

Ph 205 FINAL EXAM SOLUTIONS

1989-90

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① CENTRAL FORCE $\vec{F} = -\frac{\alpha}{r^2} e^{-\beta r} \hat{r}$

THIS CAN IN PRINCIPLE BE DERIVED FROM A POTENTIAL $V(r) = -\int_{\infty}^r \vec{F} \cdot d\vec{r} = \alpha \int_{\infty}^r \frac{e^{-\beta r}}{r^2} dr$

THE KEY IS THAT WE DO NOT ACTUALLY HAVE TO DO THE INTEGRAL!

THE ENERGY, IN POLAR COORDINATES IS $E = \frac{1}{2} m \dot{r}^2 + \frac{1}{2} m r^2 \dot{\theta}^2 + V(r) = \text{CONST}$

ANGULAR MOMENTUM IS ALSO CONSERVED: $L = m r^2 \dot{\theta} = \text{CONST}$

$$\therefore E = \underbrace{\frac{1}{2} m \dot{r}^2}_{T_{\text{eff}}} + \underbrace{\frac{L^2}{2mr^2}}_{V_{\text{eff}}} + V(r)$$

THE CONDITION FOR AN EQUILIBRIUM CIRCULAR ORBIT IS $V'_{\text{eff}}(r_0) = 0$

THE CONDITION FOR STABILITY OF SMALL OSCILLATIONS IS $V''_{\text{eff}}(r_0) > 0$

$$V'_{\text{eff}} = -\frac{L^2}{m r^3} + \frac{\alpha}{r^2} e^{-\beta r}$$

$$V''_{\text{eff}} = \frac{3L^2}{m r^4} - \frac{2\alpha}{r^3} e^{-\beta r} - \frac{\alpha\beta e^{-\beta r}}{r^2}$$

$$V'_{\text{eff}}(r_0) = 0 \Rightarrow \frac{L^2}{m r_0} = \alpha e^{-\beta r_0}$$

THE EQUILIBRIUM ANGULAR VELOCITY Ω SATISFIES $L = m r_0^2 \Omega$

SO $m \Omega^2 r_0 = \frac{\alpha e^{-\beta r_0}}{r_0^2}$ (WHICH ALSO FOLLOWS FROM $F=ma$ AT ONCE)

$$V''_{\text{eff}}(r_0) = 3m\Omega^2 - m\Omega^2 r_0 \left(\frac{2}{r_0} + \beta \right) = m\Omega^2 (1 - r_0 \beta)$$

$$\omega^2_{\text{osc}} = \frac{V''_{\text{eff}}(r_0)}{m} = \Omega^2 (1 - r_0 \beta) \Rightarrow \omega = \Omega \sqrt{1 - r_0 \beta}$$

CLEARLY FOR STABILITY WE MUST HAVE

$$r_0 < \frac{1}{\beta}$$

THIS CONTRASTS WITH THE GRAVITATIONAL FORCE, FOR WHICH STABLE ORBITS CAN HAVE ARBITRARILY LARGE r_0 .

THE NUCLEAR FORCE IS 'SHORT RANGE.'

2) STABILITY OF A 'DUMBBELL' SATELLITE

A GOOD FIRST STEP IS TO DEDUCE THE EQUILIBRIUM ORIENTATION:



THIS IS UNSTABLE; IF ONE MASS ROTATES SLIGHTLY TOWARDS THE EARTH THE PULL OF GRAVITY ON IT INCREASES AND AMPLIFIES THE PERTURBATION



THIS IS STABLE: IF THE BAR ROTATES THE ATTRACTION ON THE MASS CLOSER TO EARTH PROVIDES A GREATER RESTORING TORQUE THAN THE DESTABILIZING TORQUE OF THE FAR MASS.

SO CONSIDER IS CASE LIKE



WE PRESENT TWO SOLUTIONS

METHOD A: CONSIDER THE SYSTEM IN A ROTATING FRAME WITH THE C.M. AT REST.

THEN WE MUST CONSIDER THE TORQUE EQUATION $I \ddot{\theta} = \sum \text{TORQUE}$

HERE $I = 2ml^2$

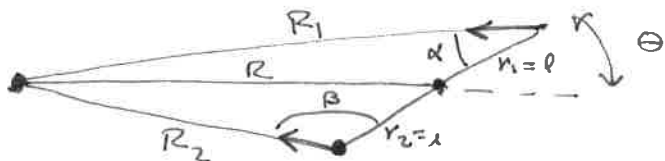
NOW $\sum \text{TORQUE} = \sum_{i=1,2} \vec{r}_i \times \vec{F}_i$

UNKNOWN CONSTRAINT FORCE!! ↓

AND $\vec{F}_i = \vec{F}_{i, \text{GRAVITY}} = m \ddot{\vec{R}} - m \vec{\omega}_0 \times (\vec{\omega}_0 \times \vec{r}_i) - 2m \vec{\omega}_0 \times \vec{v}_i + \vec{F}_{i, \text{ROD}}$

\uparrow C.M. MOTION \uparrow CENTRIFUGAL FORCE, ALONG \vec{r}_i \uparrow CORIOLIS FORCE, ALONG \vec{v}_i

NOTE THAT $\vec{r}_1 = -\vec{r}_2$ ISO $\sum \vec{r}_i \times m \ddot{\vec{R}} = 0$. IF WE IGNORE $\sum \vec{r}_i \times \vec{F}_{i, \text{ROD}}$, ONLY GRAVITY PRODUCES A TORQUE IN THE ROTATING FRAME!



LAW OF COSINES:

$$R_{1,2}^2 = R^2 + l^2 \pm 2Rl \cos \theta$$

BY LAW OF SINES:

$$\frac{\sin \alpha}{R} = \frac{\sin \theta}{R_1}$$

$$\frac{\sin \beta}{R} = \frac{\sin \theta}{R_2}$$

$\sum \text{TORQUE, GRAVITY} \approx r_1 \sin \alpha \cdot \frac{GMm}{R_1^2} - r_2 \sin \beta \cdot \frac{GMm}{R_2^2}$

$= -GMm l \sin \theta \left(\frac{R}{R_2^3} - \frac{R}{R_1^3} \right)$

$\approx -GMm l \sin \theta \left[1 - \frac{3}{2} \left(\frac{r^2}{R^2} - 2r/R \cos \theta \right) + \dots - 1 - \frac{3}{2} \left(\frac{l^2}{R^2} + 2l/R \cos \theta \right) + \dots \right]$

$\approx -6 \frac{GMm l^2 \sin \theta}{R^2}$

Ph 205 FINAL EXAM SOLUTIONS

NEAR EQUILIBRIUM, $\dot{\theta} \approx 0$. ALSO, FEMMA FOR THE C.M. ORBIT

TELLS US THAT $m\omega_0^2 R = \frac{GMm}{R^2}$

$$\text{so } \sum \tau \approx -6m\omega_0^2 l^2 \theta = I \ddot{\theta} = 2ml^2 \ddot{\theta}$$

$$\ddot{\theta} = -3\omega_0^2 \theta$$

\Rightarrow FREQUENCY OF θ OSCILLATIONS IS $\omega = \sqrt{3} \omega_0$

METHOD B USE LAGRANGE. HERE WE DON'T NEED TO KNOW $\vec{F}_{i, \text{row}}$!!

$$L = T - V$$

$$T = T_{\text{of c.m.}} + T_{\text{REL to c.m.}}$$

$$= \frac{1}{2} 2m \omega_0^2 R^2 + \frac{1}{2} 2ml^2 (\dot{\theta} + \omega_0)^2$$

MINOR POINT: ANGULAR VELOCITY ABOUT THE C.M. IS $\dot{\theta} + \omega_0$, NOT JUST $\dot{\theta}$ IN AN INERTIAL FRAME

$$V = -GMm \left(\frac{1}{R_1} + \frac{1}{R_2} \right)$$

AS BEFORE $R_{1,2} = R \left(1 + \frac{l^2}{R^2} \pm \frac{2l}{R} \omega_0 \theta \right)^{1/2}$

$$\frac{1}{R_{1,2}} = \frac{1}{R} \left(1 - \frac{1}{2} \left(\frac{l^2}{R^2} \pm \frac{2l}{R} \omega_0 \theta \right) - \frac{1}{8} \left(\frac{l^2}{R^2} \pm \frac{2l}{R} \omega_0 \theta \right)^2 + \dots \right)$$

$$= \frac{1}{R} \left(1 \mp \frac{2l}{R} \omega_0 \theta + \frac{3}{8} \left(\frac{2l}{R} \omega_0 \theta \right)^2 + \dots \right)$$

so $\frac{1}{R_1} + \frac{1}{R_2} \approx \frac{1}{R} \left(2 + 3 \frac{l^2}{R^2} \omega_0^2 \theta^2 + \dots \right)$

$$V \approx - \frac{3GMm l^2 \omega_0^2 \theta^2}{R^3} + \dots$$

$$= -3m\omega_0^2 l^2 \omega_0^2 \theta^2 + \dots \quad \text{USING } m\omega_0^2 R = \frac{GMm}{R^2}$$

$$\approx 3m\omega_0^2 l^2 \theta^2 + \dots \quad \text{IN SMALL ANGLE APPROX}$$

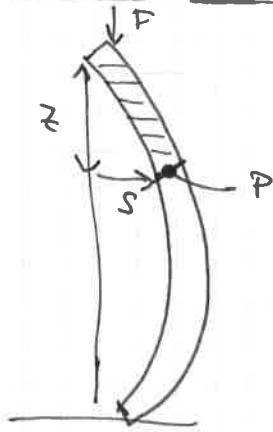
LAGRANGE $\Rightarrow \frac{d}{dt} \frac{\partial L}{\partial \dot{\theta}} = \frac{\partial L}{\partial \theta} \Rightarrow 2ml^2 \ddot{\theta} = -6m\omega_0^2 l^2 \theta$

$$\ddot{\theta} = -3\omega_0^2 \theta$$

AND THE FREQUENCY OF SMALL OSCILLATIONS IS $\omega = \sqrt{3} \omega_0$

WE INFER THAT THE $\vec{F}_{i, \text{row}}$ CAUSE NO RESTORING TORQUE!

③ CHAPLIN'S CANE : ENERGY METHODS ARE CUMBERSOME!! INSTEAD,

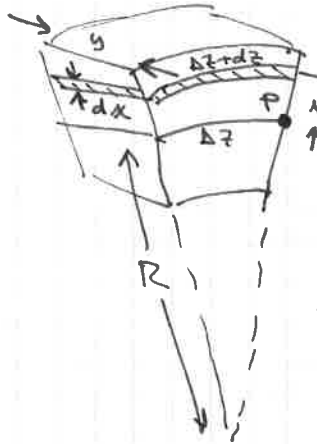


CONSIDER THE SHADED PIECE OF THE BEAM:

$$\sum \text{TORQUES ABOUT } P = 0 = Fs + \Upsilon \quad (1)$$

WHERE Υ IS THE TORQUE TRANSMITTED ACROSS A SLICE THROUGH THE BEAM AT P .

TO GET Υ , CONSIDER A WEDGE Δz LONG



$$\Upsilon = \int x df$$

df FROM YOUNG'S MODULUS:

$$E = \frac{df/A}{dz/\Delta z} \quad \text{WHERE } A = y dx$$

FROM SIMILAR TRIANGLES: $\frac{\Delta z}{R} = \frac{\Delta z + dz}{R + x}$

$$\approx \frac{\Delta z + dz}{R} \left(1 - \frac{x}{R}\right)$$

$$\approx \frac{\Delta z}{R} + \frac{dz}{R} - \frac{x \Delta z}{R^2}$$

SO $dz \approx \frac{x \Delta z}{R}$ AND $\Upsilon = \int x df = \int x y dx E \cdot \frac{x}{R} = \frac{E}{R} \int x^2 dx \cdot y$

$$= \frac{EI}{R}$$

NOW $R = \text{RADIUS OF CURVATURE}$, SO $\frac{1}{R} \approx \frac{d^2 s}{dz^2}$

THEN (1) $\Rightarrow Fs = -EI s'' \Rightarrow s = A \sin \sqrt{\frac{F}{EI}} z$

BUT $\begin{cases} s(0) = 0 \\ s(L) = 0 \end{cases}$ SO MUST HAVE $\sqrt{\frac{F}{EI}} = \frac{n\pi}{L}$

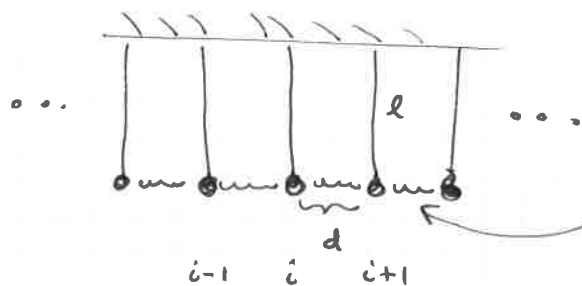
FOR $\sqrt{\frac{F}{EI}} < \frac{\pi}{L}$ CANNOT SATISFY THE 2ND BOUNDARY CONDITION AND THE BEAM DOESN'T BEND!

CLEARLY $F = EI \left(\frac{\pi}{L}\right)^2$ IS THE CRITICAL CONDITION...

[THIS PROBLEM FIRST SOLVED BY L. EULER IN EARLY 1700'S.]

NOTE: $F \sim \frac{EI}{L^2}$ COULD BE DEDUCED FROM DIMENSIONAL ANALYSIS!

④ SLUNG SLINKY (PLEASE REMEMBER TO INCLUDE GRAVITY!)



SPRING OF CONSTANT A , REST LENGTH d
 $S_i \equiv$ HORIZONTAL DISPLACEMENT OF MASS i

FOR MASS i ,
$$M \ddot{S}_i = - \underbrace{m \frac{g}{l} S_i}_{\substack{\uparrow \\ \text{PENDULUM} \\ \text{FORCE}}} + A \underbrace{(S_{i+1} - S_i)}_{\substack{\uparrow \\ \text{FORCE FROM SPRING} \\ \text{TO RIGHT}}} - A \underbrace{(S_i - S_{i-1})}_{\substack{\uparrow \\ \text{FORCE FROM SPRING} \\ \text{TO LEFT}}}$$

TAKE THE CONTINUUM LIMIT, INTRODUCING $\rho = \frac{M}{d}$

$$S' = \frac{S_{i+1} - S_i}{d}$$

$$S'' = \frac{\frac{S_{i+1} - S_i}{d} - \frac{S_i - S_{i-1}}{d}}{d}$$

THEN
$$\rho \ddot{S} = - \frac{\rho g}{l} S + \underbrace{A d}_{\substack{\text{HAS DIMENSIONS OF A FORCE}}}$$

[RECALL $\rho \ddot{S} = T S''$ FOR A STRING]

$$\ddot{S} = - \frac{g}{l} S + \frac{A d}{\rho} S''$$

$$\equiv - \omega_0^2 S + c^2 S'' \quad \text{WITH } \omega_0^2 \equiv \frac{g}{l} \quad c^2 = \frac{A d}{\rho}$$

TRY A WAVE SOLUTION: $S = \cos(kx - \omega t)$

PLUG IN TO WAVE EQUATION TO GET THE DISPERSION EQUATION:

$$\omega^2 = \omega_0^2 + c^2 k^2$$

THE LOWEST FREQUENCY IS FOR LONG WAVES: $k = \frac{2\pi}{\lambda} \rightarrow 0$

$\Rightarrow \underline{\underline{\omega_{\text{MIN}} = \omega_0 = \text{PENDULUM FREQUENCY!}}}$

AT ω_{MIN} , ALL MASSES SWING TOGETHER AS FREE PENDULA,
 THE SPRINGS DO NOT STRETCH OR COMPRESS!

PH 205 FINAL EXAM SOLUTION

WHAT HAPPENS IF DRIVE THE SLINKY WITH $\omega < \omega_{\min}$?

I.E. SUPPOSE $S(0,t) = S_0 \cos \omega t$ $\omega < \omega_{\min}$

TRY FOR A STANDING-WAVE SOLUTION AT FREQUENCY ω

$$S(x,t) = f(x) \cos \omega t$$

PLUG IN:
$$-\omega^2 f = -\omega_0^2 f + c^2 f''$$

$$f'' = \frac{\omega_0^2 - \omega^2}{c^2} f$$

IF $\omega_0 < \omega$ THEN $f \approx \int_0^{\omega_0} \cos \sqrt{\frac{\omega^2 - \omega_0'^2}{c^2}} x$ AND WE HAVE LONG WAVES (THAT CAN BE CONSIDERED AS TRAVELLING WAVES AS WELL)

BUT IF $\omega_0 > \omega$, THEN $f = \int_0^{\omega_0} e^{-\sqrt{\frac{\omega_0'^2 - \omega^2}{c^2}} x}$ AND THE DISTURBANCE

AT THE ORIGIN DIES OUT IN SPACE.

THE FREQUENCY IS SO LOW THAT THE MOTION IS SLOWER THAN FREE PENDULUM ACTION, AND THE SPRINGS CAN ADJUST TO A 'QUASI-STATIC' CONFIGURATION WITH ONLY A LOCALIZED REGION OF DISPLACEMENTS...