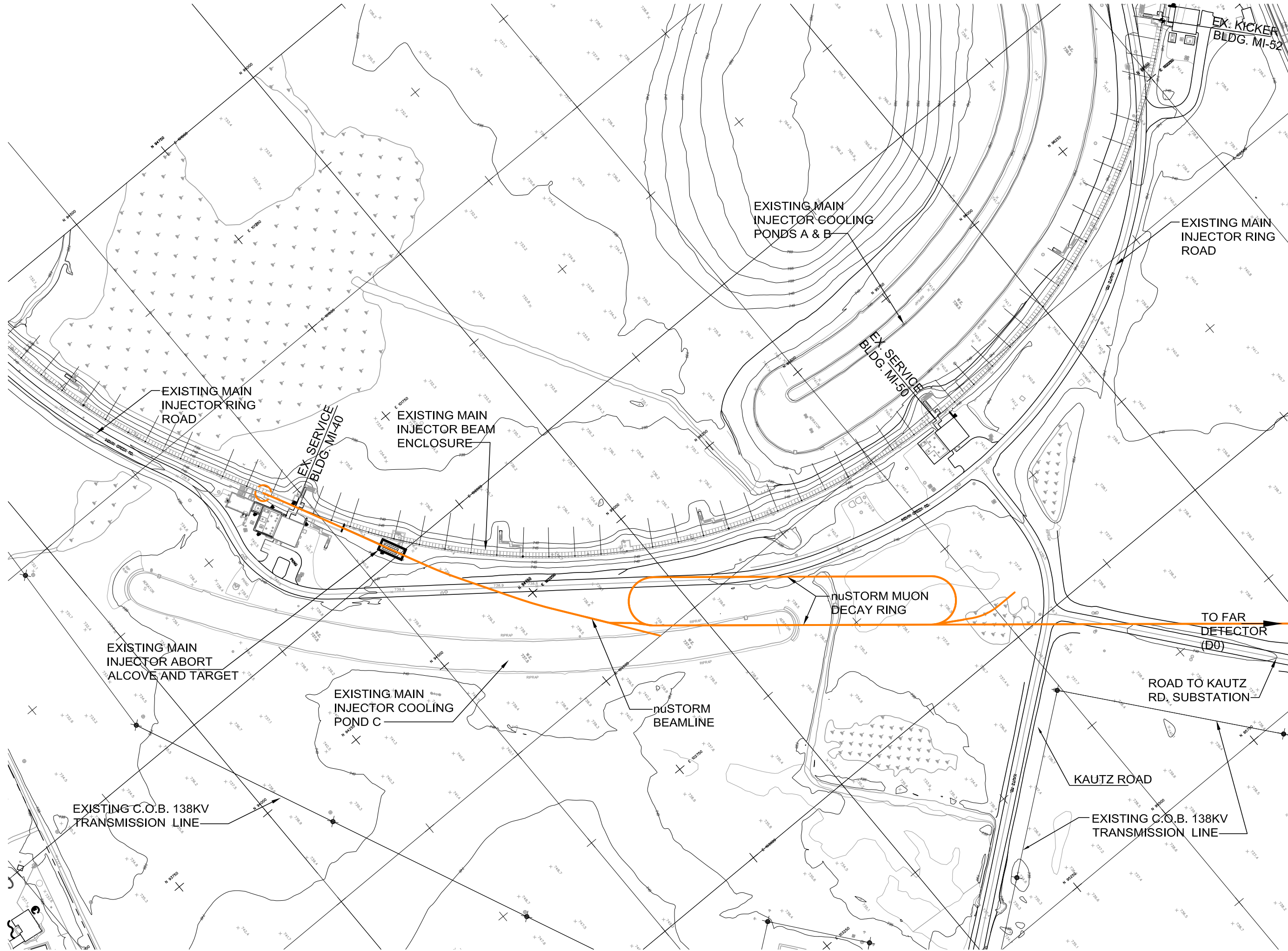
PROJECT NO.

6-13-1

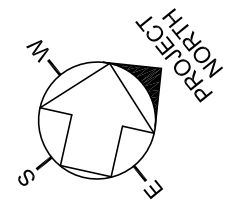
DRAWING NO.

PDR-01

May 13, 2013 - 6:53am \\blue1\less\FESS_ENG\Active Projects\6131111 - Pre-conceptual\Drawings\June 2012\From NuMI MI-40 SBL\PDR-2_6-13-11\PDR-02_6-13-1.dwg



SCALE:
1" = 60'-0"
SCALE
60 FEET



nuSTORM
EXISTING - SITE PLAN

PDR



Fermilab



DATE

08 MAY, 2013

PROJECT NO.

6-13-1

DRAWING NO.

PDR-02

SITE UTILITIES

INDUSTRIAL COOLING WATER (ICW)

- EXTEND FROM KAUTZ ROAD
- INCLUDE FIRE HYDRANTS
- FEED TO ALL BUILDING FIRE RISERS

DOMESTIC WATER (DW)

- EXTENDED FROM MI-60 AREA
- TO NORMALLY OCCUPIED SERVICE BUILDINGS

SANITARY SEWER (SS)

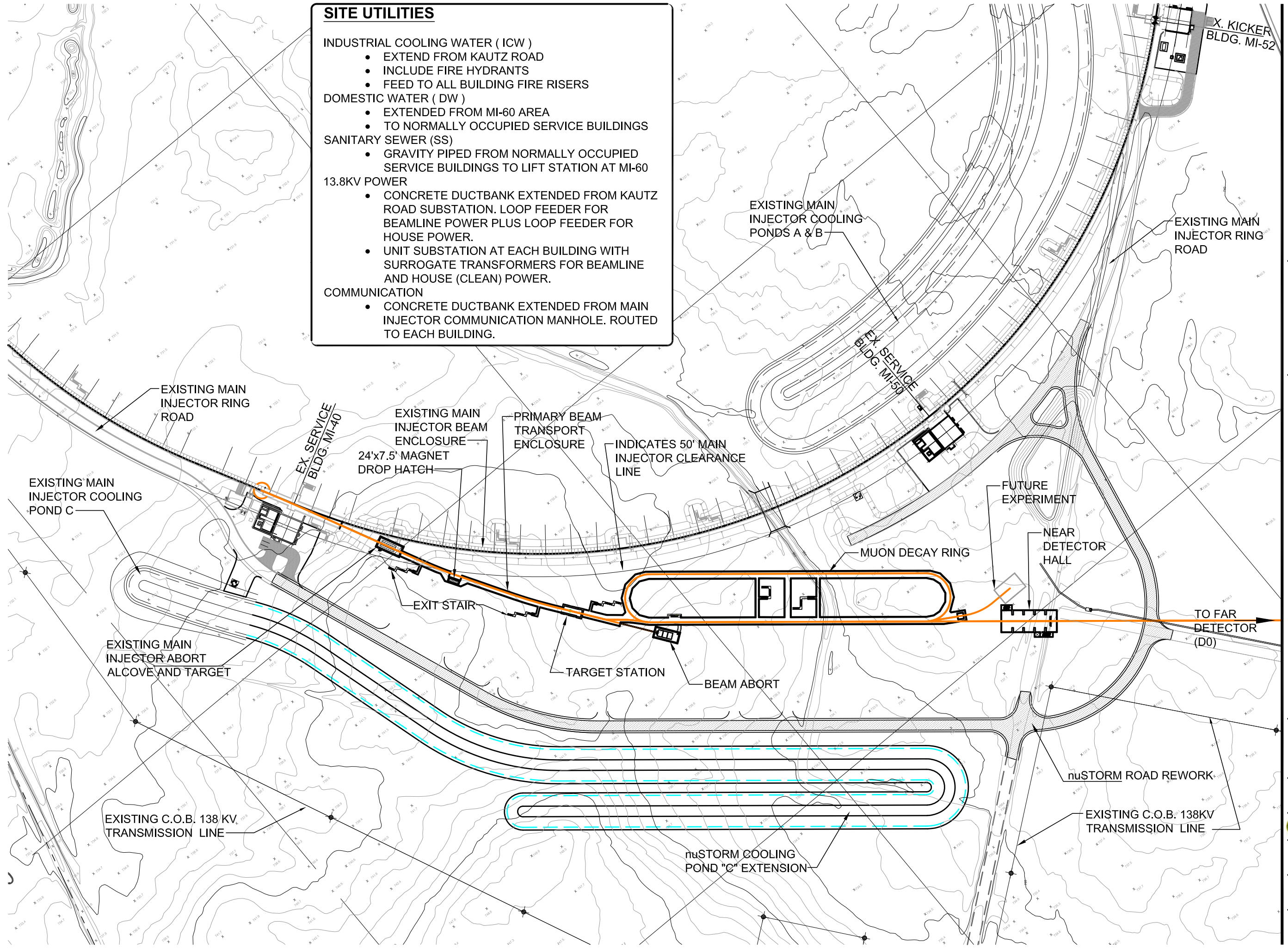
- GRAVITY PIPED FROM NORMALLY OCCUPIED SERVICE BUILDINGS TO LIFT STATION AT MI-60

13.8KV POWER

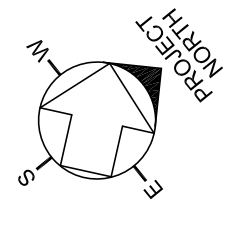
- CONCRETE DUCTBANK EXTENDED FROM KAUTZ ROAD SUBSTATION. LOOP FEEDER FOR BEAMLINE POWER PLUS LOOP FEEDER FOR HOUSE POWER.
- UNIT SUBSTATION AT EACH BUILDING WITH SURROGATE TRANSFORMERS FOR BEAMLINE AND HOUSE (CLEAN) POWER.

COMMUNICATION

- CONCRETE DUCTBANK EXTENDED FROM MAIN INJECTOR COMMUNICATION MANHOLE. ROUTED TO EACH BUILDING.



SCALE:
1" = 60'-0"
60 FEET



nuSTORM
UNDERGROUND - SITE PLAN

PDR



Fermilab



DATE

08 MAY, 2013

PROJECT NO.

6-13-1

DRAWING NO.

PDR-3

May 13, 2013 - 6:55am \\blue1\less\FESS_ENG\Active Projects\613111 - Pre-conceptual\Drawings\June 2012\From NuMI MI-40 SBL\PDR-03_6-13-1.dwg

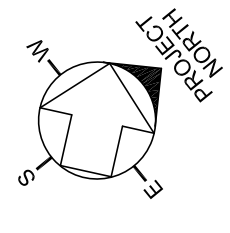
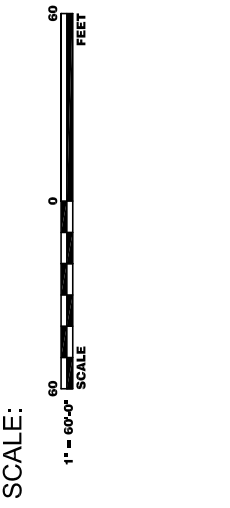
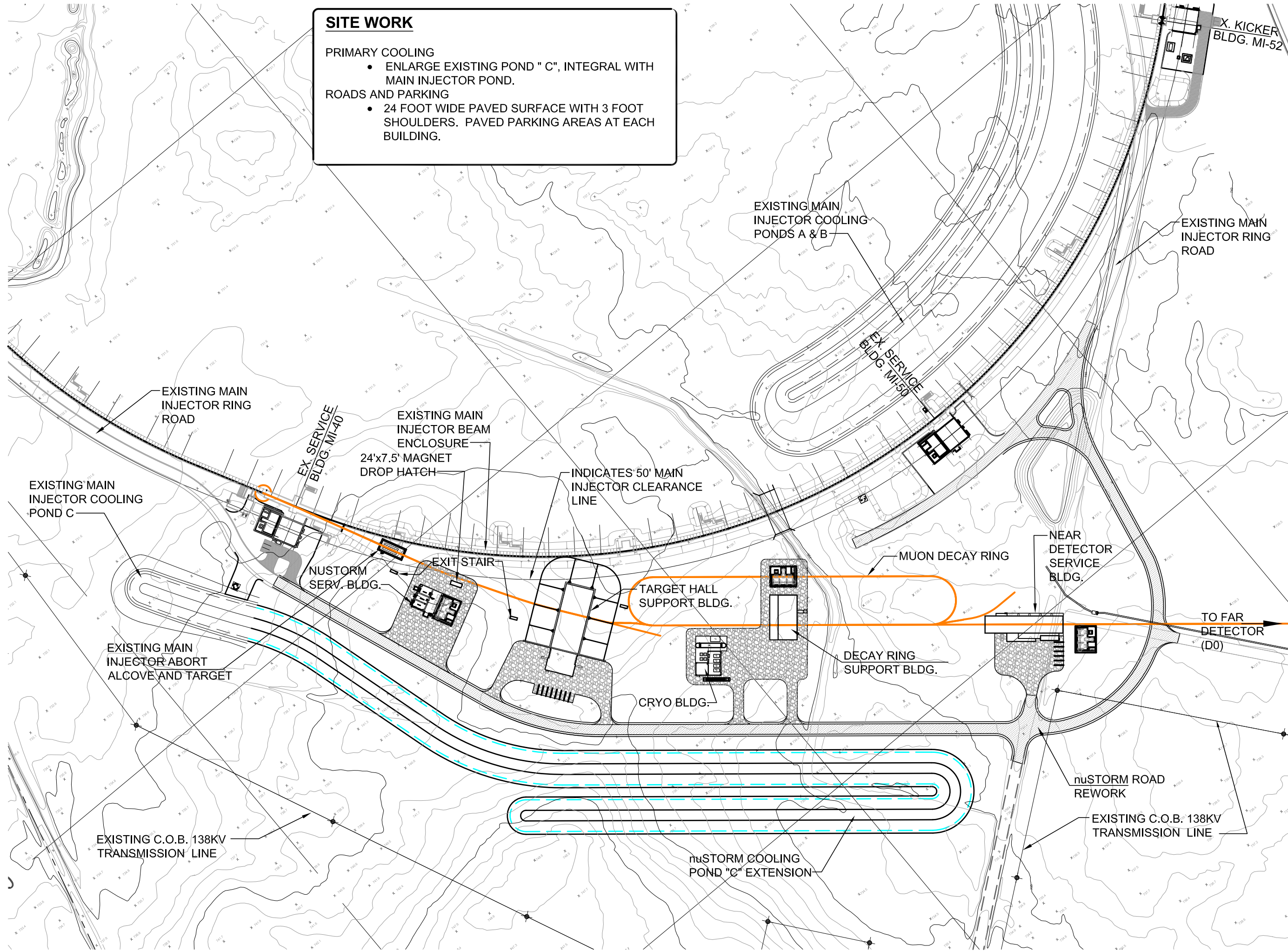
SITE WORK

PRIMARY COOLING

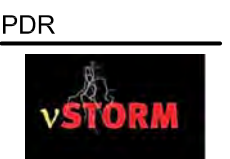
- ENLARGE EXISTING POND "C", INTEGRAL WITH MAIN INJECTOR POND.

ROADS AND PARKING

- 24 FOOT WIDE PAVED SURFACE WITH 3 FOOT SHOULDERS. PAVED PARKING AREAS AT EACH BUILDING.



nuSTORM
SURFACE BUILDINGS - SITE PLAN

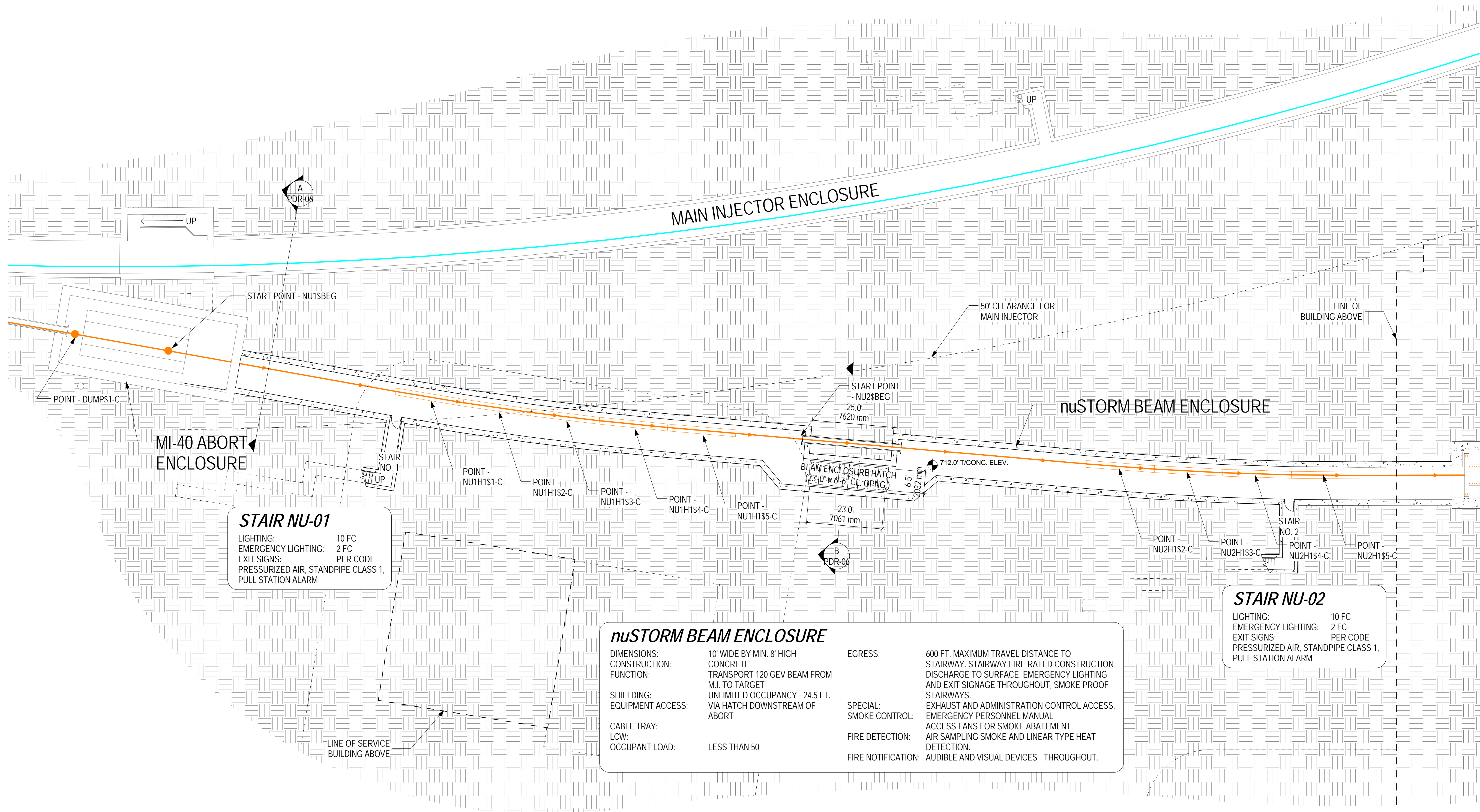


DATE
08 MAY, 2013

PROJECT NO.
6-13-1

DRAWING NO.
PDR-04

May 13, 2013 - 6:58am \\blue1\less\FESS_ENG\Active Projects\613111 - Pre-conceptual\Drawings\June 2012\From NuMI MI-40 SBL\PDR-04_6-13-1.dwg



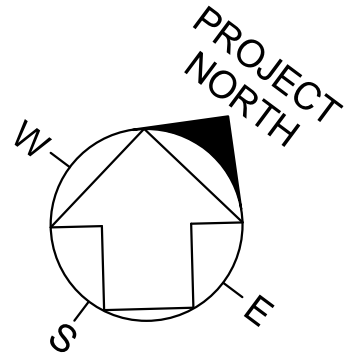
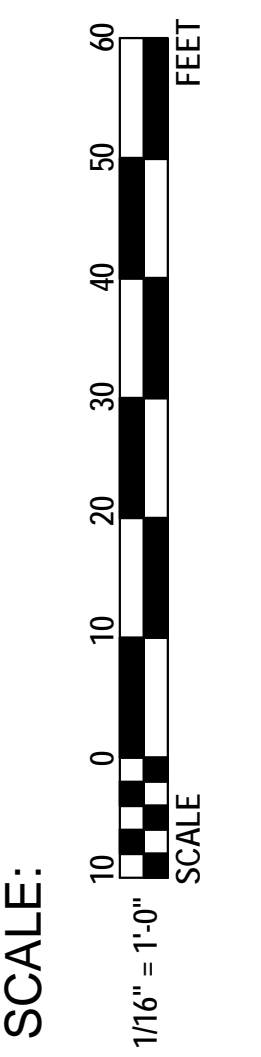
STAIR NU-01
 LIGHTING: 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

nuSTORM BEAM ENCLOSURE
 DIMENSIONS: 10' WIDE BY MIN. 8' HIGH
 CONSTRUCTION: CONCRETE
 FUNCTION: TRANSPORT 120 GEV BEAM FROM M.I. TO TARGET
 SHIELDING: UNLIMITED OCCUPANCY - 24.5 FT.
 EQUIPMENT ACCESS: VIA HATCH DOWNSTREAM OF ABORT
 CABLE TRAY: LCW:
 OCCUPANT LOAD: LESS THAN 50
 EGRESS: 600 FT. MAXIMUM TRAVEL DISTANCE TO STAIRWAY. STAIRWAY FIRE RATED CONSTRUCTION DISCHARGE TO SURFACE. EMERGENCY LIGHTING AND EXIT SIGNAGE THROUGHOUT, SMOKE PROOF STAIRWAYS.
 SPECIAL: EXHAUST AND ADMINISTRATION CONTROL ACCESS.
 SMOKE CONTROL: EMERGENCY PERSONNEL MANUAL ACCESS FANS FOR SMOKE ABATEMENT.
 FIRE DETECTION: AIR SAMPLING SMOKE AND LINEAR TYPE HEAT DETECTION.
 FIRE NOTIFICATION: AUDIBLE AND VISUAL DEVICES THROUGHOUT.

STAIR NU-02
 LIGHTING: 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

PRIMARY BEAM LINE

SCALE: 1/16" = 1'-0"



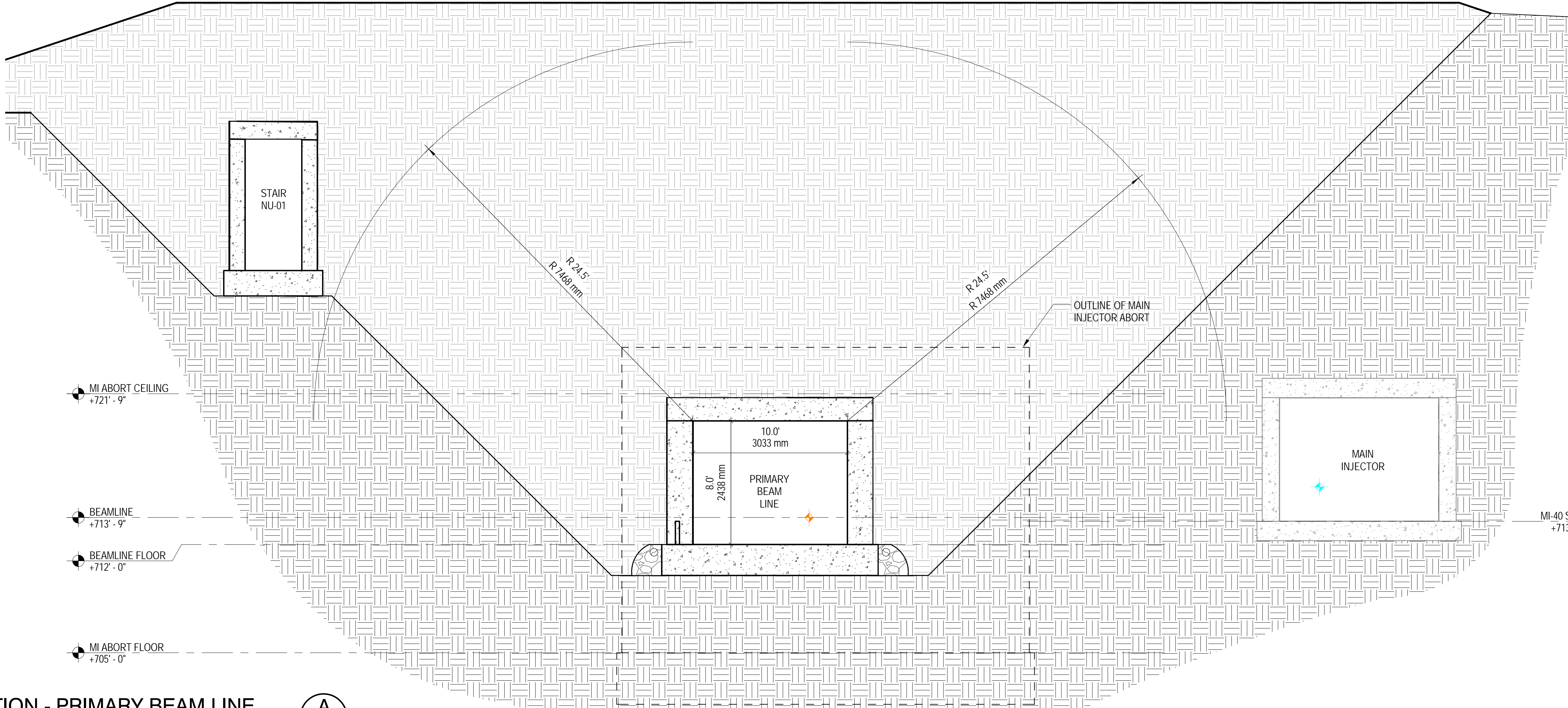
PRIMARY BEAMLINE



DATE: **08 MAY 2013**

PROJECT NO.: **6-13-1**

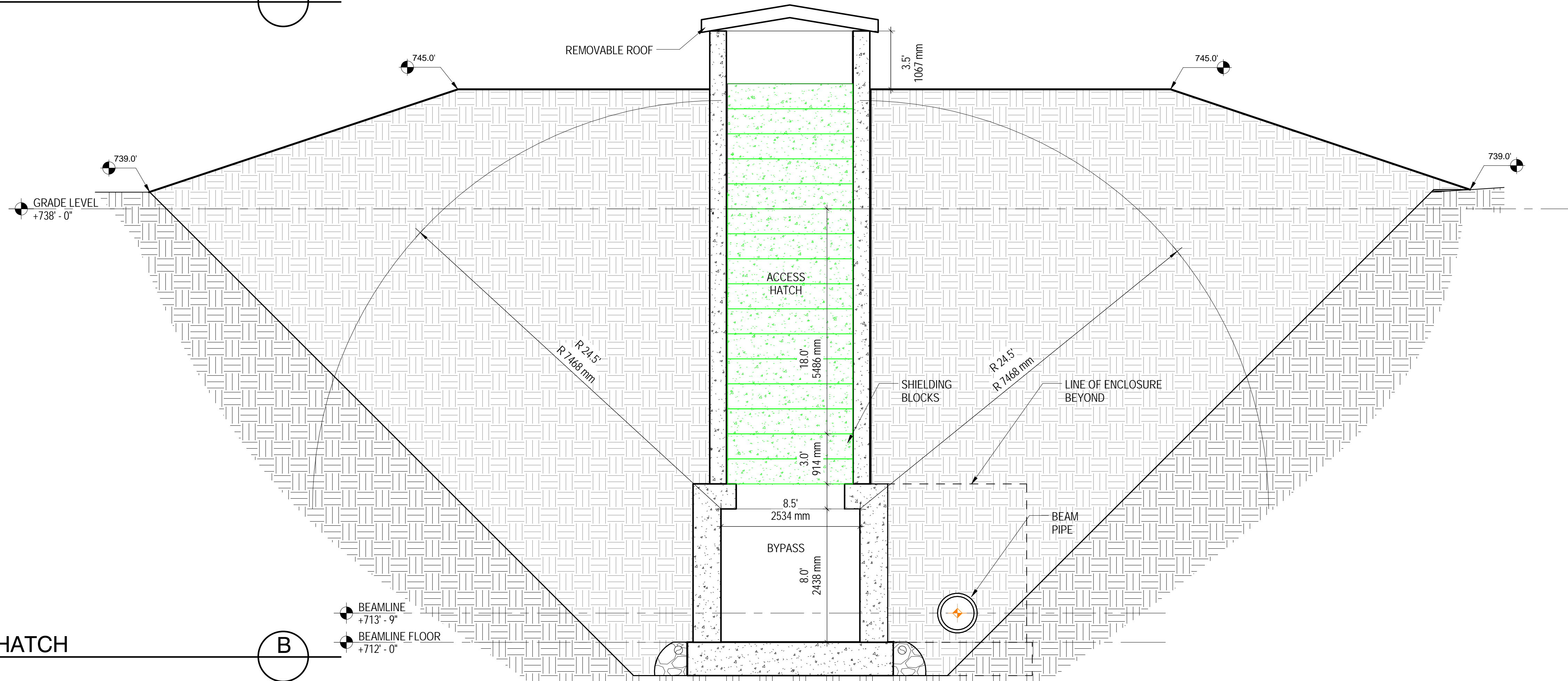
DRAWING NO.: **PDR-05**



SECTION - PRIMARY BEAM LINE

A

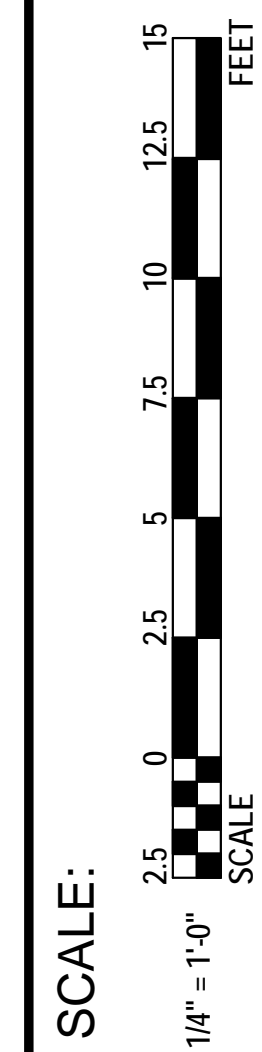
SCALE: 1/4" = 1'-0"



SECTION - HATCH

B

SCALE: 1/4" = 1'-0"



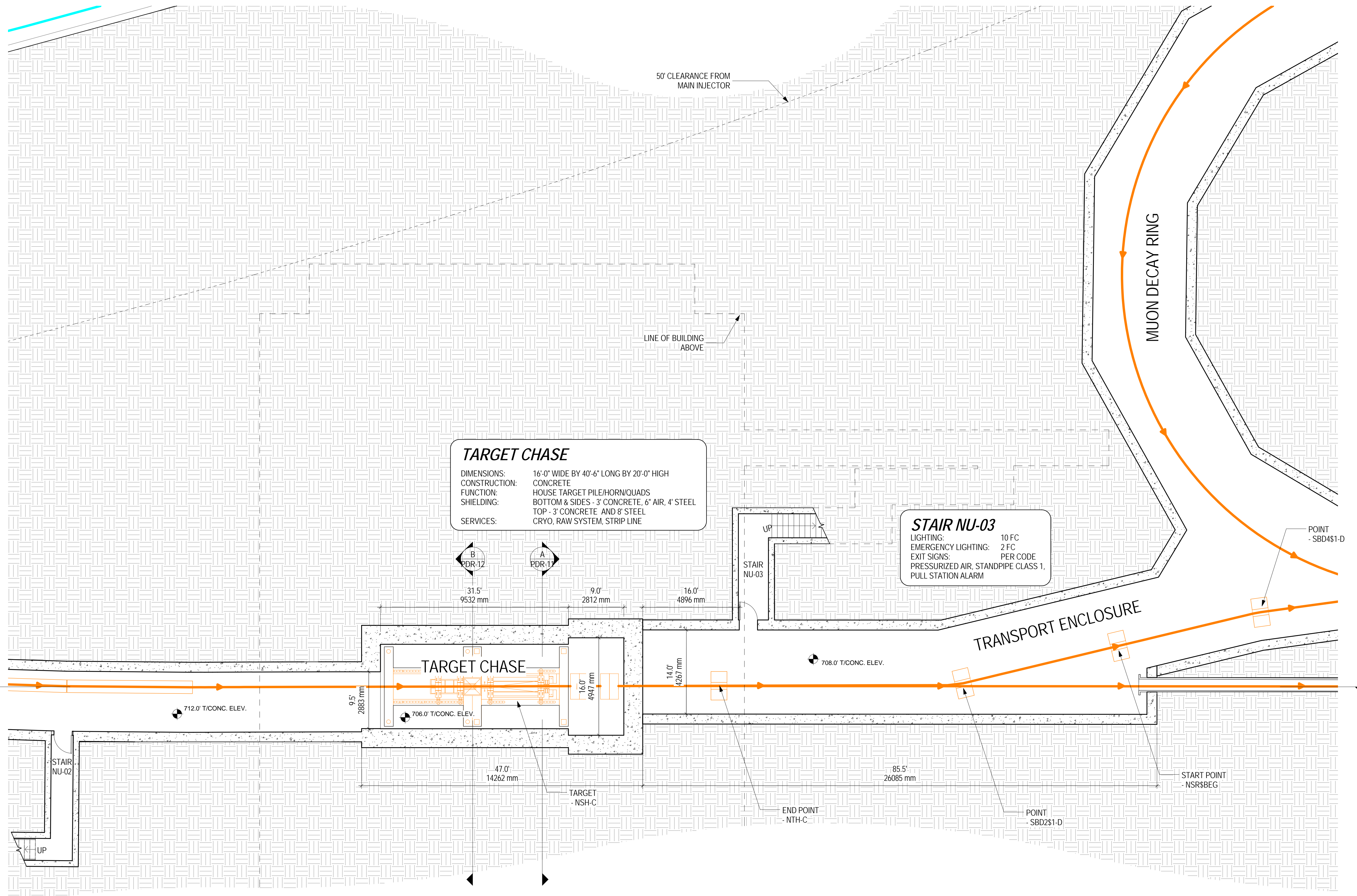
MAIN INJECTOR & PRIMARY BEAMLINE SECTIONS



DATE
08 MAY 2013

PROJECT NO.
6-13-1

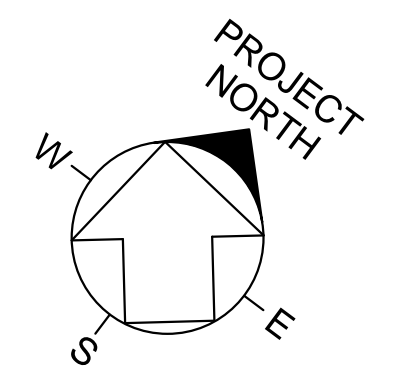
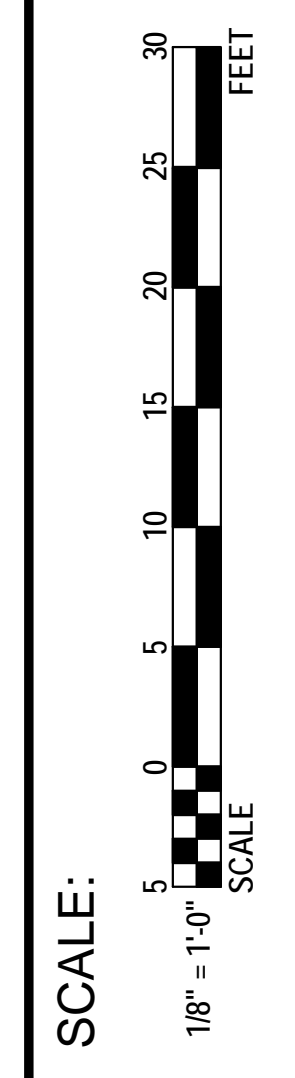
DRAWING NO.
PDR-06



TARGET CHASE
 DIMENSIONS: 16'-0" WIDE BY 40'-6" LONG BY 20'-0" HIGH
 CONSTRUCTION: CONCRETE
 FUNCTION: HOUSE TARGET PILE/HORN/QUADS
 SHIELDING: BOTTOM & SIDES - 3' CONCRETE, 6" AIR, 4' STEEL
 TOP - 3' CONCRETE AND 8" STEEL
 SERVICES: CRYO, RAW SYSTEM, STRIP LINE

STAIR NU-03
 LIGHTING: 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

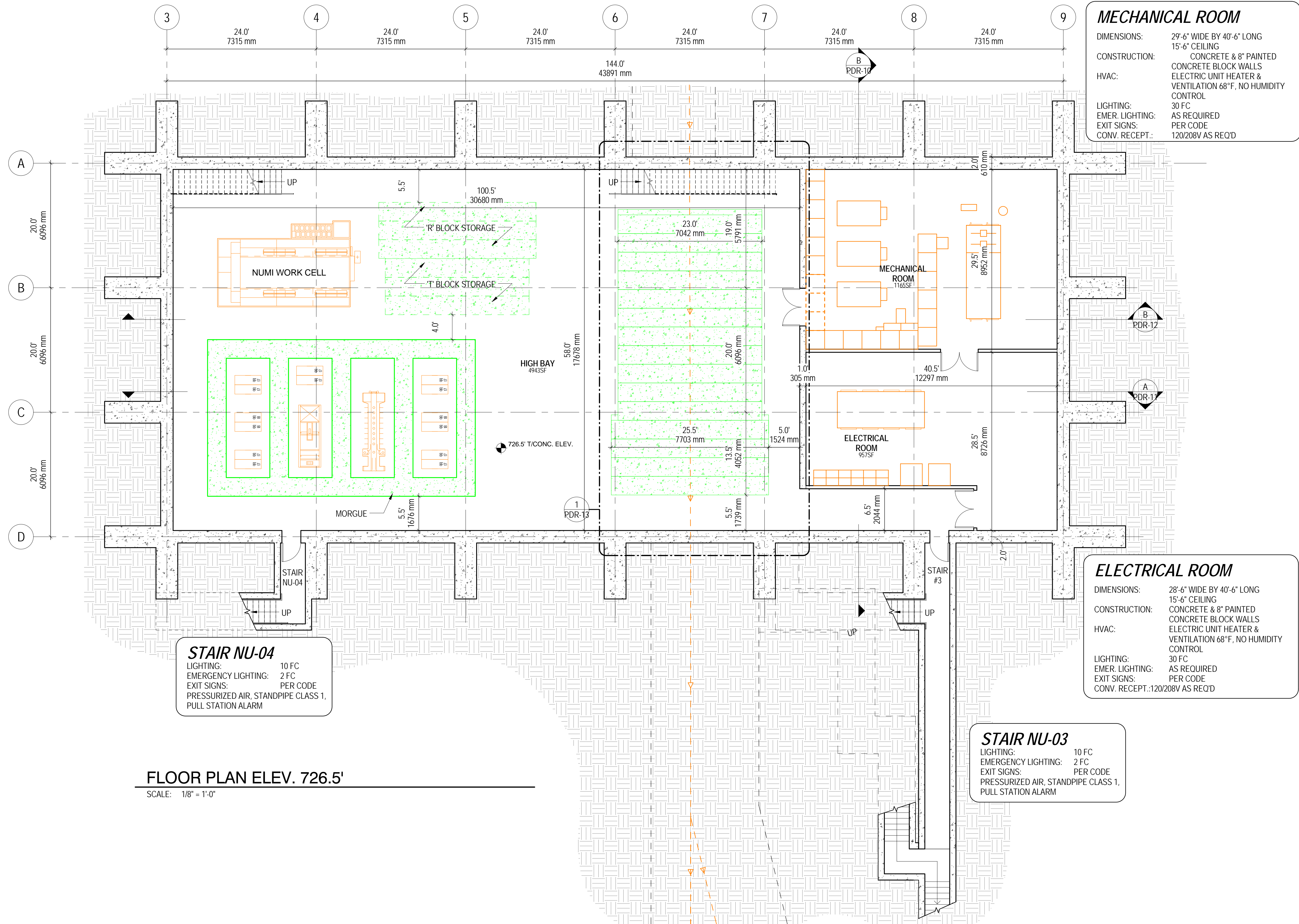
ENCLOSURE AT TARGET CHASE
 SCALE: 1/8" = 1'-0"



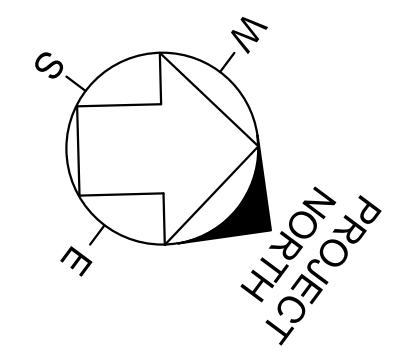
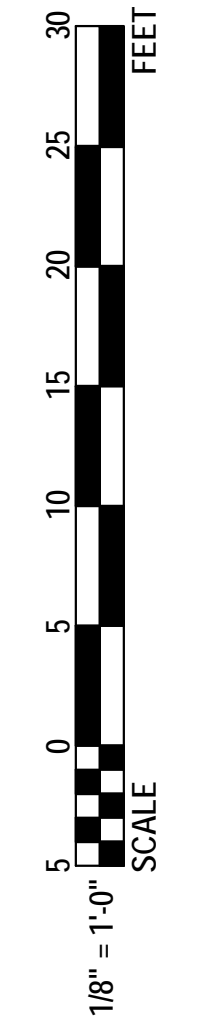
ENCLOSURE PLAN AT TARGET HALL



DATE: **08 MAY 2013**
 PROJECT NO.: **6-13-1**
 DRAWING NO.: **PDR-07**



SCALE:



TARGET HALL BUILDING PLAN SHEET 1



DATE: **08 MAY 2013**

PROJECT NO.: **6-13-1**

DRAWING NO.: **PDR-08**

MECHANICAL ROOM

DIMENSIONS: 20'-0" WIDE BY 23'-6" LONG BY 17'-6" HIGH
 CONSTRUCTION: STEEL FRAMED, METAL SIDED
 HVAC: ELECTRIC UNIT HEATER & VENTILATION
 68°F, NO HUMIDITY CONTROL
 LIGHTING: 30 FC
 EMER. LIGHTING: AS REQUIRED
 EXIT SIGNS: PER CODE
 CONV. RECEPT.: 120/208V AS REQ'D

TOILETS

DIMENSIONS: 11'-0" WIDE BY 9'-0" LONG
 BY 17'-6" HIGH (EACH)
 CONSTRUCTION: 6" PAINTED CONCRETE BLOCK
 WALLS
 SUSPENDED ACT CEILING
 CERAMIC TILE FLOOR

STAIR NU-04

LIGHTING: 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

HIGH BAY

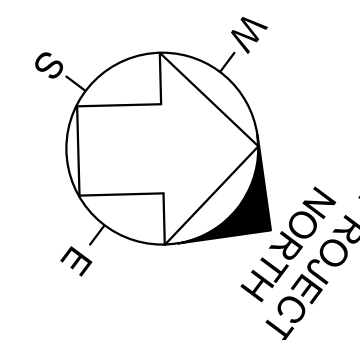
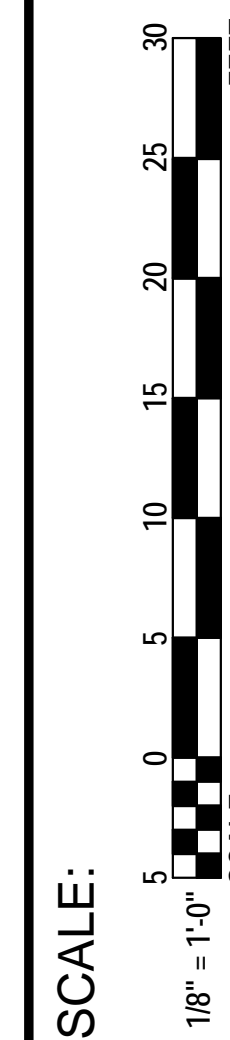
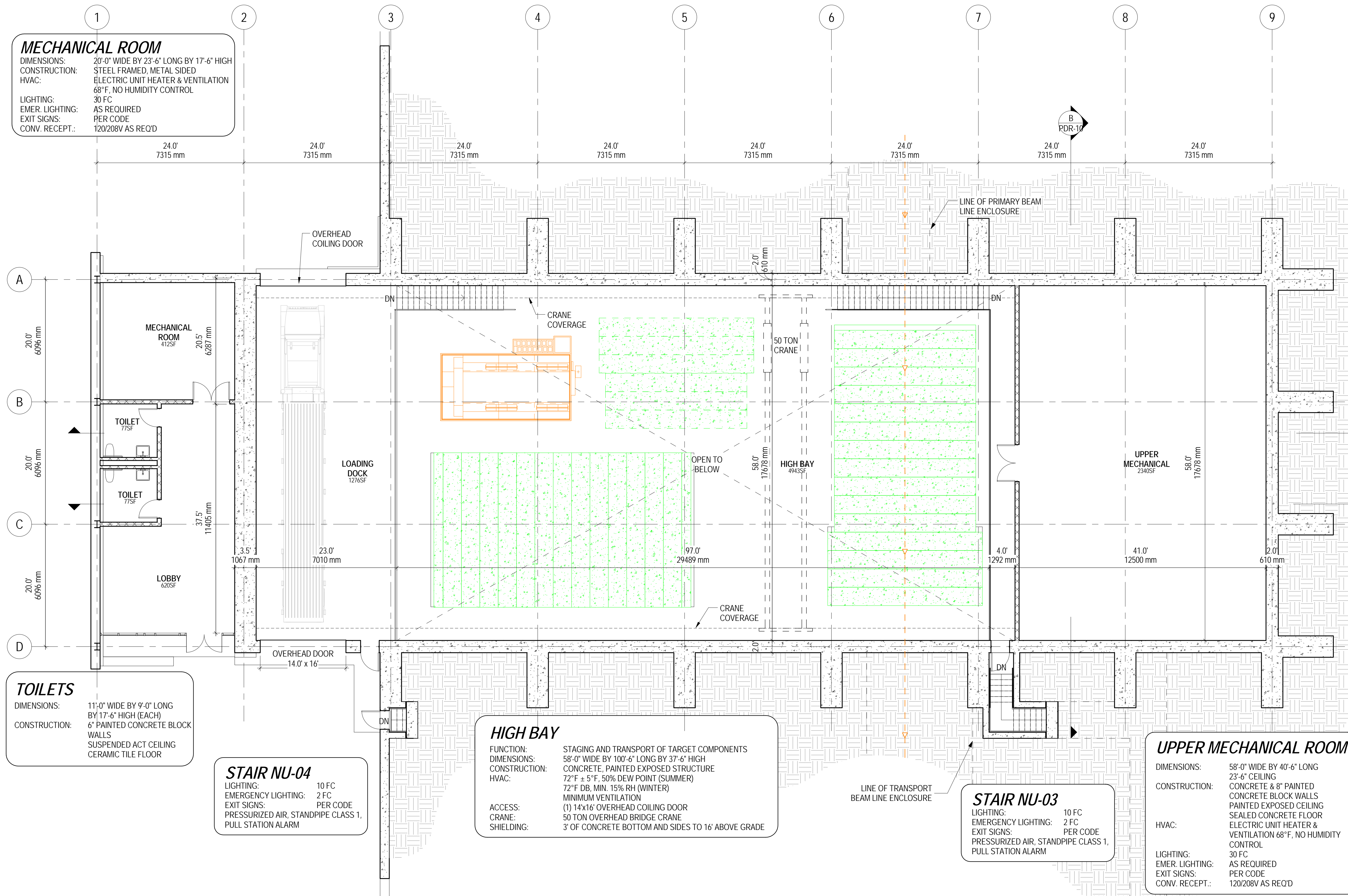
FUNCTION: STAGING AND TRANSPORT OF TARGET COMPONENTS
 DIMENSIONS: 58'-0" WIDE BY 100'-6" LONG BY 37'-6" HIGH
 CONSTRUCTION: CONCRETE, PAINTED EXPOSED STRUCTURE
 HVAC: 72°F ± 5°F, 50% DEW POINT (SUMMER)
 72°F DB, MIN. 15% RH (WINTER)
 MINIMUM VENTILATION
 ACCESS: (1) 14'x16' OVERHEAD COILING DOOR
 CRANE: 50 TON OVERHEAD BRIDGE CRANE
 SHIELDING: 3' OF CONCRETE BOTTOM AND SIDES TO 16' ABOVE GRADE

STAIR NU-03

LIGHTING: 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

UPPER MECHANICAL ROOM

DIMENSIONS: 58'-0" WIDE BY 40'-6" LONG
 CONSTRUCTION: 23'-6" CEILING
 CONCRETE & 8" PAINTED
 CONCRETE BLOCK WALLS
 PAINTED EXPOSED CEILING
 SEALED CONCRETE FLOOR
 ELECTRIC UNIT HEATER &
 VENTILATION 68°F, NO HUMIDITY
 CONTROL
 HVAC: 30 FC
 LIGHTING: AS REQUIRED
 EMER. LIGHTING: PER CODE
 EXIT SIGNS: PER CODE
 CONV. RECEPT.: 120/208V AS REQ'D



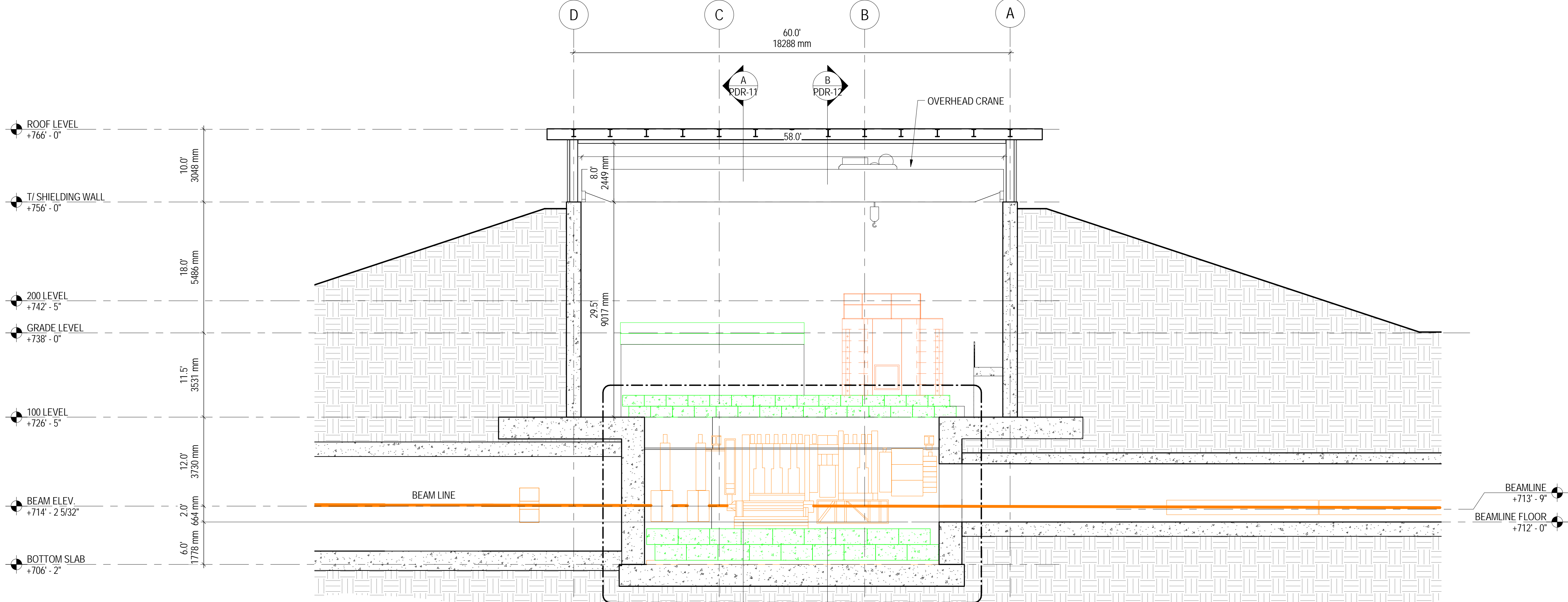
TARGET HALL BUILDING PLAN SHEET 2



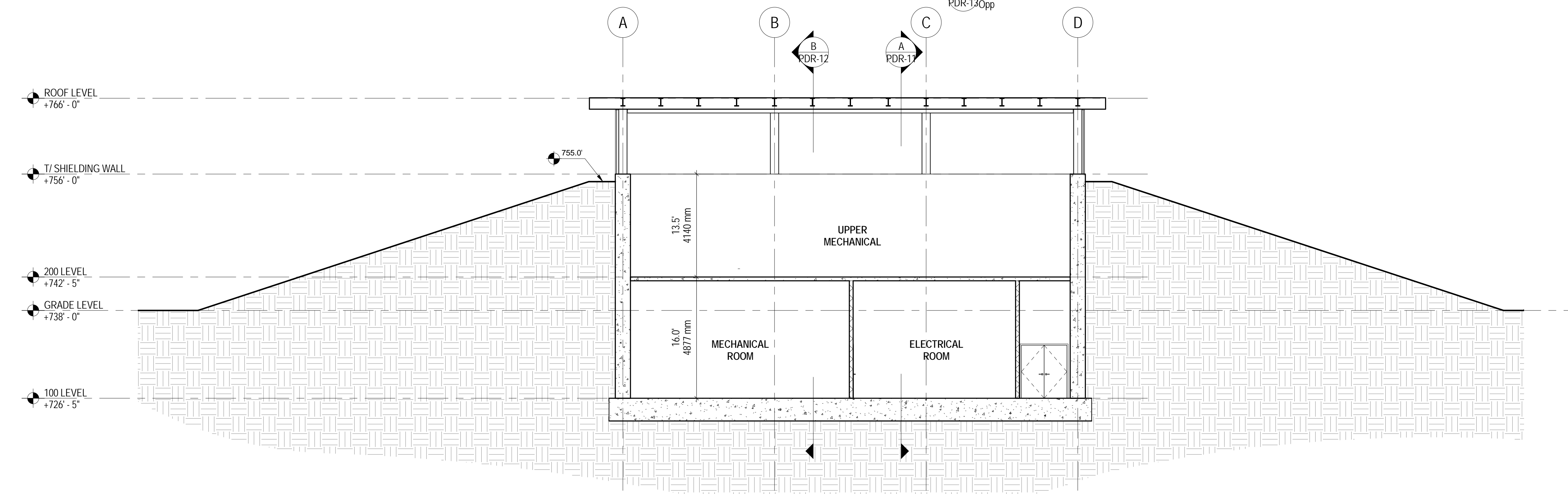
DATE: **08 MAY 2013**
 PROJECT NO.: **6-13-1**
 DRAWING NO.: **PDR-09**

FLOOR PLAN ELEV. 738.00' & 742.50'

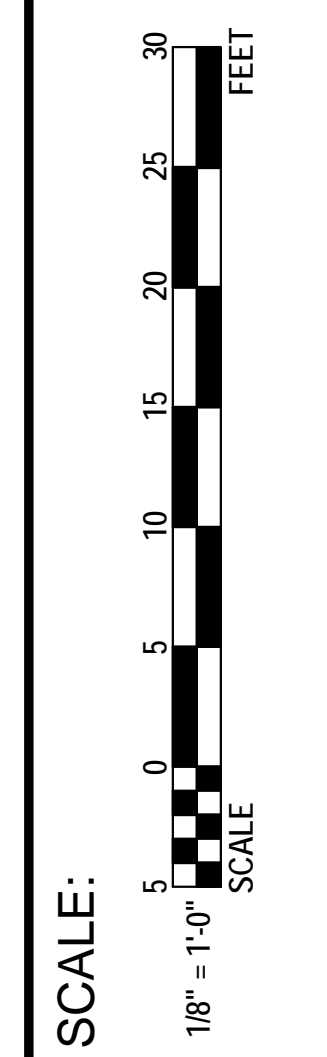
SCALE: 1/8" = 1'-0"



TRANSVERSE SECTION - A
SCALE: 1/8" = 1'-0"



TRANSVERSE SECTION - B
SCALE: 1/8" = 1'-0"



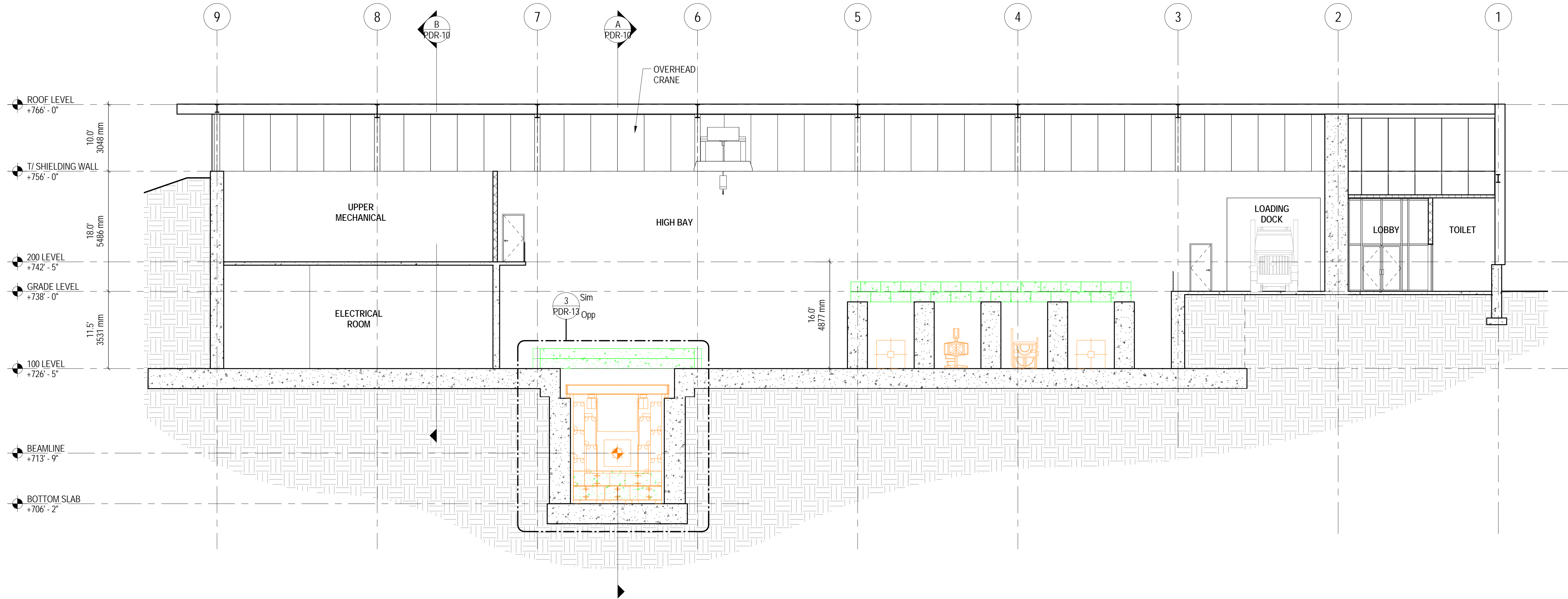
TARGET HALL BUILDING SECTIONS
SHEET 1



DATE
08 MAY 2013

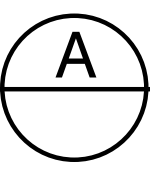
PROJECT NO.
6-13-1

DRAWING NO.
PDR-10

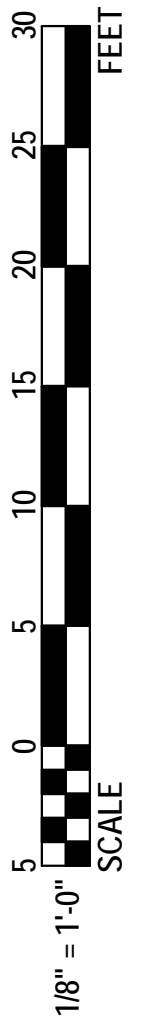


LONGITUDINAL SECTION - A

SCALE: 1/8" = 1'-0"



SCALE:



TARGET HALL BUILDING SECTIONS
SHEET 2



DATE

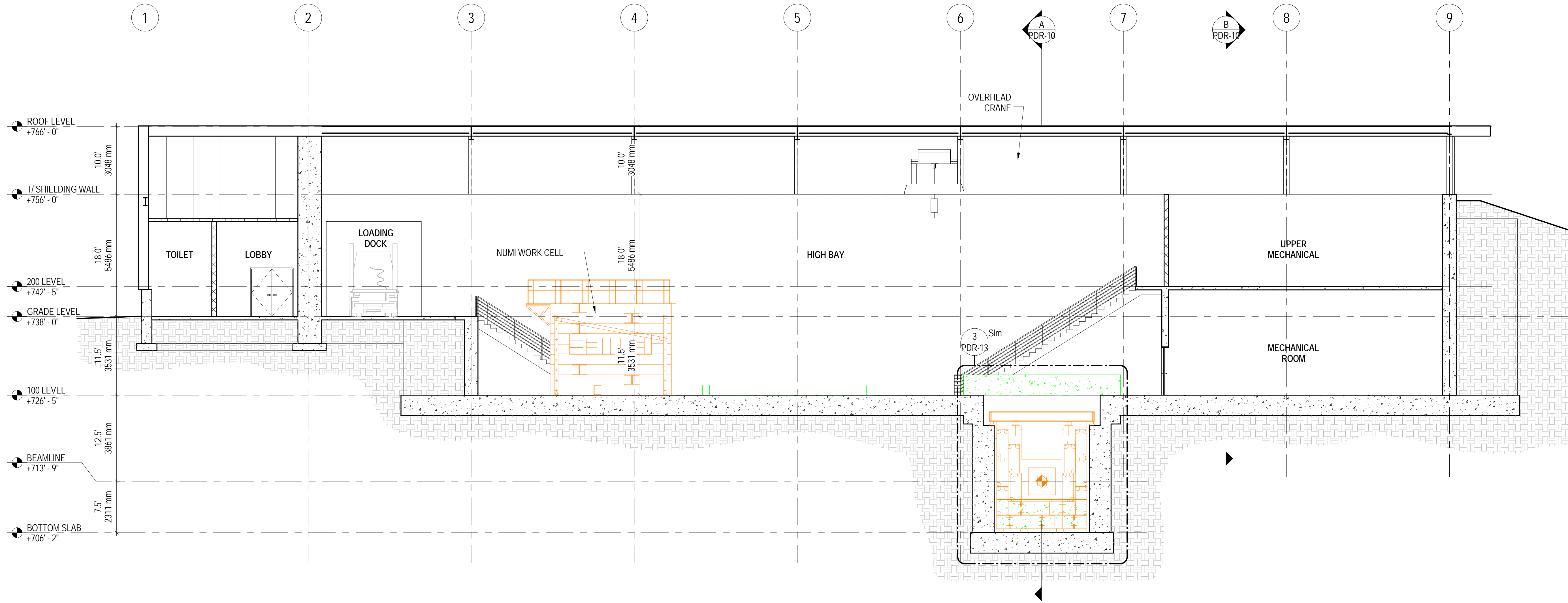
08 MAY 2013

PROJECT NO.

6-13-1

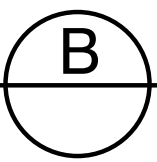
DRAWING NO.

PDR-11

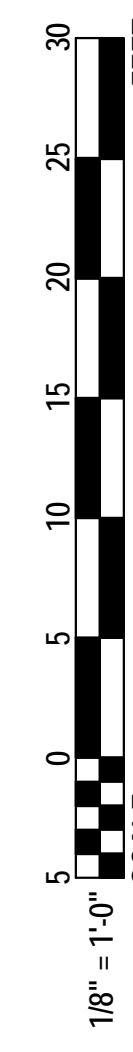


LONGITUDINAL SECTION - B

SCALE: 1/8" = 1'-0"



SCALE:



TARGET HALL BUILDING SECTIONS
SHEET 3



DATE

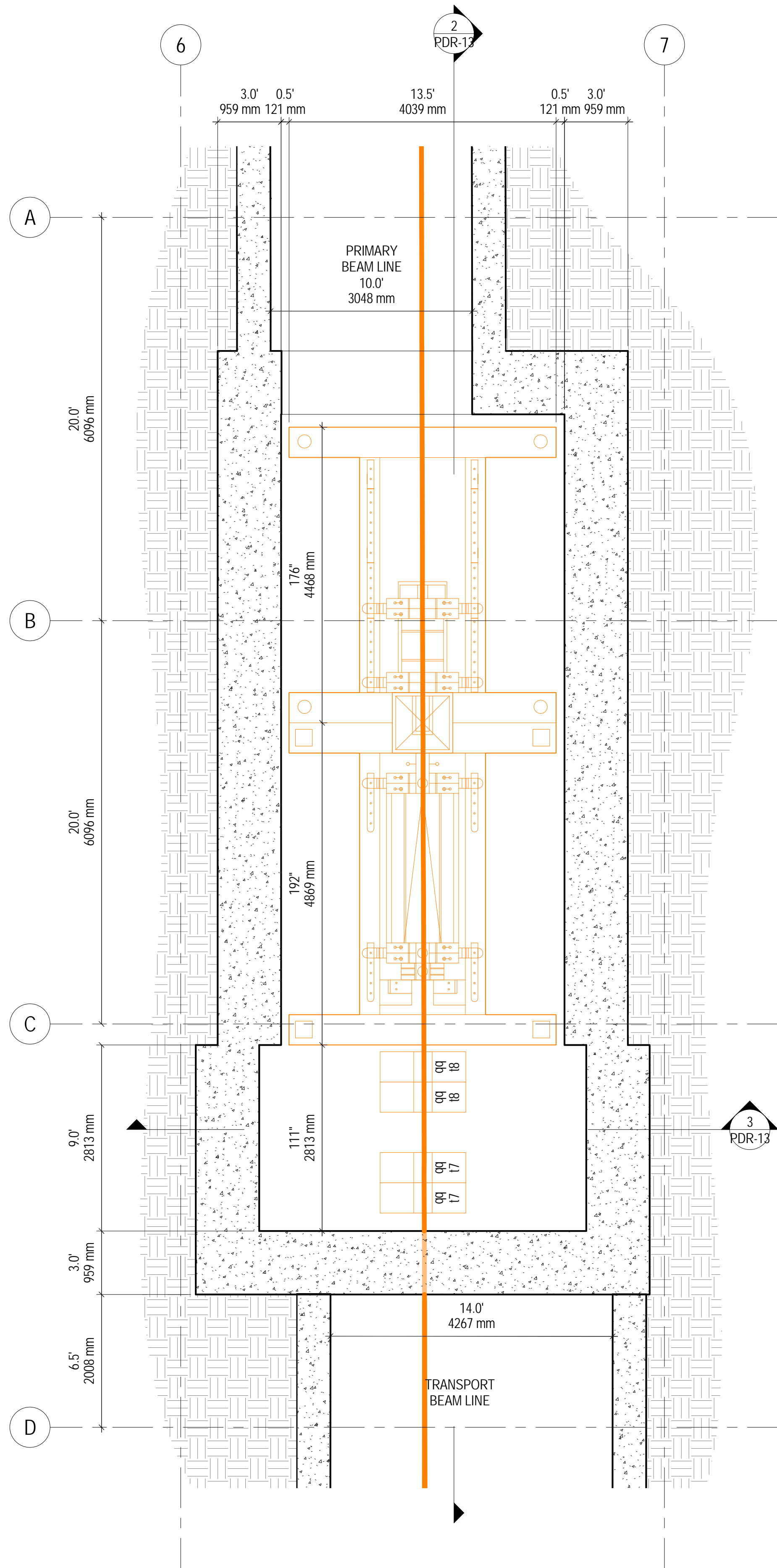
08 MAY 2013

PROJECT NO.

6-13-1

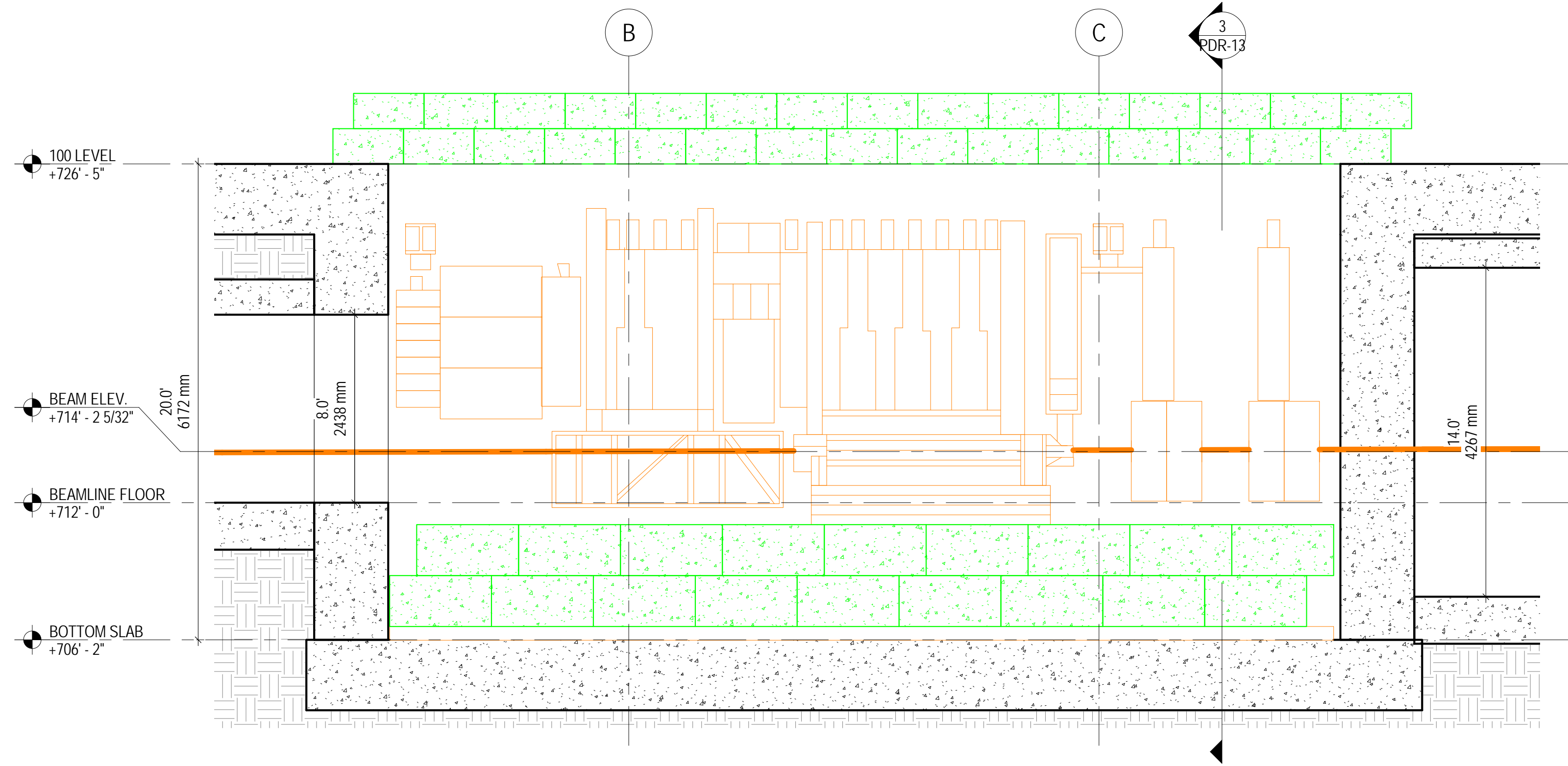
DRAWING NO.

PDR-12



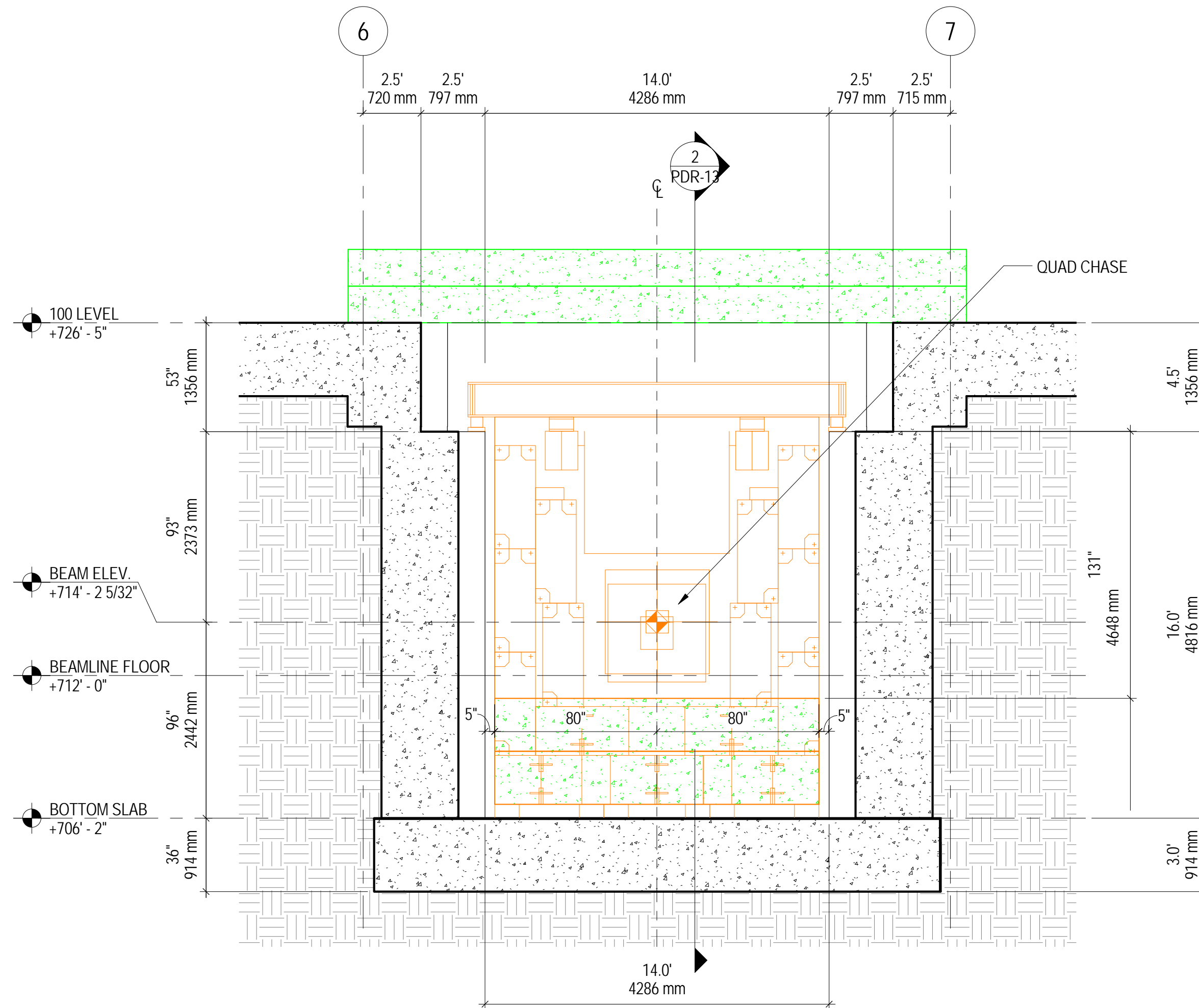
TARGET HALL - 100 LEVEL ENLARGED PLAN

SCALE: 1/4" = 1'-0"



LONGITUDINAL SECTION DETAIL - TARGET

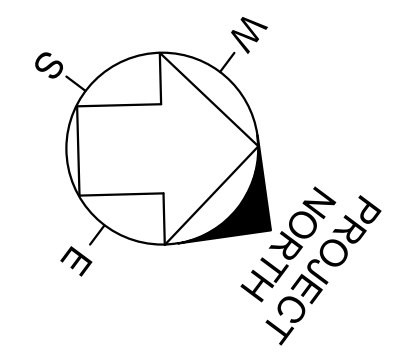
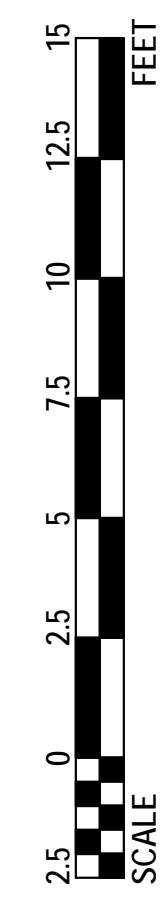
SCALE: 1/4" = 1'-0"



TRANSVERSE SECTION DETAIL - TARGET

SCALE: 1/4" = 1'-0"

SCALE:



ENLARGED PLANS AND SECTIONS



DATE

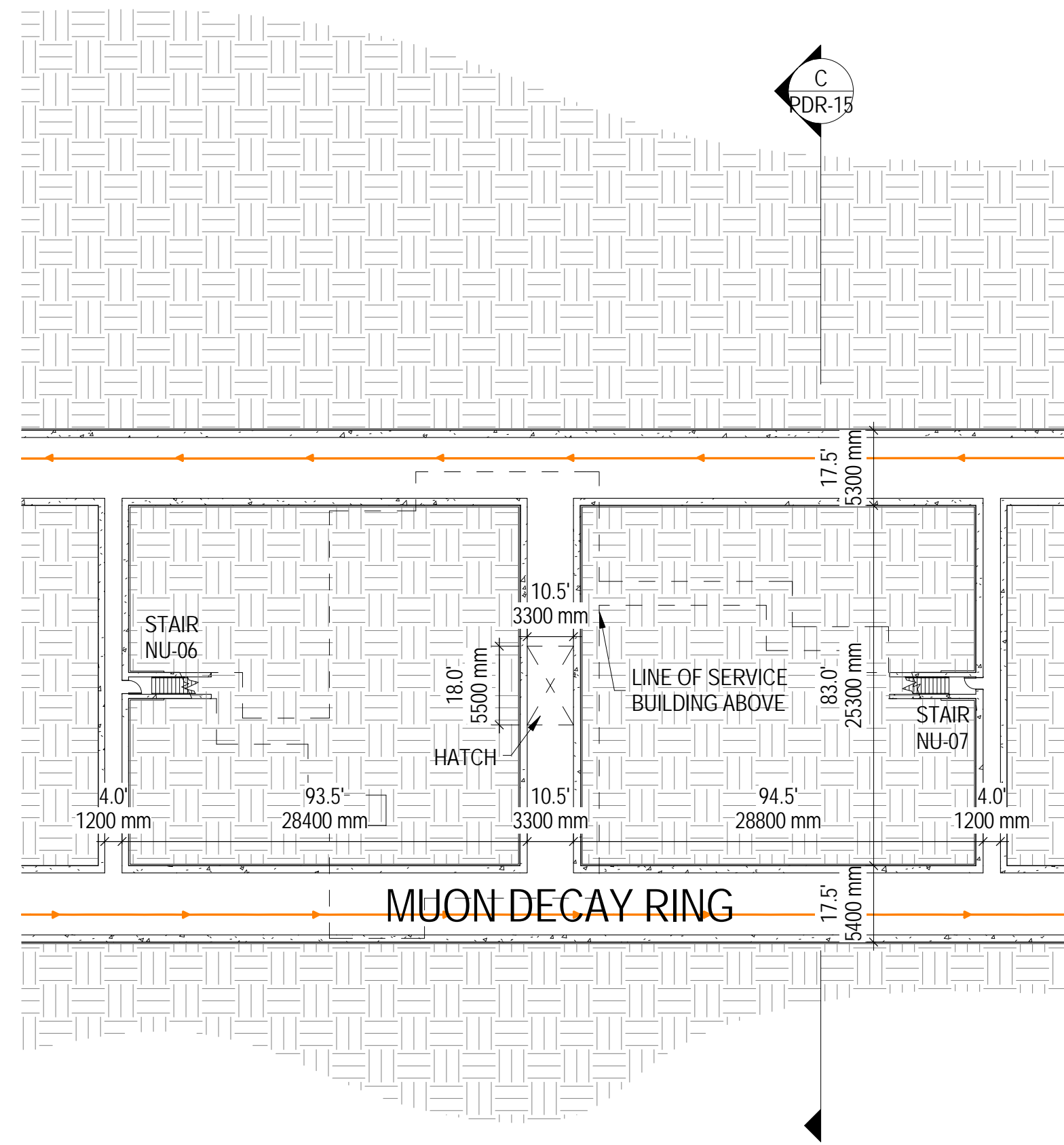
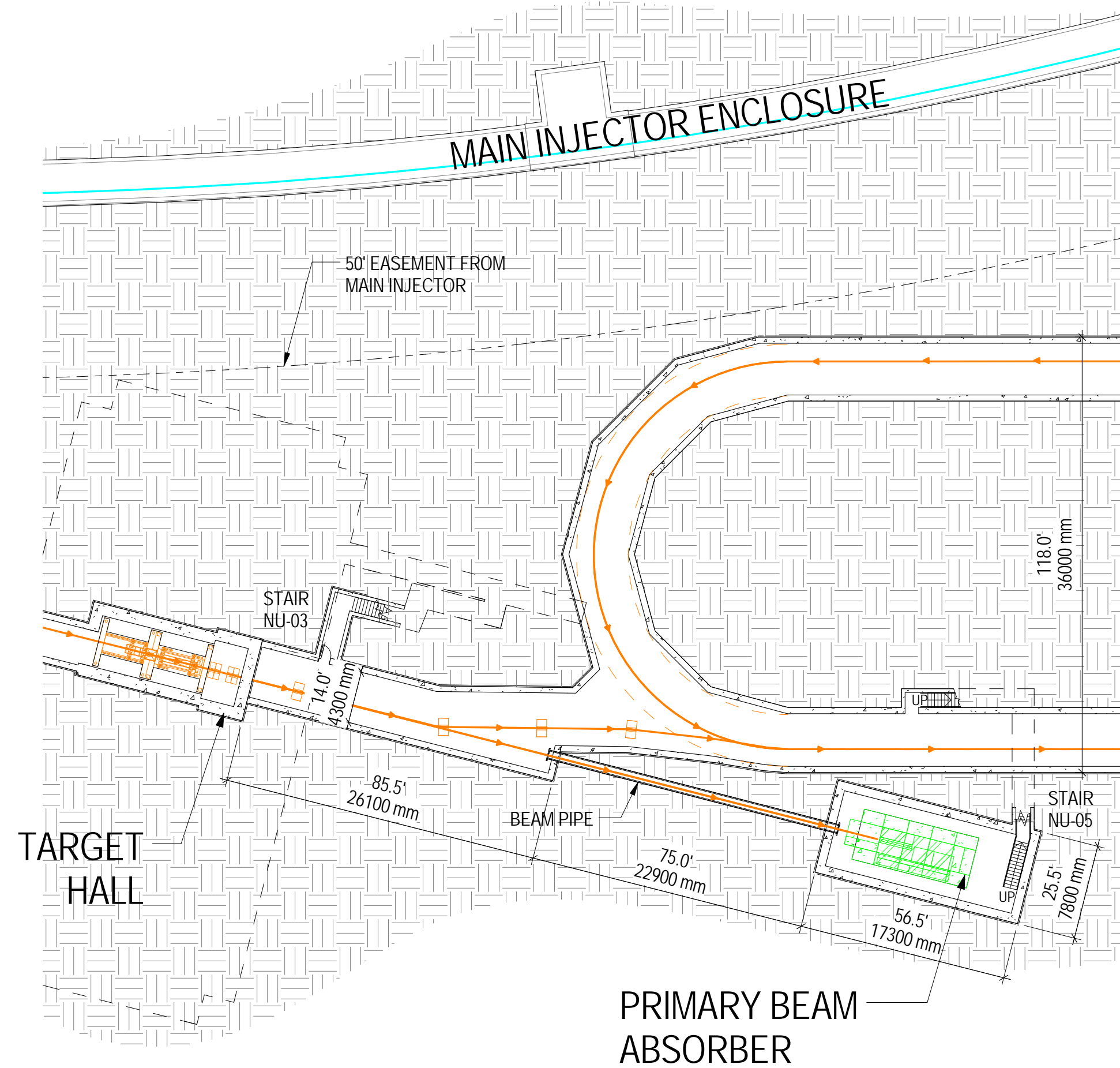
08 MAY 2013

PROJECT NO.

6-13-1

DRAWING NO.

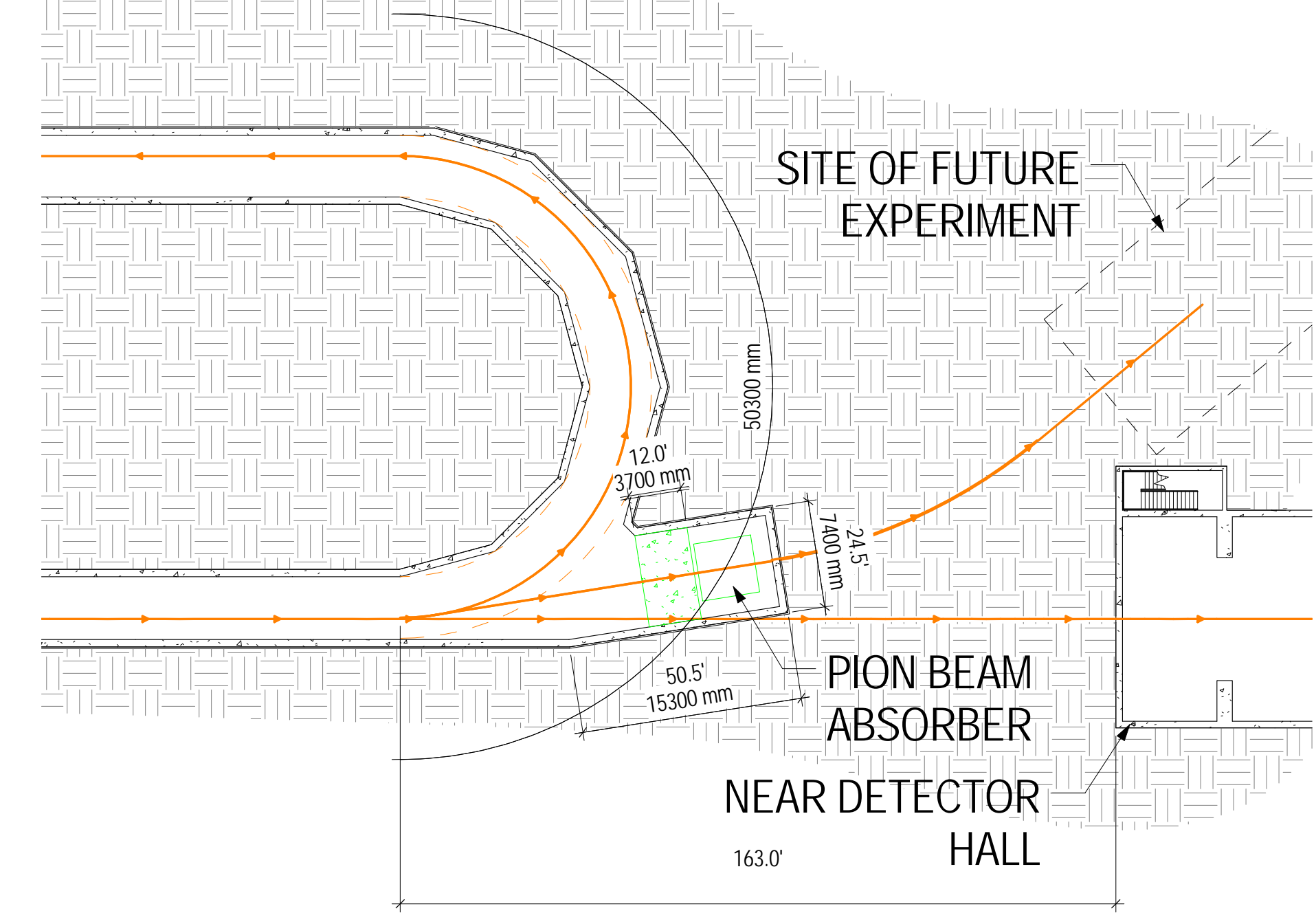
PDR-13



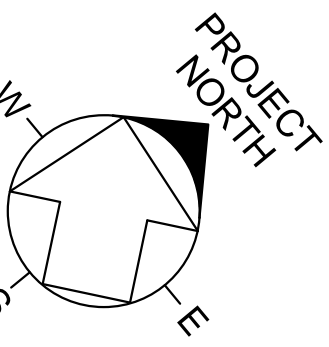
FLOOR PLAN ELEV. 708.00'
SCALE: 1" = 30'-0"

MUON DECAY RING ENCLOSURE

DIMENSIONS:	14' WIDE BY 14' HIGH	SPECIAL:	EXHAUST AND ADMINISTRATION CONTROL ACCESS.
CONSTRUCTION:	CONCRETE	SMOKE CONTROL:	EMERGENCY PERSONNEL MANUAL ACCESS FANS FOR SMOKE ABATEMENT.
FUNCTION:	HOUSE BEAMLINE COMPONENTS	FIRE DETECTION:	AIR SAMPLING SMOKE AND LINEAR TYPE HEAT DETECTION.
SHIELDING:	12 FT EARTH EQUIVALENT	FIRE NOTIFICATION:	AUDIBLE AND VISUAL DEVICES THROUGHOUT.
EQUIPMENT ACCESS:	VIA SHIELDED HATCH		
CABLE TRAY:	(2) 18" BY ACCEL.		
LCW:	LESS THAN 50		
OCCUPANT LOAD:	600 FT. MAXIMUM TRAVEL DISTANCE TO STAIRWAY. STAIRWAY FIRE RATED CONSTRUCTION DISCHARGE TO SURFACE. EMERGENCY LIGHTING AND EXIT SIGNAGE THROUGHOUT, SMOKE PROOF STAIRWAYS.		
EGRESS:			



SCALE:
1/16" = 1'-0"



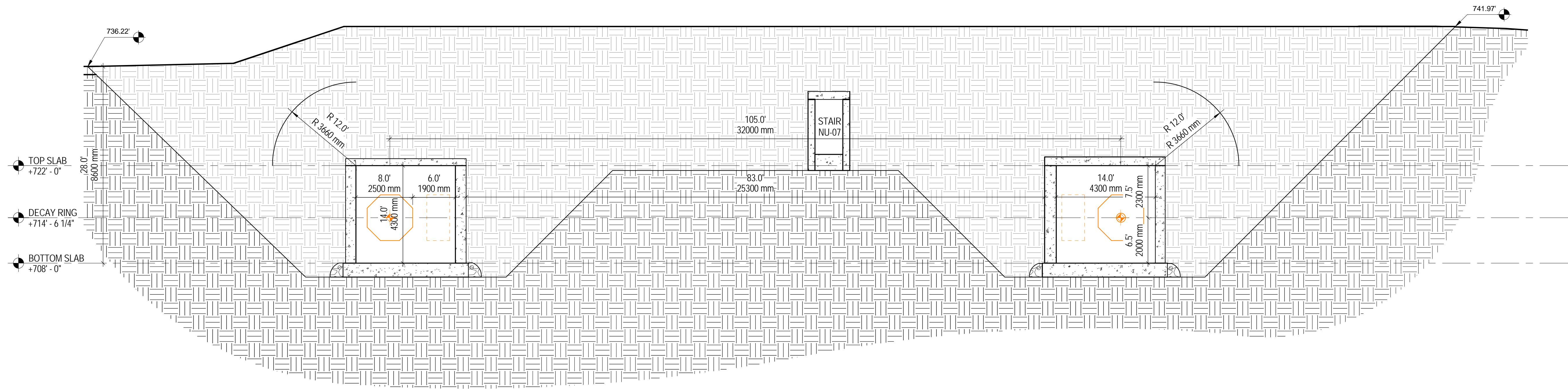
MUON DECAY RING PLAN



DATE
08 MAY 2013

PROJECT NO.
6-13-1

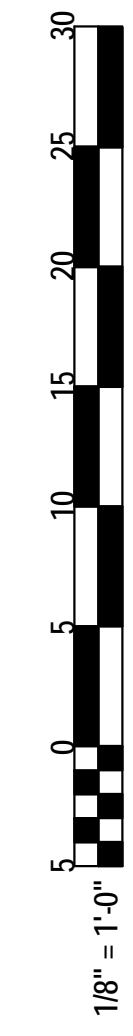
DRAWING NO.
PDR-14



SECTION
SCALE: 1/8" = 1'-0"

C

SCALE:



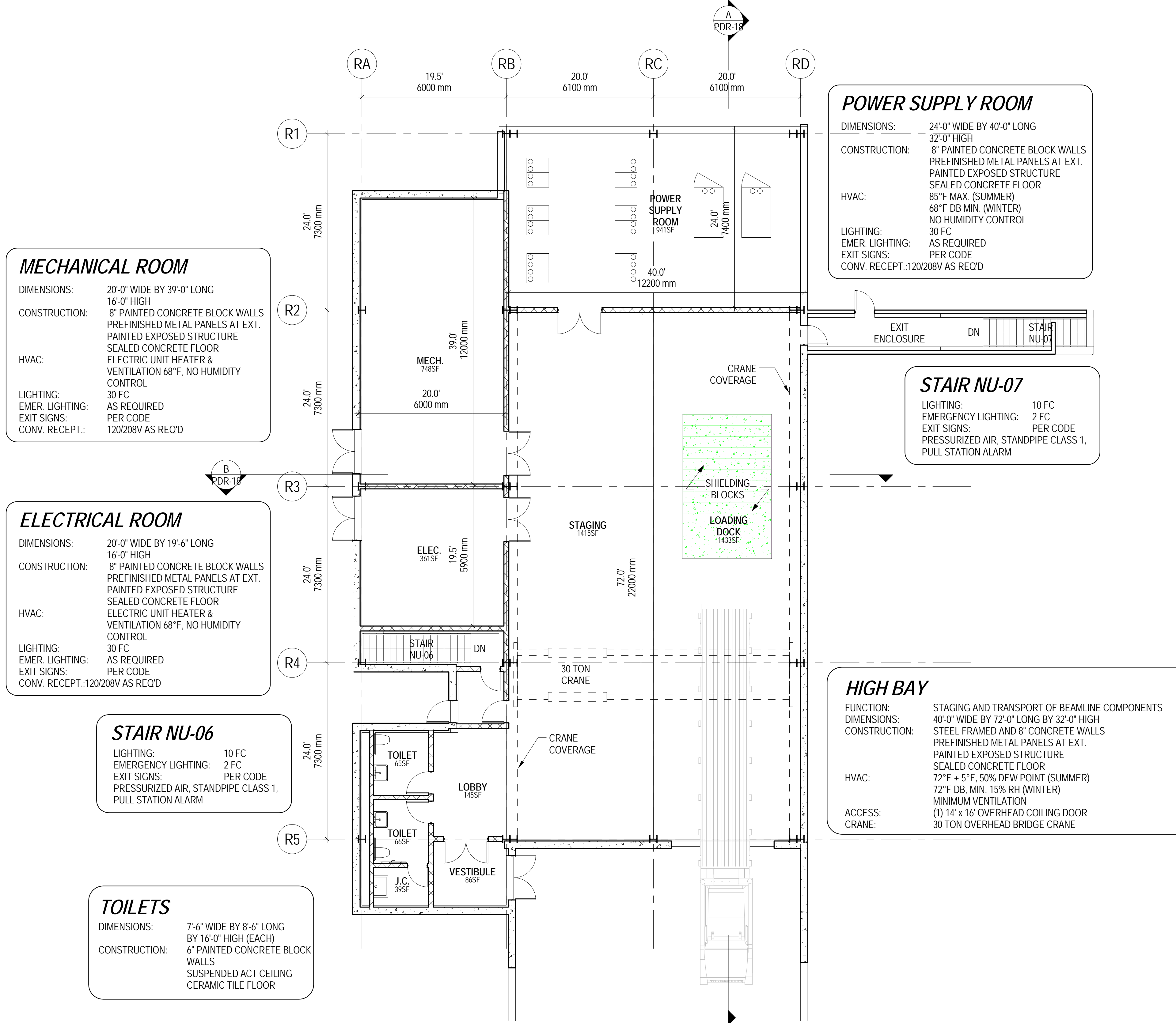
MUON DECAY RING SECTION



DATE
08 MAY 2013

PROJECT NO.
6-13-1

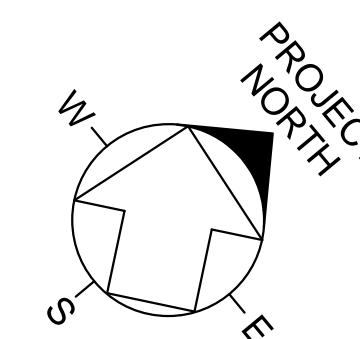
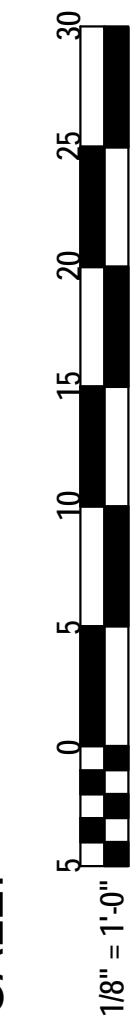
DRAWING NO.
PDR-15



FLOOR PLAN ELEV. 737.50'

SCALE: 1/8" = 1'-0"

SCALE:



MUON DECAY RING BUILDING PLAN



DATE

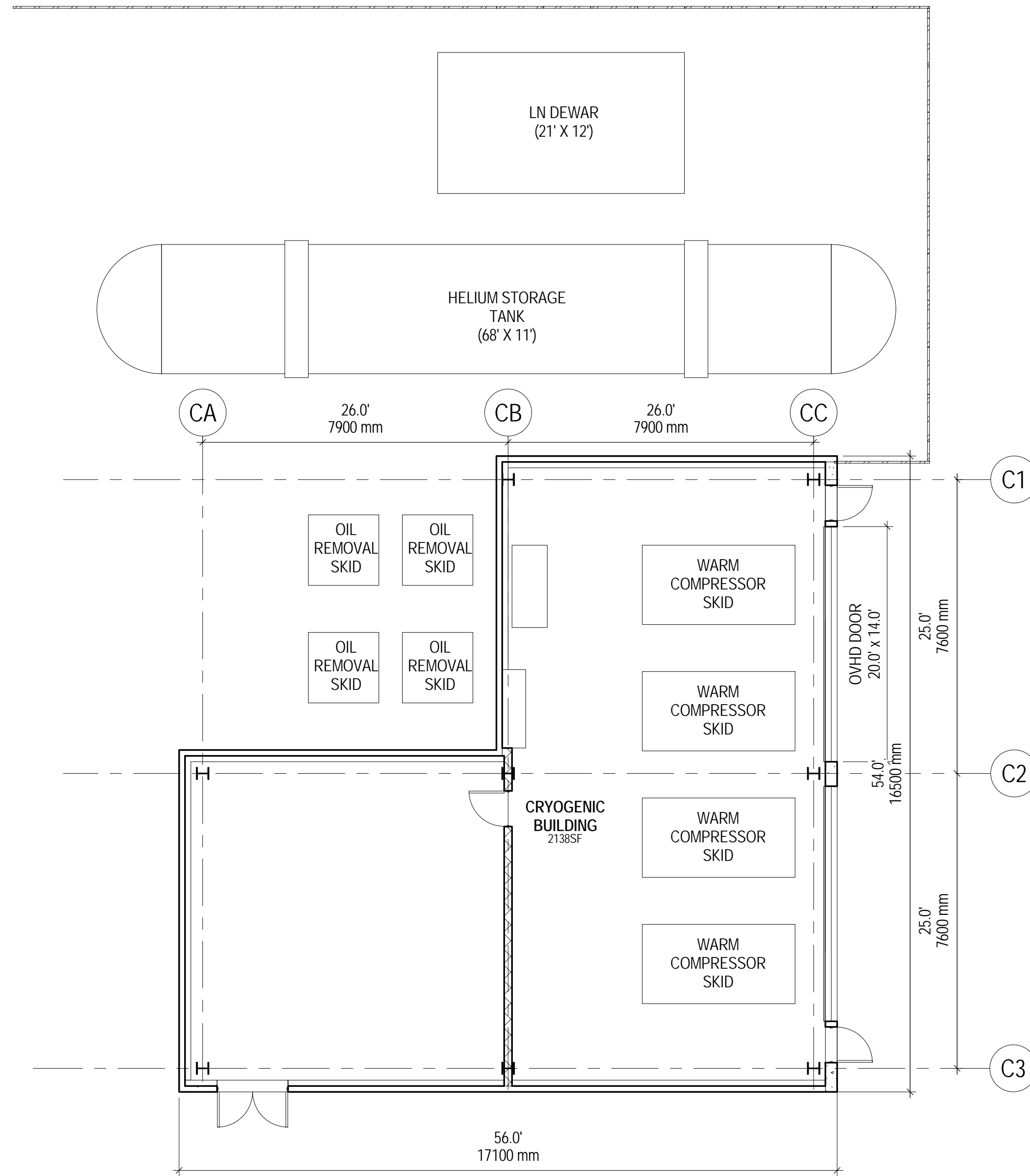
08 MAY 2013

PROJECT NO.

6-13-1

DRAWING NO.

PDR-16



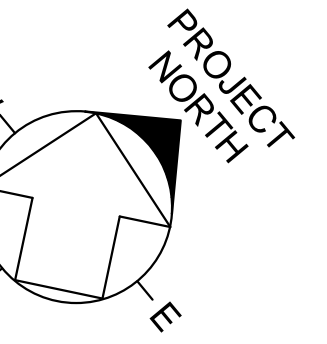
FLOOR PLAN ELEV. 737.50'

SCALE: 1/8" = 1'-0"

CRYOGENIC BUILDING

- FUNCTION:** HOUSES CRYO EQUIPMENT TO PROVIDE SEPARATION FROM SENSITIVE ELECTRONIC EQUIPMENT.
- DIMENSIONS:** 54'-0" WIDE BY 56'-0" LONG
- CONSTRUCTION:** METAL PANELS ON BRACED STEEL FRAME; BUILT UP ROOF ON INSULATION AND METAL DECK
- ACCESS:** (2) 20' x 14' OVERHEAD COILING DOORS FOR EQUIPMENT ACCESS
- HANDLING:** FORKLIFT
- HVAC:** VENTILATION AND HEATING ONLY
MIN. 68°F, NO MIN. RH
- PROCESS WATER:** ICW FOR WARM COMPRESSOR
- PURGE (ODH) VENT.:** REQUIRED
- EGRESS:** 400 FT MAXIMUM TRAVEL DISTANCE TO STAIRWAY, STAIRWAY FIRE RATED CONSTRUCTION DISCHARGE TO SURFACE. EMERGENCY LIGHTING AND EXIT SIGNAGE THROUGHOUT. MANUAL PULLS STATIONS AT EXIT DOORS
- ERRKWCP:** O2 MONITORING SENSORS THROUGHOUT, EXHAUST PURGE FANS AND ADMINISTRATION CONTROL ACCESS PROVIDED.
- SMOKE CONTROL:** EMERGENCY PERSONAL MANUAL ACCESS FANS FOR SMOKE ABATEMENT.
- FIRE DETECTION:** AIR SAMPLING SMOKE & LINEAR TYPE HEAT DETECTION.
- FIRE NOTIFICATION:** AUDIBLE & VISUAL DEVICES THROUGHOUT.
- FIRE SUPPRESSION:** PREACTION (DRY PIPE) AUTOMATIC SPRINKLER SYSTEM (DUAL INTERLOCK)

SCALE:



CRYOGENIC BUILDING PLAN



DATE

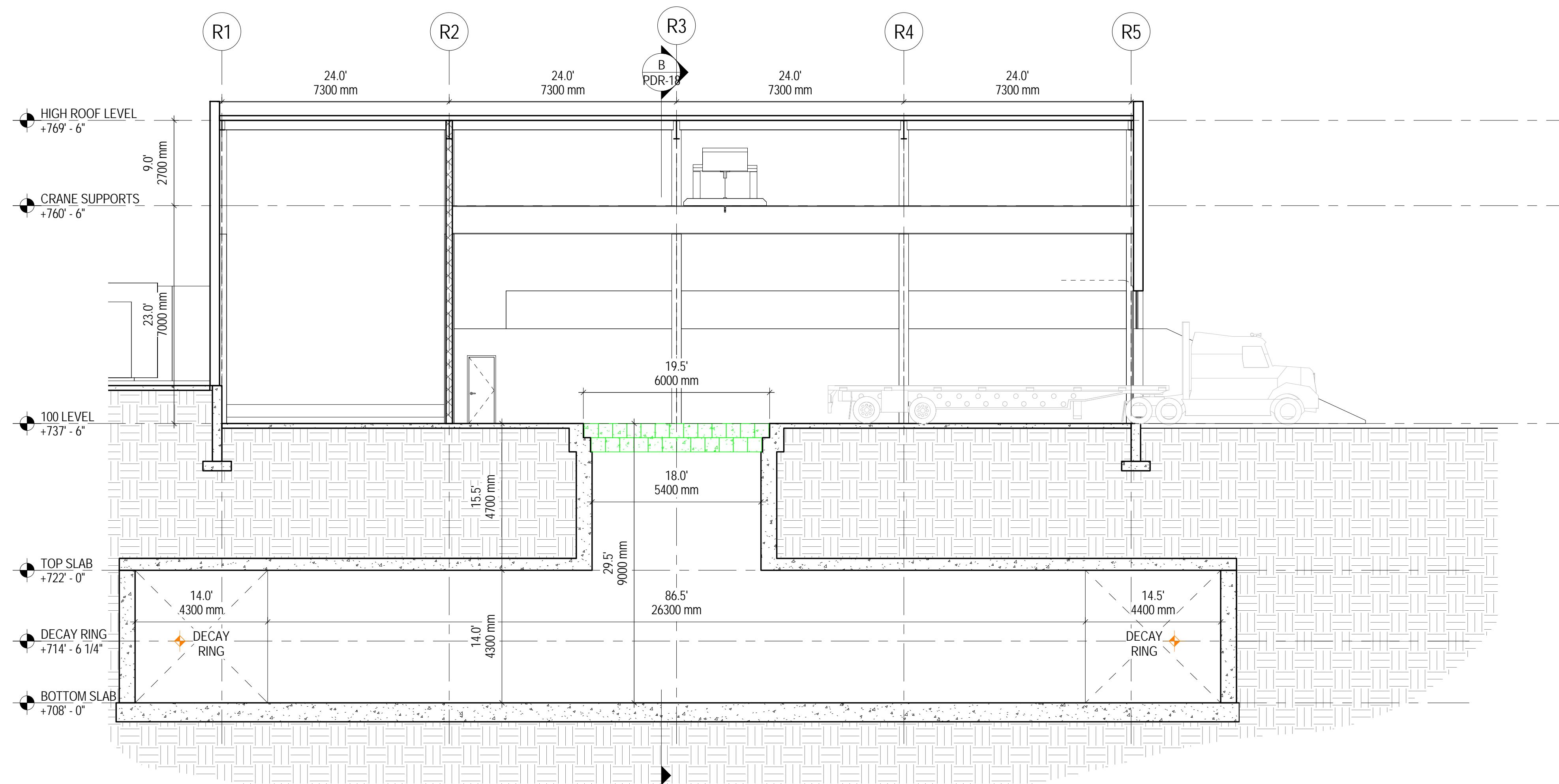
08 MAY 2013

PROJECT NO.

6-13-1

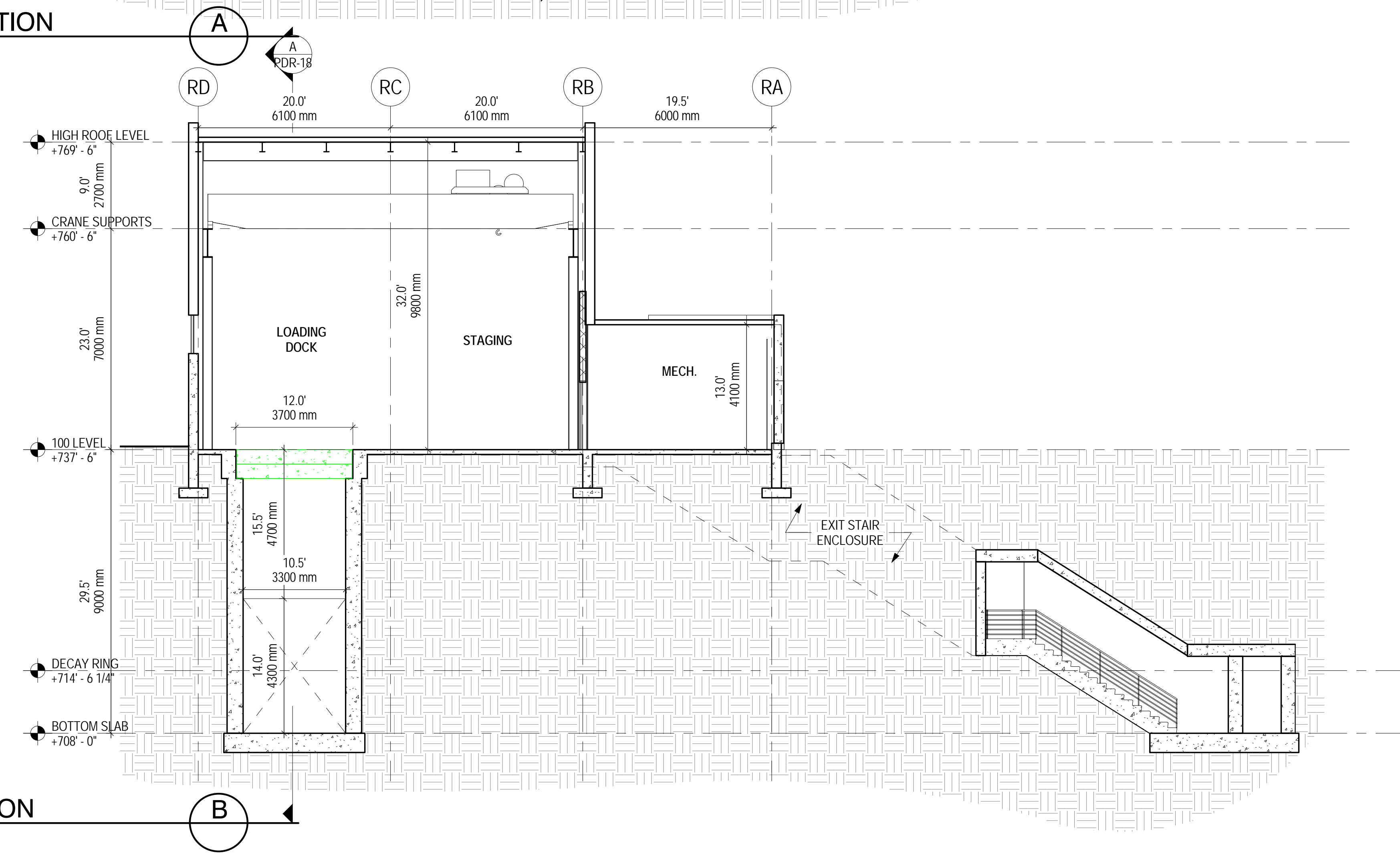
DRAWING NO.

PDR-17



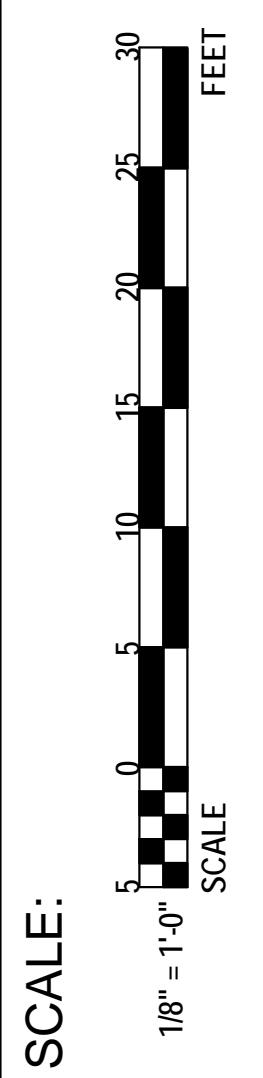
LONGITUDINAL SECTION

SCALE: 1/8" = 1'-0"



TRANSVERSE SECTION

SCALE: 1/8" = 1'-0"



SCALE:

MUON DECAY RING BUILDING SECTIONS



DATE

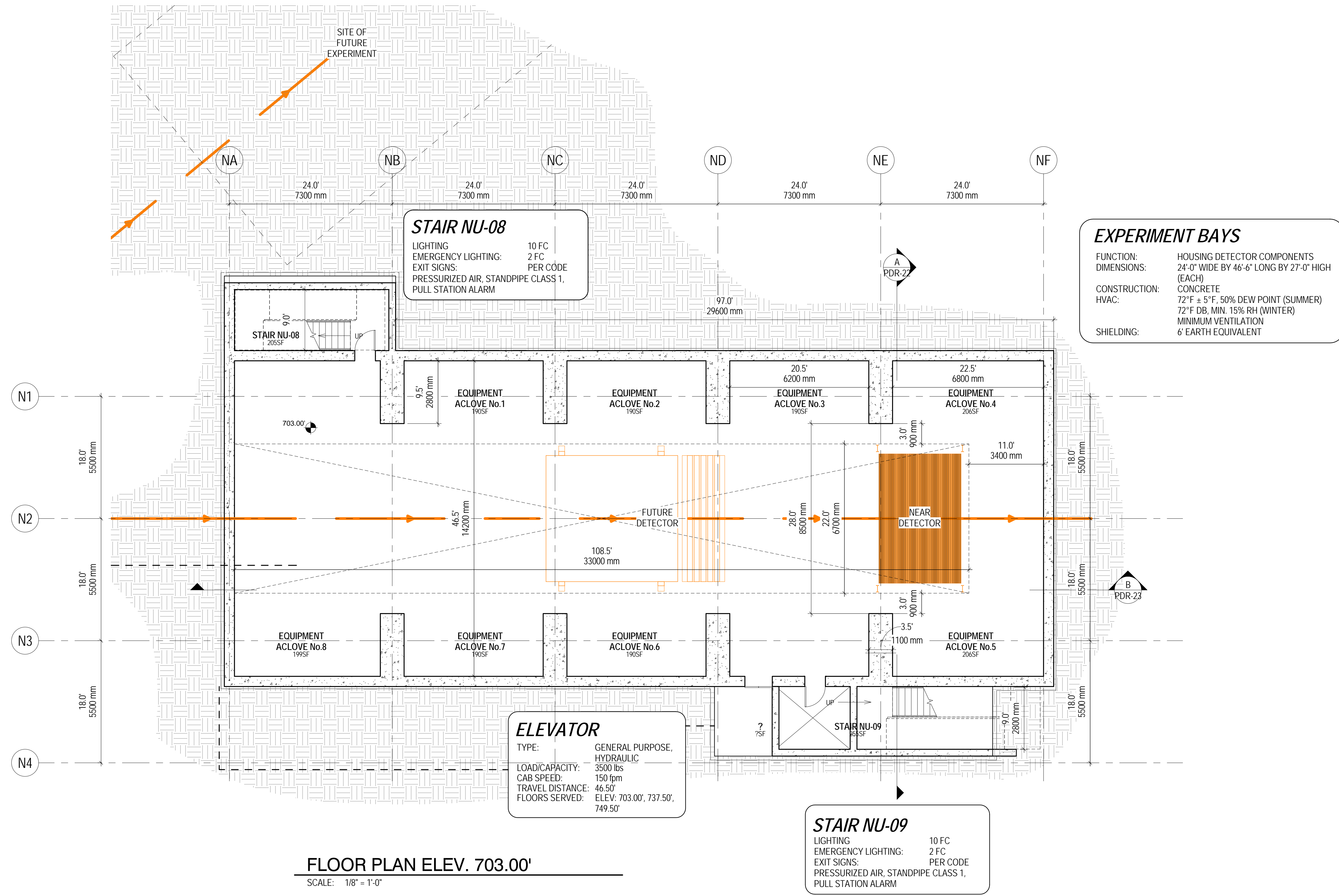
08 MAY 2013

PROJECT NO.

6-13-1

DRAWING NO.

PDR-18



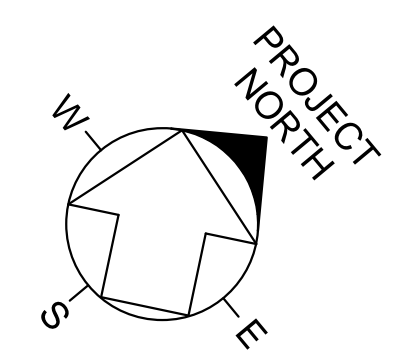
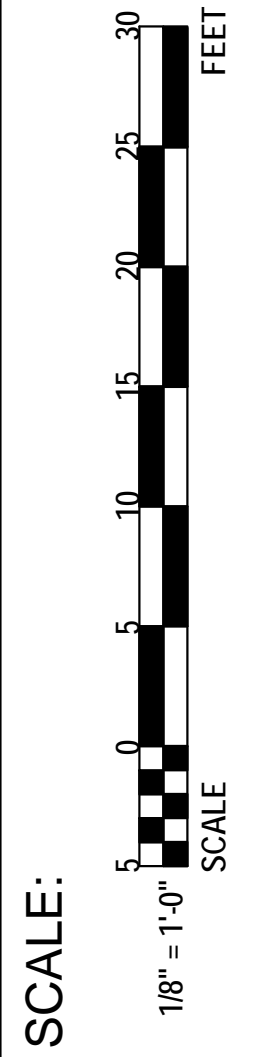
STAIR NU-08
 LIGHTING 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

EXPERIMENT BAYS
 FUNCTION: HOUSING DETECTOR COMPONENTS
 DIMENSIONS: 24'-0" WIDE BY 46'-6" LONG BY 27'-0" HIGH (EACH)
 CONSTRUCTION: CONCRETE
 HVAC: 72°F ± 5°F, 50% DEW POINT (SUMMER)
 72°F DB, MIN. 15% RH (WINTER)
 MINIMUM VENTILATION
 SHIELDING: 6' EARTH EQUIVALENT

ELEVATOR
 TYPE: GENERAL PURPOSE, HYDRAULIC
 LOAD/CAPACITY: 3500 lbs
 CAB SPEED: 150 fpm
 TRAVEL DISTANCE: 46.50'
 FLOORS SERVED: ELEV. 703.00', 737.50', 749.50'

STAIR NU-09
 LIGHTING 10 FC
 EMERGENCY LIGHTING: 2 FC
 EXIT SIGNS: PER CODE
 PRESSURIZED AIR, STANDPIPE CLASS 1,
 PULL STATION ALARM

FLOOR PLAN ELEV. 703.00'
 SCALE: 1/8" = 1'-0"



NEAR DETECTOR HALL FLOOR PLAN SHEET 1



DATE
08 MAY 2013
 PROJECT NO.
6-13-1
 DRAWING NO.
PDR-19

C:\Users\Matl_B\Documents\152381B-ARCH-NEAR_Matl_B.rvt 5/29/2013 11:27:25 AM

HIGH BAY

FUNCTION: PROVIDE INSTALLATION AND ASSEMBLY OF nuSTORM NEAR DETECTOR AND PROVIDE SPACE FOR FUTURE DETECTORS
DIMENSIONS: 317'-0" WIDE BY 169'-0" LONG BY 29'-6" HIGH
CONSTRUCTION: CONCRETE
SHIELDING: BOTTOM & SIDES: 1'-6" CONCRETE W/ 4'-6" EARTH
 TOP: 6'-0" CONC. (2 LAYERS OF 3'-0" CONC. SHIELDING BLOCKS)
EQUIPMENT ACCESS: (1) 14' X 16' OVERHEAD ROLLUP DOOR FOR SEMI TRUCK ACCESS
CRANE: (2) 30 TON OVERHEAD BRIDGE CRANES
HVAC: SUMMER: 72°F (+/- 5°F), 50°F DEW POINT
 WINTER: 72°F, MIN. 15% RH
EGRESS: VENTILATION: TBD
 400 FOOT MAXIMUM TRAVEL DISTANCE TO STAIRWAY. STAIRWAY TO BE OF FIRE RATED CONSTRUCTION; DISCHARGE TO SURFACE.
SMOKE CONTROL: EMERGENCY LIGHTING AND EXIT SIGNAGE THROUGHOUT MANUAL; PULL STATIONS AT EXIT DOORS. EMERGENCY PERSONAL MANUAL ACCESS FANS FOR SMOKE ABATEMENT
FIRE DETECTION: AIR SAMPLING SMOKE & LINEAR TYPE HEAT DETECTION
FIRE NOTIFICATION: AUDIBLE AND VISUAL DEVICES THROUGHOUT
FIRE SUPPRESSION: PREACTION (DRY PIPE) AUTOMATIC SPRINKLER SYSTEM (DUAL INTERLOCK)

MECHANICAL ROOM

DIMENSIONS: 24'-0" WIDE BY 17'-6" LONG
 16'-0" HIGH
CONSTRUCTION: 8" PAINTED CONCRETE BLOCK WALLS
 PREFINISHED METAL PANELS AT EXT.
 PAINTED EXPOSED STRUCTURE
 SEALED CONCRETE FLOOR
 ELECTRIC UNIT HEATER & VENTILATION 68°F, NO HUMIDITY CONTROL
HVAC:
LIGHTING: 30 FC
EMER. LIGHTING: AS REQUIRED
EXIT SIGNS: PER CODE
CONV. RECEPT.: 120/208V AS REQ'D

ELECTRICAL ROOM

DIMENSIONS: 22'-6" WIDE BY 17'-6" LONG
 16'-0" HIGH
CONSTRUCTION: 8" PAINTED CONCRETE BLOCK WALLS
 PREFINISHED METAL PANELS AT EXT.
 PAINTED EXPOSED STRUCTURE
 SEALED CONCRETE FLOOR
 ELECTRIC UNIT HEATER & VENTILATION 68°F, NO HUMIDITY CONTROL
HVAC:
LIGHTING: 30 FC
EMER. LIGHTING: AS REQUIRED
EXIT SIGNS: PER CODE
CONV. RECEPT.: 120/208V AS REQ'D

TOILETS

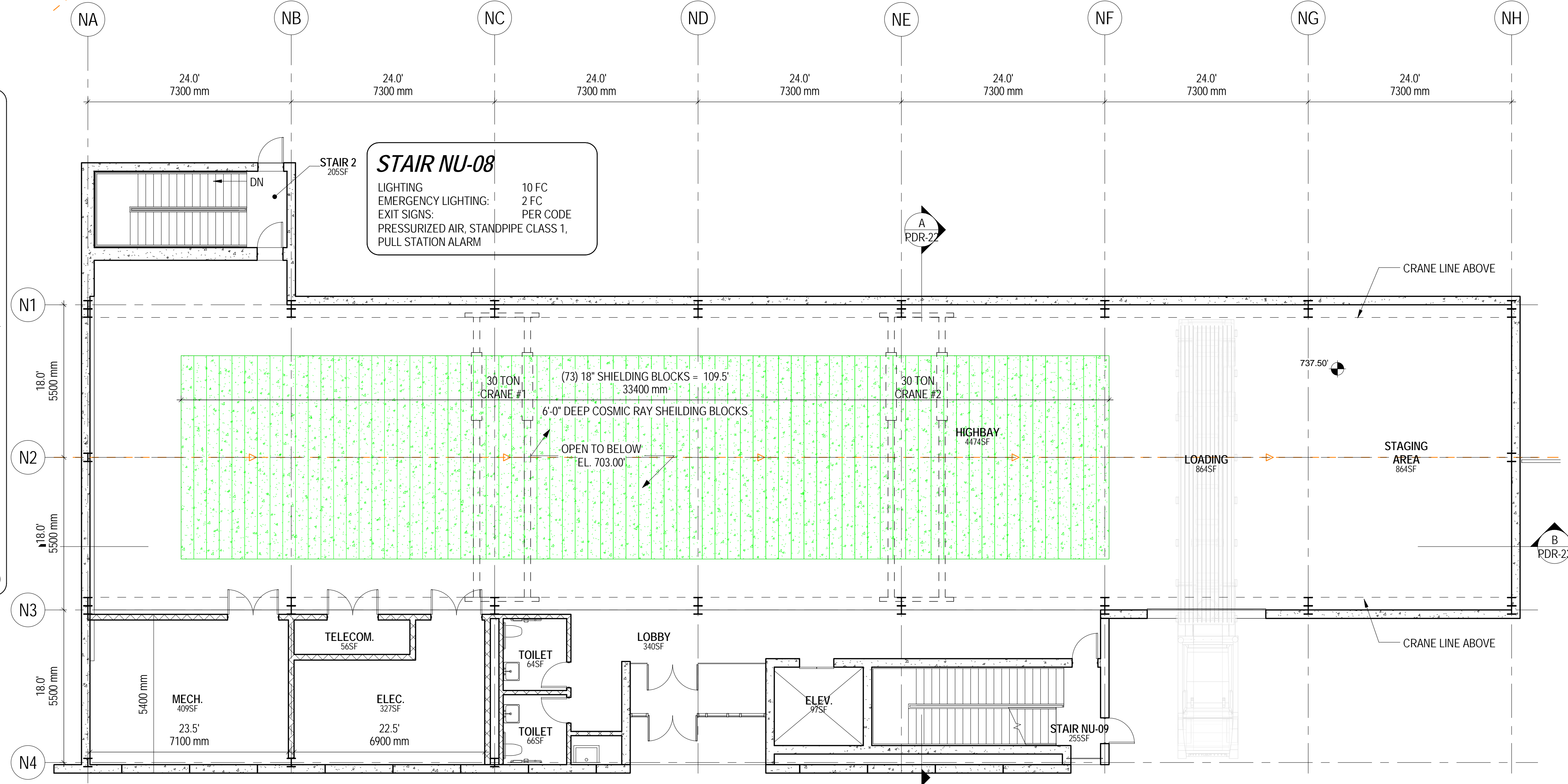
DIMENSIONS: 7'-6" WIDE BY 8'-6" LONG
 BY 16'-0" HIGH (EACH)
CONSTRUCTION: 6" PAINTED CONCRETE BLOCK WALLS
 SUSPENDED ACT CEILING
 CERAMIC TILE FLOOR

ELEVATOR

TYPE: GENERAL PURPOSE, HYDRAULIC
LOAD/CAPACITY: 3500 lbs
CAB SPEED: 150 fpm
TRAVEL DISTANCE: 46.50'
FLOORS SERVED: ELEV: 703.00', 737.50', 749.50'

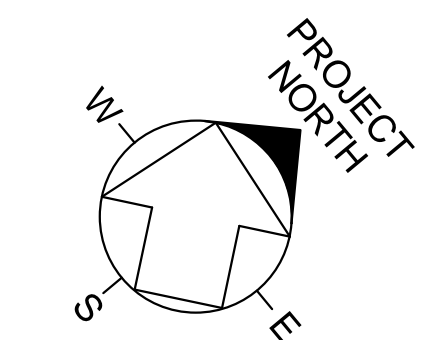
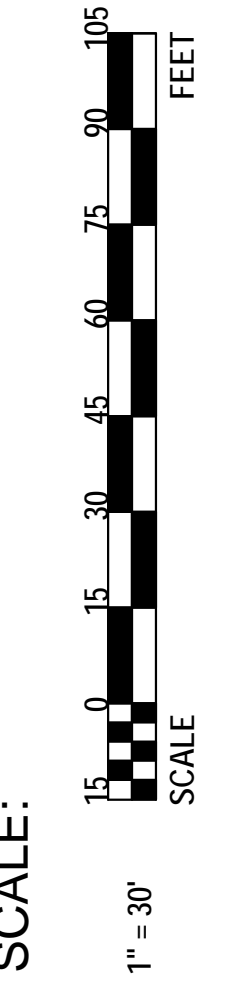
STAIR NU-09

LIGHTING: 10 FC
EMERGENCY LIGHTING: 2 FC
EXIT SIGNS: PER CODE
PRESSURIZED AIR, STANDPIPE CLASS 1,
PULL STATION ALARM



FLOOR PLAN ELEV. 737.50'

SCALE: 1/8" = 1'-0"



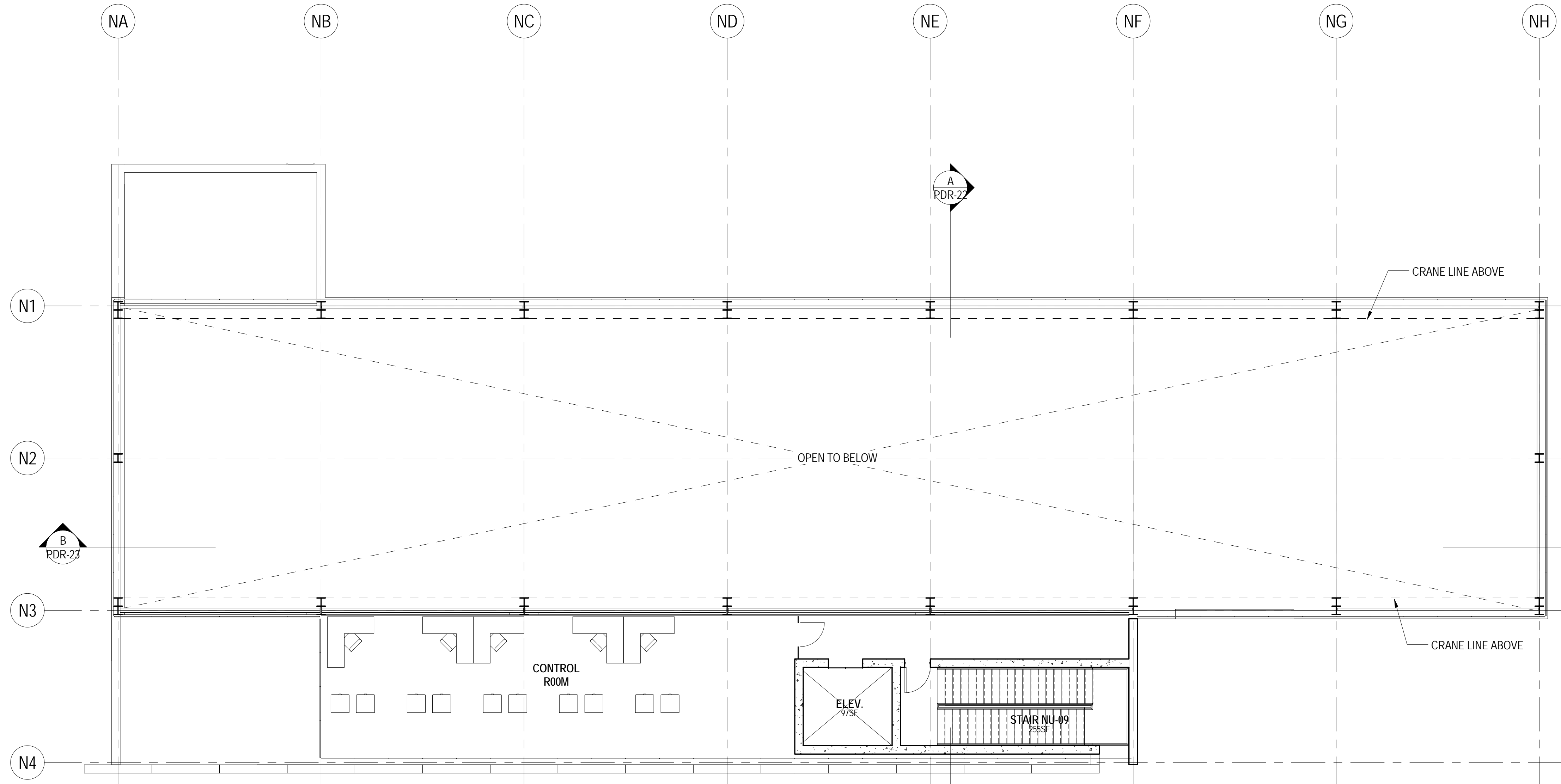
NEAR DETECTOR HALL FLOOR PLAN SHEET 2



DATE
08 MAY 2013

PROJECT NO.
6-13-1

DRAWING NO.
PDR-20



CONTROL ROOM	
HVAC:	85°F AT 55% RH MAX. 21% RH MIN.
PROCESS WATER:	NONE
ODH VENTILATION:	NONE
SMOKE CONTROL:	EMERGENCY PERSONAL MANUAL AIR SAMPLING SMOKE DETECTION
FIRE DETECTION:	AUDIBLE AND VISUAL DEVICES THROUGHOUT
FIRE NOTIFICATION:	PREACTION (DRY) AUTOMATIC SPRINKLER SYSTEM (DUAL INTERLOCK)
FIRE SUPPRESSION:	

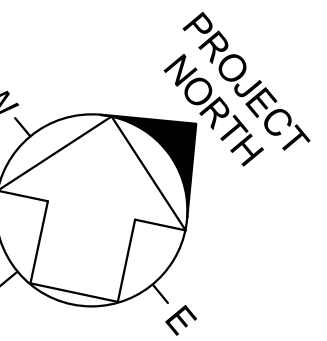
ELEVATOR	
TYPE:	GENERAL PURPOSE, HYDRAULIC
LOAD/CAPACITY:	3500 lbs
CAB SPEED:	150 fpm
TRAVEL DISTANCE:	46.50'
FLOORS SERVED:	ELEV: 703.00', 737.50', 749.50'

STAIR NU-09	
LIGHTING	10 FC
EMERGENCY LIGHTING:	2 FC
EXIT SIGNS:	PER CODE
PRESSURIZED AIR, STANDPIPE CLASS 1, PULL STATION ALARM	

FLOOR PLAN ELEV. 749.50'

SCALE: 1/8" = 1'-0"

SCALE:



**NEAR DETECTOR HALL FLOOR PLAN
SHEET 3**



DATE

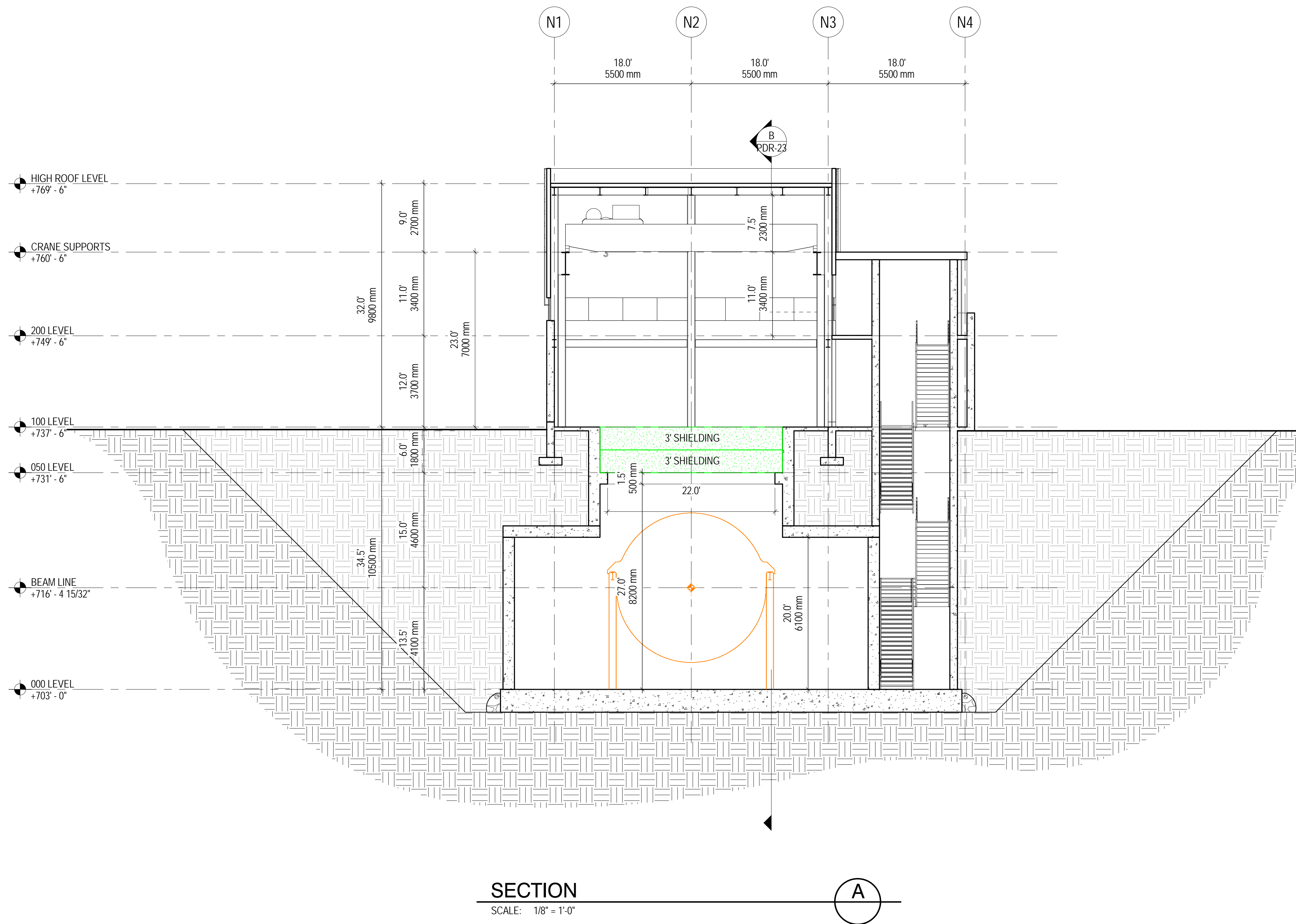
08 MAY 2013

PROJECT NO.

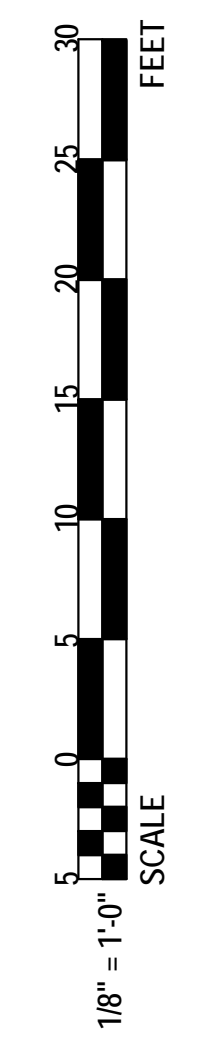
6-13-1

DRAWING NO.

PDR-21



SCALE:



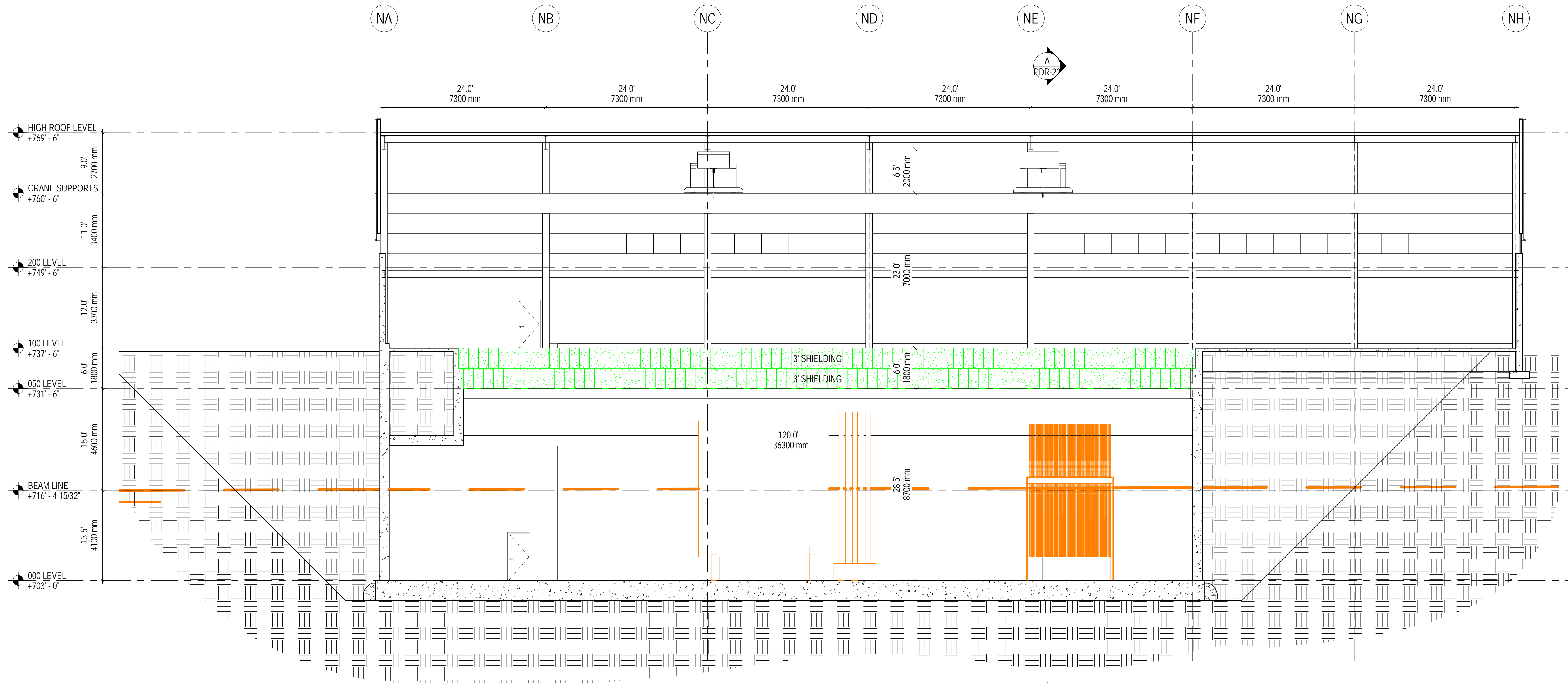
BUILDING & ENCLOSURE SECTION
SHEET 1



DATE
08 MAY 2013

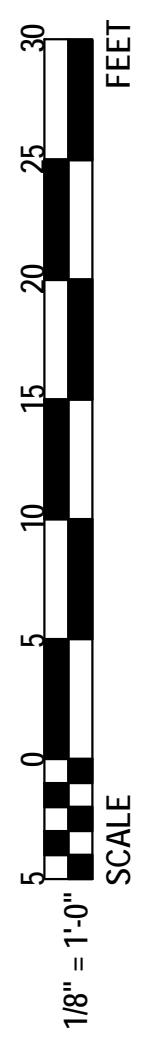
PROJECT NO.
6-13-1

DRAWING NO.
PDR-22



SECTION
SCALE: 1/8" = 1'-0"
B

SCALE:



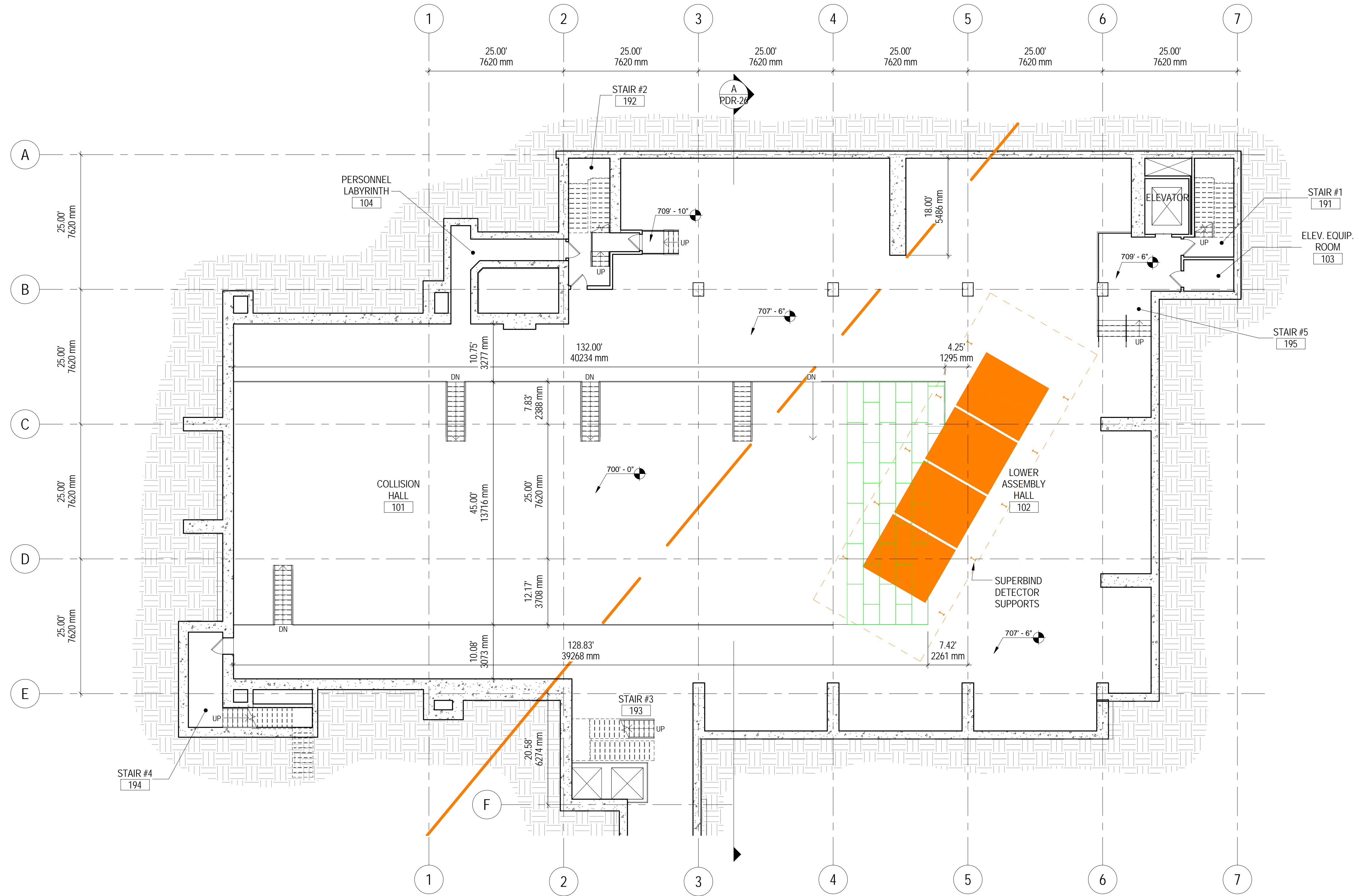
**BUILDING & ENCLOSURE SECTION
SHEET 2**



DATE
08 MAY 2013

PROJECT NO.
6-13-1

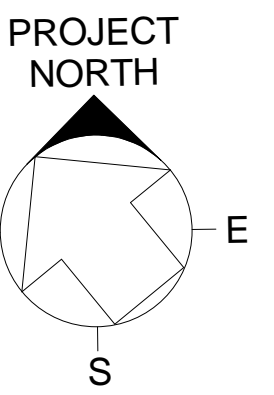
DRAWING NO.
PDR-23



FLOOR PLAN ELEV. 700.00' & 707.50'

SCALE: 3/32" = 1'-0"

SCALE:



FAR DETECTOR FLOOR PLAN



DATE

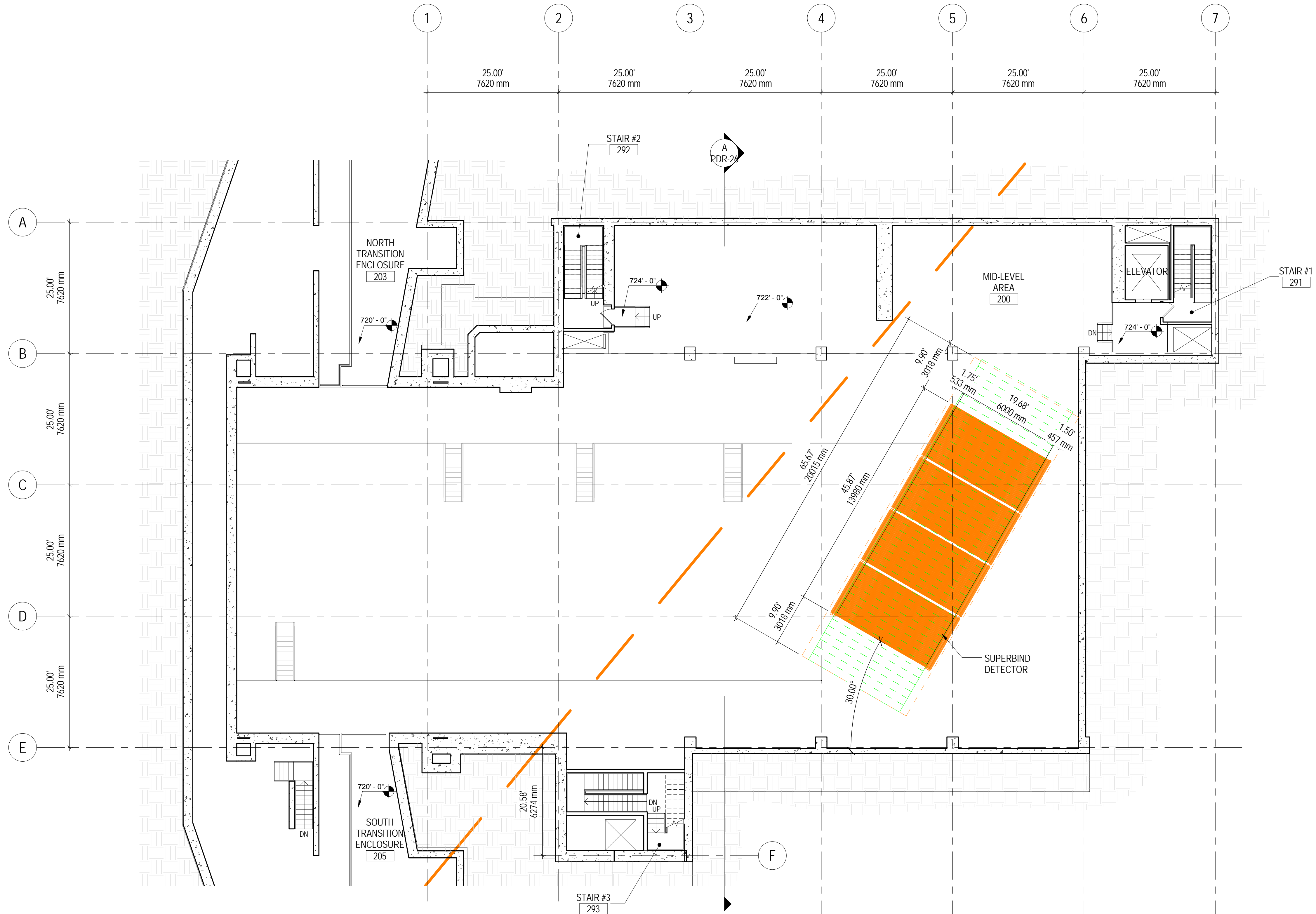
08 MAY 2013

PROJECT NO.

6-13-1

DRAWING NO.

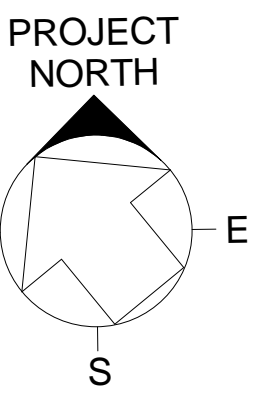
PDR-24



FLOOR PLAN ELEV. 722.00'

SCALE: 3/32" = 1'-0"

SCALE:



FAR DETECTOR FLOOR PLAN



DATE

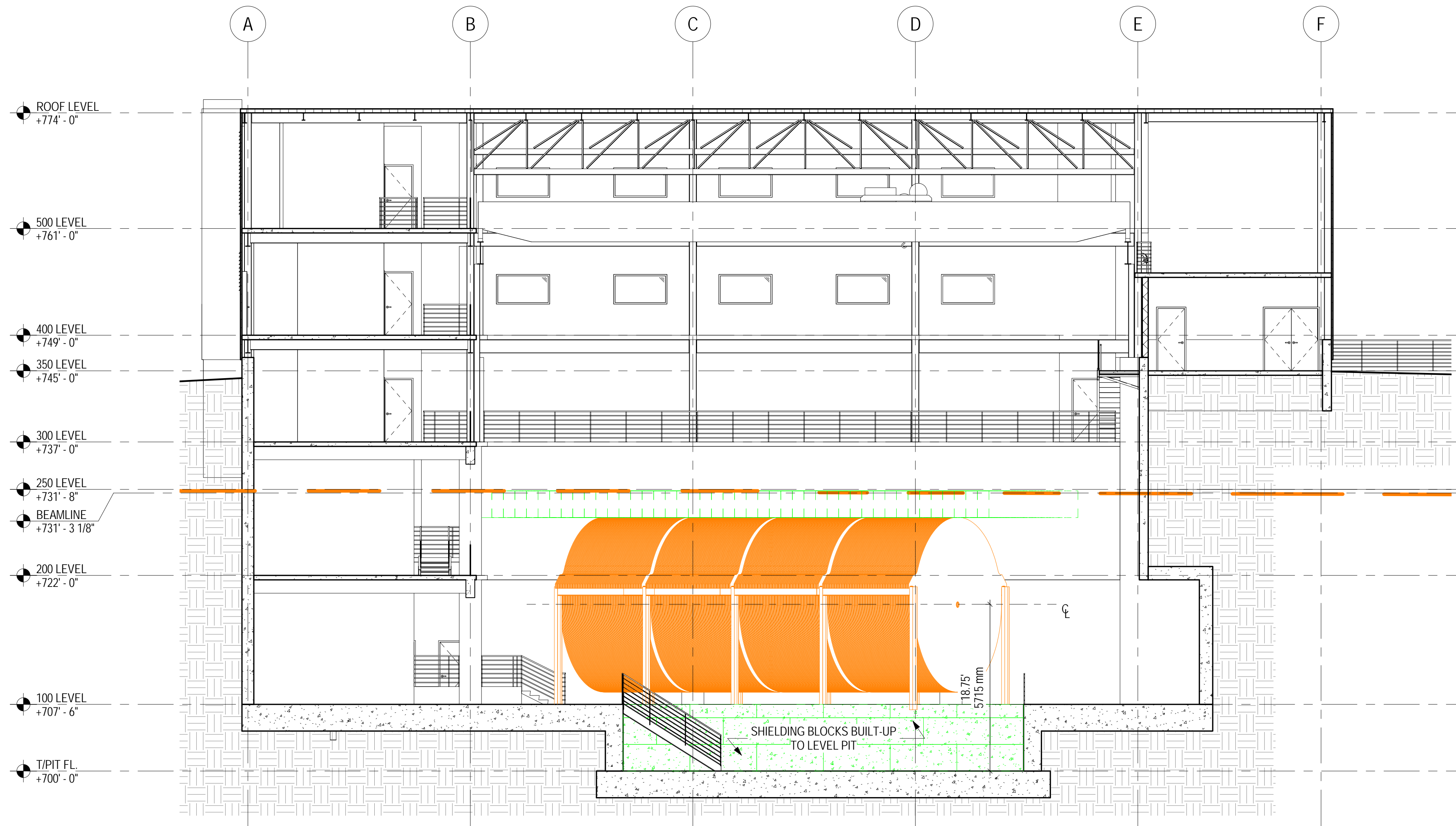
08 MAY 2013

PROJECT NO.

6-13-1

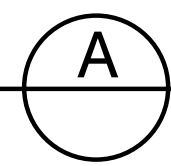
DRAWING NO.

PDR-25

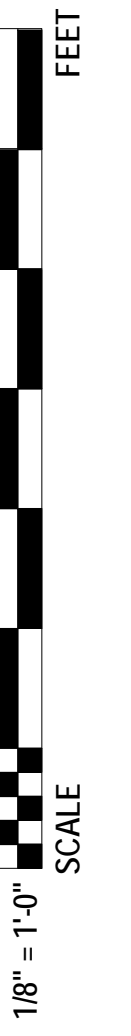


TRANSVERSE SECTION

SCALE: 1/8" = 1'-0"



SCALE:



BUILDING SECTION



DATE

08 MAY 2013

PROJECT NO.

6-13-1

DRAWING NO.

PDR-26



nuSTORM Costing Documentation

nuSTORM Costing

Overview

Detailed costing of the nuSTORM conventional facilities has been done by the Fermilab Facilities Engineering Services Section (FESS) and is reported on in the nuSTORM Project Definition Report (PDR) 6-13-1. Estimates for outfitting the primary proton beam line, the target station, the pion capture/transport line and decay ring are based on either experience from existing Fermilab infrastructure (NuMI) or is based on the detailed costing exercises for DOE CD-1 approval for future experiments (mu2e and LBNE). The detector costing utilized the Euronu costing for the Neutrino Factory Magnetized Iron Neutrino Detector (MIND), extrapolations from MINOS as-built costs and from recent vendor quotes. Costs included all manpower and are fully burdened (FY2013 dollars). The costs are not escalated, however, beyond the 5-year project timeline, since a project start for nuSTORM is unknown. Escalation can be estimated from various models (see Figure 1). LBNE has used the Jacob's model to determine their cost escalation [1].

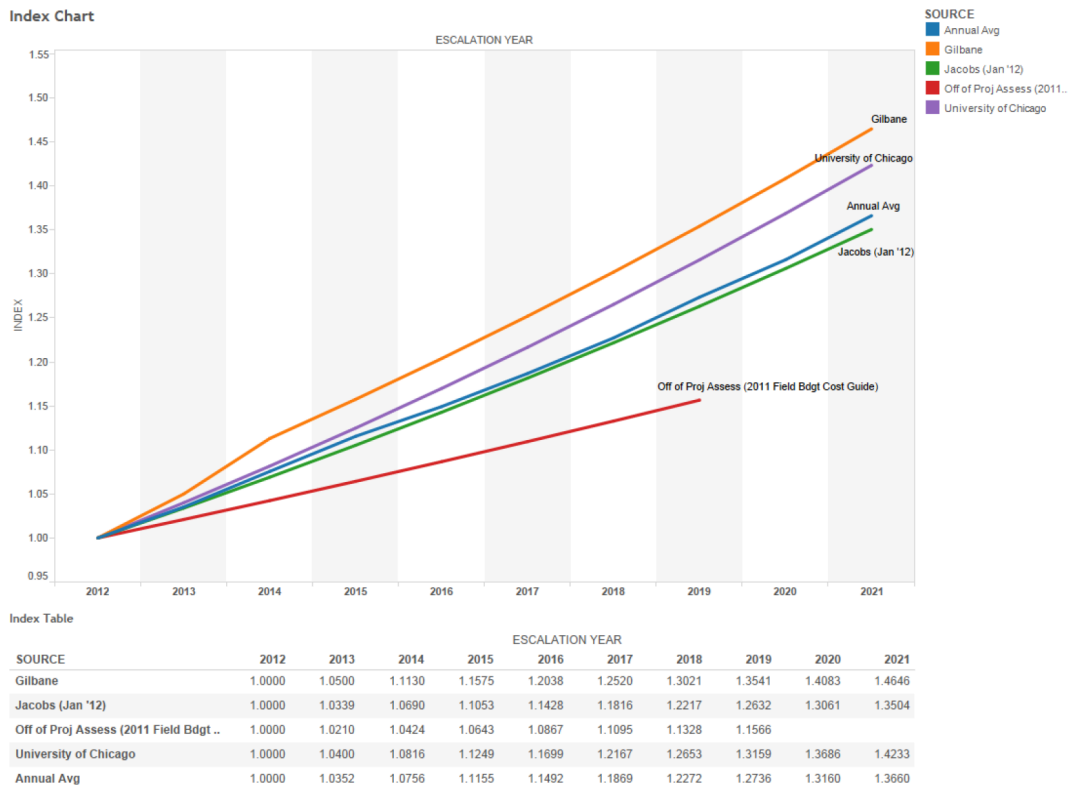


Figure 1. Cumulative Effect of Predictive Escalation Rate Models

The cost breakdown for nuSTORM is given in Table 1 and the overall costing details are given in Appendix 1.

Table 1. nuSTORM cost breakdown

Subsystem	Base cost	Contingency	Cost
Proton beam line	21,143,940	7,356,253	28,500,193
Target Station	26,674,694	11,225,150	37,899,844
Capture/transport	10,811,010	5,681,943	16,492,953
Decay ring	89,248,924	45,956,474	135,205,398
Near detector hall	16,778,572	6,711,429	23,490,001
Far detector hall	1,182,581	650,420	1,833,001
SuperBIND	21,057,070	4,190,528	25,247,598
Site work	17,429,678	9,586,323	27,526,000
CF other	1,804,286	721,714	2,526,000
TOTAL	206,130,755	92,080,233	298,210,988
Management			37,080,186
TPC		45% contingency	335,291,175

Cost Breakdown

The conventional facilities costs are detailed in the PDR and include construction, EDIA (Engineering, Design, Inspection and Administration/Management), contingency and indirect costs. The TPC has been estimated in FY13 dollars. The Indirect Costs are associated with laboratory rates, dated October 2012.

Costing for outfitting the various sub-systems is supported by estimates provided by:

1. Michael Geelhoed Primary beam line/transport line Appendix 2
2. Kris Anderson Target Station Appendix 3
3. T.J. Gardner Quadrupole magnets Appendix 4
4. Paul Soler MIND costing (Euronu) Appendix 5

In addition, cost estimates for the superconducting dipoles in the transport line and decay ring were provided by Vladimir Kashikhin, based on the Strauss-Green costing model [2]. Appendices 6 and 7 are vendor quotes for detector components (scintillator and wavelength shifting fiber, respectively). Management costs are based on LBNE costing and are 10% for the project office (does not include Top-down contingency), 9.4% for L1 management and 4% for L3 management.

[1] T. Lundin, "LBNE Conventional Facilities (CF) Approach to Cost Escalation", April 25, 2013.

[2] M.A. Green and B. P. Strauss, "The Cost of Superconducting Magnets as a Function of Stored Energy and Design Magnetic Induction Times the Field Volume", IEEE Trans. On Appl. Superconductivity, Vol. **18**, No. 2, June 2008.

Appendix 1 nuSTORM Work Breakdown Structure

WBS	Unit	Number	Cost/unit	Cost	Contingency factor	Contingency	Total	Sub-system cost	BOE
1 Primary beam line									
1.1 Conventional Facilities									
1.1.1 Primary beam		1	10,130,714	10,130,714	1.40	14,183,000	28,500,193	14,183,000	PDR
		1	11,013,226	11,013,226	1.30	14,317,194		14,317,194	AD estimate
				21,143,940		7,356,253			
2 Target Station									
2.1 Conventional Facilities		1	12,890,968	12,890,968	1.55	19,981,000	37,899,844	19,981,000	PDR
2.1.1 Target station outfitting		1	13,783,726	13,783,726	1.30	17,918,844		17,918,844	AD estimate
				26,674,694		11,225,150			
3 Capture and transport									
3.1 Conventional Facilities		1	2,764,375	2,764,375	1.60	4,423,000	16,492,963	4,423,000	PDR
3.1.1 Secondary beam line		1	8,046,635	8,046,635	1.50	12,069,953		12,069,953	AD/TD estimate
				10,811,010		5,681,943			
4 Decay Ring									
4.1 Conventional Facilities		1	36,733,750	36,733,750	1.60	58,774,000	135,206,398	58,774,000	PDR
4.2 RT magnets									
4.2.1 Quad A		40	88,624	3,544,960	1.60	5,671,936		5,671,936	TD estimate
4.2.2 Quad B		50	128,112	6,405,600	1.60	10,248,960		10,248,960	TD estimate
4.2.3 Quad C		28	115,957	3,246,796	1.60	5,194,874		5,194,874	TD estimate
4.2.4 Quad D		6	126,503	759,018	1.60	1,214,429		1,214,429	TD estimate
4.2.5 Quad power supplies		2	100,000	200,000	1.40	280,000		280,000	TD estimate
4.3 SC magnets (dipoles)		16	1,668,750	26,700,000	1.35	36,045,000		36,045,000	TD estimate
4.3.1 SC magnet power supplies		2	50,000	100,000	1.40	140,000		140,000	TD estimate
4.4 Beam pipe		480	6,560	3,148,800	1.50	4,723,200		4,723,200	TD estimate
4.5 Cryo-plant		1	2,600,000	2,600,000	1.50	3,900,000		3,900,000	TD estimate
4.6 Installation		1	945,000	945,000	1.50	1,417,500		1,417,500	TD estimate
4.7 Cabling		1	1,080,000	1,080,000	1.50	1,620,000		1,620,000	TD estimate
4.8 Water		1	1,275,000	1,275,000	1.50	1,912,500		1,912,500	TD estimate
4.9 Controls		1	510,000	510,000	1.30	663,000		663,000	TD estimate
4.1 Instrumentation		1	2,000,000	2,000,000	1.70	3,400,000		3,400,000	TD estimate
				89,248,924		45,956,474			
5 Near Detector Hall									
5.1 Conventional Facilities		1	16,778,572	16,778,572	1.40	23,490,001	23,490,001	23,490,001	PDR
6 Far Detector Hall									
6.1 Conventional Facilities		1	1,182,581	1,182,581	1.55	1,833,001	1,833,001	1,833,001	PDR
				1,182,581		650,420			
7 Far & Near Detectors									
7.1 Steel									
7.1.1 Detector plane prototypes		1	500,000	500,000	1.30	650,000		650,000	Euroou costing document
7.1.2 Steel procurement	ton	1500	850	1,275,000	1.25	1,593,750		1,593,750	Euroou costing document
7.1.3 Steel plate assembly	ton	1500	510	765,000	1.25	956,250		956,250	Euroou costing document
7.1.4 Steel transport	ton	1500	40	60,000	1.25	75,000		75,000	Euroou costing document
7.1.5 Steel support structures and handling fixtures	ton	1500	225	337,500	1.25	421,875		421,875	Euroou costing document
7.2 Scintillator									
7.2.1 Scintillator strips	ton	190	15,343	2,915,170	1.25	3,643,963		3,643,963	Vendor quote
7.2.2 WLS fibre	m	1,370,000	1,44	1,972,800	1.20	2,367,360		2,367,360	Vendor quote
7.2.3 Scintillator modules	planes	880	2,500	2,200,000	1.30	2,860,000		2,860,000	MINOS extrapolation
7.3 Electronics, DAQ and database									
7.3.1 SPM		264,000	10	2,640,000	1.25	3,300,000		3,300,000	32ch readout ASIC- NOVA chip derivative
7.3.2 Front end electronics		1	1,720,000	1,720,000	1.50	2,580,000		2,580,000	
7.3.2.1 ASIC/FEE development		1	1,000,000	1,000,000					
7.3.2.2 Production and testing		12000	30	360,000					
7.3.2.3 Interface		3000	120	360,000					
7.3.3 Readout Infrastructure					1.30	3,250,000		3,250,000	
7.3.3.1 L1 concentrator development		1	500,000	500,000					
7.3.3.2 L1 concentrator production		1000	1,500	1,500,000					
7.3.3.3 L2 concentrator development		1	300,000	300,000					
7.3.3.4 L2 concentrator production		80	2,500	200,000					
7.3.4 Data acquisition and triggering									
7.3.4.1 Online computer cluster		12	5,000	60,000					
7.3.4.2 Clock distribution and machine interface		1	30,000	30,000					
7.3.5 Software		1	50,000	50,000	1.50	75,000		75,000	
7.3.6 Integrations		1	250,000	250,000	1.50	375,000		375,000	
7.3.7 Superconductors		1	250,000	250,000	1.30	325,000		325,000	
7.3.8 Electronics management		1	300,000	300,000	1.30	390,000		390,000	
7.4 Magnet									
7.4.1 Engineering, design		1	280,000	280,000	1.50	420,000		420,000	TD estimate
7.4.2 STL fabrication		1	680,000	680,000	1.50	1,020,000		1,020,000	TD estimate
7.4.3 Superconductor		480	45	21,600	1.50	32,400		32,400	TD estimate
7.4.5 Power supplies		2	40,000	80,000	1.50	120,000		120,000	TD estimate
				21,057,070		41,905,528			

Appendix 3

nuSTORM Target Station Cost Estimate										
23-May-13										
M&S Escalated (x1.3) Per Alan Gross										
Item	qty	qty (ft^3)	qty. (lbs)	units	Cost per unit	M&S (unesc)	M&S Escalated (x1.3)	SWF hrs.	SWF \$ With Overhead	Comments
Target Station Engineering Management & Integration										
Mechanical Engineer								2080		Assume 25% effort over 4 year time period
Electrical Engineer for Control and Electronics								2080		Place Holder; Maybe 33% Over 3 year time period- might be light here
Designer / Drafter								416		Assume 5% effort over 4 year period (Providing images for meetings and reviews)
Sub Total Hours TS WBS Management (base hours)								4576		
Target Station Shield Pile										
Mechanical Engineer								2496		Assume 40% of FTE over 3 years- Includes general TS layout and integration
Designer / Drafter								3744		Assume 60% of FTE over 3 years
Technician Time for Installation Activities								5600		4 man technician crew 35 weeks- to cover installation tasks
Installation of Shield Pile						\$ 400,000	\$ 520,000			4 months, 80 days @ \$5k/day-WAG
Chase Cover Poly	571	ft^3			\$ 288.72	\$ 164,859.12	\$ 214,317			Used to mitigate neutron sky shine per LBNE
Chase Cover Steel	1712.2	ft^3	832129.2		\$ 2.13	\$ 1,772,435.20	\$ 2,304,166			Finished steel for air-tight fit
Target and Horn T-Blocks	578	ft^3	280908	lbs.	\$ 1.71	\$ 480,352.68	\$ 624,458			Rough Fabrication CCSS
Filler Steel	153	ft^3	74358	lbs.	\$ 2.13	\$ 158,382.54	\$ 205,897			A36-Finished
Quad T-blocks	150	ft^3	72900	lbs.	\$ 1.71	\$ 124,659.00	\$ 162,057			Rough Fabrication CCSS
Quad 1 Collimator	90	ft^3	43740	lbs.	\$ 2.13	\$ 93,166.20	\$ 121,116			A36
Quad 2 Collimator	104	ft^3	50544	lbs.	\$ 2.13	\$ 107,658.72	\$ 139,956			A36
Duratek Blocks	140			ea	\$ 300.00	\$ 42,000.00	\$ 54,600			
R-Blocks	32	3328		ft^3	\$ 22.60	\$ 75,212.80	\$ 97,777			
Shielding Subtotal Man-hours								11840		
Shielding M&S (Base)						\$ 3,418,726.26				
Shielding M&S (Burdened)						\$ 4,444,344.13				
Modules										
Mechanical Engineer								3120		Assume 75% of FTE over 2 year- Redesign current modules for 0 beamline pitch
Designer / Drafter								3120		Assume 75% of FTE over 2 years
Technician Time for Module Fabrication								6240		3 technicians for 1 year
Module Assembly Stands	4			ea	\$ 20,000	\$ 80,000	\$ 104,000.0			
Target	1				\$ 400,000	\$ 400,000	\$ 520,000			

Horn	1				\$	400,000	\$	400,000	\$	520,000										
Stripline Block	1				\$	200,000	\$	200,000	\$	260,000										
Quad 1 Module	1				\$	250,000	\$	250,000	\$	325,000										
Quad 2 Module	1				\$	250,000	\$	250,000	\$	325,000										
Module and Block Handling Fixtures					\$		\$	50,000	\$	65,000										
Carriage Beams	3			ea	\$	70,000	\$	210,000	\$	273,000									Qty. 3- Target, Horn, Quads	
Module Subtotal Man-hours											12480									
Module M&S (Base)																				
Module M&S (Burdened)																				
Item	qty	qty (ft^3)	qty. (lbs)	units	Cost per unit	M&S (unesc)	M&S Escalated (x1.3)	SWF hrs.	SWF \$ With Overhead	Comments										
Target Station Beamline Devices and Support Systems																				
Mechanical Engineer Designer / Drafter								3120		General Engineering for Devices: Assume 50% of FTE over 3 years- Includes integration of beamline devices										
Technician Time for General Assembly Issues not covered specifically in devices (e.g., horns, targets)								3744		Assume 60% of FTE over 3 years										
Horn	1				\$500,000	\$500,000	\$650,000		\$	300,000	NuMI Documented Costs- includes technician assembly time and fabrication oversight Estimate from Ken Bourkland for LBNE- Includes fully burdened SWF and M&S									
Horn Power Supply	1				\$	1,700,000	\$2,210,000													
Stripline	50			ft	\$	1,300	\$84,500												2 FTE technicians for 1 year	
Target	1				\$300,000	\$300,000	\$390,000		\$	100,000	NuMI Documented Costs- includes technician assembly time and fabrication oversight									
Quads	2				\$1,500,000	\$3,000,000	\$3,900,000													
Quad Power Supply	2				\$	100,000	\$260,000												Cost from FRIB	
Cryo					\$	100,000	\$130,000												A guess- needs to include cabling, etc.	
RAW Skid	5				\$50,000	\$250,000	\$325,000												Guess- Piping from Cryo feed	
Mechanical Engineer for RAW Skid Layout								1040											Qty 5 RAW skids- Target, Horn, Each Quad, Collimators; Rough numbers from Karl Williams	
TP Air Fan and Chiller					\$	250,000	\$325,000												Per Karl Williams	
Munters Dehumidifier					\$	125,000	\$162,500												Need number from Lee Hammond; guess at system cost plus installation	
Neutralization Systems and Evaporator					\$	75,000	\$97,500												From NuMI, Large Munters at \$80k in FY2008; Add \$45k to cover escalation and installation	
Train Cart					\$	40,000	\$52,000												From NuMI, System cost ~\$25k in FY2007 dollars, add \$25k for installation	
Cameras					\$	20,000	\$26,000													
Workcell					\$	500,000	\$650,000													
Morgue Doors and Hardware Placeholder					\$	200,000	\$260,000												Placeholder for pull-up morgue doors similar to C0	

Beamline Devices Subtotal Man-hours				6864	
Beamline Devices M&S (Base)					
Module M&S (Burdened)				\$ 7,325,000	\$ 9,522,500
Cost Summary					
	Man Hours	Man-Years	Cost per Man-Year (Estimate of Burdened Cost per Man-Year)	Total SWF (Burdened)	
Man-Hour Rollup Technician Drafting Category	27024	12.99	\$ 250,000	\$ 3,248,077	
Man-Hour Rollup Engineering Category	13936	6.7	\$ 325,000	\$ 2,177,500	
SWF \$ Burdened for Target and Horn Assy.				\$ 400,000	
Un-Escalated M&S				\$ 12,583,726.26	
Cost Rollup TPC Escalated M&S plus Burdened Labor = (Excluding Contingency)				\$ 18,409,303	

Appendix 4

nuSTORM Racetrack Conventional Quadrupoles

Price stated for each unit		Conventional hollow square copper with fiberglass/epoxy insulation in a potted (multi-pancake) mass.										Total \$				
Aperature	I +/-	Fe L	Turns	Cu lin ft	\$/ft	Fe in 3	Fe raw #	Fe \$	Mach	Addl parts	I tech hrs	Tech SWF\$	EDIA 0.9 T \$	T \$ M&S	I \$ Labor	Total \$
A	0.3m R	2	28	700	\$ 4,200	8000	2267	\$ 1,813	\$ 14,506.50	\$ 7,000	804	\$ 32,160	\$ 28,944	\$ 27,520	\$ 61,104	\$ 88,624
B	0.3m R	7.8 max	42	900	\$ 5,400	14400	4080	\$ 3,264	\$ 26,111.69	\$ 7,000	1,136	\$ 45,440	\$ 40,896	\$ 41,776	\$ 86,336	\$ 128,112
C	0.3m R	11 max	32	1100	\$ 6,600	26000	7367	\$ 5,893	\$ 35,359.58	\$ 7,000	804	\$ 32,160	\$ 28,944	\$ 54,853	\$ 61,104	\$ 115,957
D	0.5m R	5	32	1800	\$ 10,800	30000	8500	\$ 6,800	\$ 40,799.52	\$ 7,000	804	\$ 32,160	\$ 28,944	\$ 65,399	\$ 61,104	\$ 126,503
Technician labor breakout																
Pancake hrs	Qty techs	Hrs/pancake	# pancake	Wind hrs	Mag assy hrs	Qty techs	Assy hrs	Final hrs	Qty techs	Final hrs	I tech hrs	Techs	Pancake op	Hours	T hours	
A	83	-	8	664	40	2.5	100	40	1	40	804	2.5	Winding hrs	10	25	
B	83	-	12	996	40	2.5	100	40	1	40	1136	1	Insulation	10	10	
C	83	-	8	664	40	2.5	100	40	1	40	804	2	Impregnate	20	40	
D	83	-	8	664	40	2.5	100	40	1	40	804	1	Clean-up	8	8	
E*	40	2.5	8	800	80	2.5	200	40	1	40	1040				83	
A pancake coil is (2) layers * either (7) or (8) turns, thus either (14) or (16) turns per pancake.																
Tech SWF is estimated at \$40/hr. Fully loaded value is ~ double.																
* High radiation quad assumes hollow square conductor is mineral insulated inside of an outer metal jacket estimated at \$35/linear foot.																
Aperature	I +/-	Fe L	Turns	Cu lin ft	\$/ft	Fe in 3	Fe raw #	Fe \$	Mach	Addl parts	I tech hrs	Tech SWF\$	EDIA 1.4 T \$	T \$ M&S	I \$ Labor	Total \$
E*	10cm R	1.67	28	1100	\$ 38,500	6000	1700	\$ 1,360	\$ 12,239.86	\$ 10,000	1,040	\$ 41,600	\$ 58,240	\$ 62,100	\$ 99,840	\$ 161,940
Engineering, Design, Inspection and Administration is historically 90%-140% of tech dollar value (varies by project complexity)																
EDIA SWF breakout																
Scientist			2%													
M Engineer			23%													
Drafter			25%													
Proc Eng M			20%													
Proc Eng W			20%													
Support/Supervision			10%													
Blue font is calculated field																

Appendix 5

Euronu Magnetized Iron Neutrino Detector Costing (MIND)

WBS	Description	Unit	Number	Cost/unit (€)	Material Cost (€)	Duration (months)	FTE	FTE months	Comments	Total cost (€)
2.2.	Intermediate baseline detector (MIND 100 kton)									
2.2.1.	Detector R&D									
2.2.1.1.	Scintillator R&D	units	1	300000	300000		24	2	48 Develop scintillator geometry and co-extrusion	1276000
2.2.1.2.	STL R&D	units	1	200000	200000		24	1	24 Develop STL prototype	216000
2.2.1.3.	Photon detector and electronics R&D	units	1	200000	200000		24	1	24 Testing and characterisation SiPMs	189218040
2.2.2.	Underground cavern									
2.2.2.1.	Geomechanical studies	volume(m3)	60000	1185	71100000		12	3	0 Scaled from 13174 m2 of MINOS cavern	150857700
2.2.2.2.	Cavern construction	length (m)	150		36000000		31		0 Double of MINOS (since double length)	29899650
2.2.2.3.	Cavern outfitting				0		0		0	72000
2.2.3.	Steel plate fabrication									
2.2.3.1.	Engineering, design				0		24	3	72	2232000
2.2.3.2.	Steel management	tonne	188	1750	329000		60	3	180	1296000
2.2.3.3.	Detector plane prototypes	tonne	105268	1000	105268000		60	60	0 Prototype with 5 planes	2232000
2.2.3.4.	Steel procurement	tonne	105268	1000	105268000		60	60	0 €774 per tonne constructed in MINOS	150857700
2.2.3.5.	Steel plate assembly	tonne	105268	600	63160800		60	60	0 60% of steel cost in fabricatin in MINOS	29899650
2.2.3.6.	Steel transport	tonne	105268	30	3158040		60	60	0 3% of steel cost in transport	1296000
2.2.3.7.	Steel support structures and handling fixtures	tonne	105268	150	15790200		60	60	0 15% of steel costs in handling in MINOS	720000
2.2.4.	Magnet coil									
2.2.4.1.	Engineering, design	length (m)	400	500	200000		12	1	0 Price from STL prototype for VLHC	1512000
2.2.4.2.	STL fabrication	Plants	1	500000	500000		0		0 1 cryo plant	488569390
2.2.4.3.	STL cryo plant	HV supplies	10	20000	200000		0		0 10 power supplies of 10 kA	1276000
2.2.4.4.	Power supplies				0		0		0	107316000
2.2.5.	Scintillator detector fabrication									
2.2.5.1.	Engineering, design	tonne	9209	6000	55254000		24	3	72	576000
2.2.5.2.	Scintillator strips	length (km)	25058	1000	25058000		60	60	0 \$10/kg extruded scintillator in MINOS (could be as low as \$6-7/kg)	1276000
2.2.5.3.	WLS fibre	tonne	9209	600	5525400		60	60	0 Kuraray \$1/m WLS fibre	216000
2.2.5.4.	Scintillator modules	units	4412800	10	44128000		60	60	0 Assembly around 10% cost material (MINOS)	189218040
2.2.5.5.	Photon detectors (SiPMs)	units	68950	50	3447500		60	60	0 Projection of cost of €10 per SiPM	972000
2.2.5.6.	Multiplexing boxes and connectors	units	4412800	1	4412800		60	60	0 Estimate of cost of mechanical box	2232000
2.2.5.7.	Calibration systems	units	4	1200000	4800000		60	4	0 Similar price to MINOS	1296000
2.2.5.8.	Assembly and test equipment	units	4	1500000	6000000		60	4	0 Similar price to MINOS	29899650
2.2.5.9.	Factories	units	4	1500000	6000000		60	4	0 Similar price to MINOS	720000
2.2.5.10.	Scintillator management				0		60	5	300	1512000
2.2.6.	Electronics, DAQ and database									
2.2.6.1.	Front end electronics	units	4412800	5	22064000		60	60	0 Estimate of price per channel	1276000
2.2.6.2.	Data routing and trigger farm	units	4412800	1	4412800		30	0	0 In MINOS 20% of front-end electronics	216000
2.2.6.3.	Data acquisition and triggering	units	1	250000	250000		24	3	72 Same cost as MINOS (Moore's law helps)	189218040
2.2.6.4.	Database				0		24	1	24	972000
2.2.6.5.	Auxiliary systems	units	1	620000	620000		60	60	0 Same as MINOS	2232000
2.2.6.6.	Slow controls and monitoring	units	1	1050000	1050000		60	60	0 Same as MINOS	150857700
2.2.6.7.	High Voltage systems	units	68950	3	206850		60	60	0 Similar to MINOS	29899650
2.2.6.8.	Electronics management				0		60	2	120	720000
2.2.7.	Detector installation									
2.2.7.1.	Management				0		60	2	120	1512000
2.2.7.2.	Lab infrastructure	units	1	1350000	1350000		60	2	0 Double of MINOS (since double length)	488569390
2.2.7.3.	Plane assembly area	units	1	774000	774000		0		0 Double of MINOS (since double length)	216000
2.2.7.4.	Installation	units	1	4356000	4356000		0		0 Double of MINOS (since double length)	189218040
2.2.7.5.	Alignment and survey	units	1	318000	318000		84	3	252	2232000
2.2.8.	Project management									
					480433390				1356	1296000
Total					480433390				1356	8136000
2.2.	Intermediate baseline detector (MIND 100 kton)									
2.2.1.	Detector R&D									
2.2.1.1.	Underground cavern	Total Cost (%)	0.3		700000		0.7	96	Manpower cost per month (€6000)	576000
2.2.1.2.	Steel plate fabrication	Material (%)	22.3	0.1	107100000		107.1	36	FTE months	216000
2.2.1.3.	Magnet coil	Material cost (€)	38.7	22.3	187706040		187.70604	252	Material cost (M€)	1512000
2.2.1.4.	Scintillator detector fabrication	Material cost (M€)	0.2	39.1	900000		0.9	12	Manpower cost per month (€6000)	72000
2.2.1.5.	Electronics, DAQ and database	Material (%)	30.9	30.9	148625700		148.6257	372	FTE months	2232000
2.2.1.6.	Detector installation	Material cost (€)	6.1	6.0	28603650		28.60365	216	Material cost (M€)	1296000
2.2.1.7.	Project management	Material cost (M€)	1.5	1.4	6796000		6.796	252	Manpower cost per month (€6000)	720000
2.2.1.8.		Material (%)	0.3	0.0	0		0	252	FTE months	1512000
Total		Total Cost (%)	100	100.0	480433390		480.43339	1356	Manpower cost per month (€6000)	8136000

Appendix 6

EXTRUDED SCINTILLATOR FOR vSTORM

Requested by Alan Bross
 Prepared by Anna Pla-Dalmau
 Date: May 17, 2013

IMPORTANT: PROJECT WILL BE BILLED AT ACTUAL COSTS. THIS IS AN ESTIMATE.

Rectangular scintillator bars: 20 mm x 7.5 mm with 1 hole
 With white reflective coating (15% TiO2 in polystyrene)
 Total amount for detector: 190,000 kg

	Estimated Materials and Services Cost (\$)	Estimated Time (hours)	Rate (hours)	Estimated Labor Effort (\$)	Total Estimated Cost Materials and Labor (\$)
Material - tuning and production					
Die and sizing tooling* - 2 sets	\$30,000.00				
Polystyrene pellets* (222,000 Kg @ \$2.80 each)	\$616,000.00				
Dopants** (5,110 bottles @ \$175 each)	\$894,250.00				
Titanium dioxide pellets** (5,550 Kg @ \$7.50 each)	\$41,625.00				
Nitrogen gas (1 year supply)	\$15,000.00				
Consumables (1 year supply)	\$10,000.00				
Labor - tuning and production***					
Extrusion preparation and operation (2FTE)		6,000	\$60.00	\$360,000.00	
Extrusion QC (2FTE) - contract?		6,000	\$35.00	\$210,000.00	
Shipping					
Crates					
Extrusion equipment maintenance	\$10,000.00				
					\$2,186,875.00
Estimated Direct Cost	\$1,616,875.00			\$570,000.00	\$318,039.31
FNAL Indirect Charges (19.67% M&S)	\$318,039.31			\$410,286.00	\$410,286.00
FNAL Indirect Charges (71.98% Labor)				\$980,286.00	\$2,915,200.31
TOTAL Estimated Cost	\$1,934,914.31				

*Current price

**Estimated, adjusted price for large quantity

***Estimated 125 kg / h production - 1 line, 1 shift

Appendix 7



KURARAY AMERICA, INC.
2625 Bay Area Blvd., Suite 600
Houston, TX 77059
Phone: 281-283-1739 Fax: 281-283-1722

TO: Alan Bross
Fermi Lab
bross@fnal.gov
(630) 840-4880 (Office)

Date 4/25/2013
Quotation # FNAL-042513

QUOTATION (Valid for 30 Days)

Product Description	Quantity (M)	U Price	Total
Y-11(150)MS, 0.7mmD., BJ	3,100,000	\$1.44	\$4,464,000.00
Total			

Delivery Schedule TBA

Terms FCA Japan. (Air freight, insurance, tax and all other forwarding charges will be borne by BUYER after you receive your order)

Other Remarks:

Thank you very much for your interest in our products. If you have any question, please do not hesitate to contact me.

Best Regards,

Hui Yao

Hui Yao